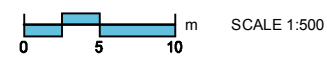
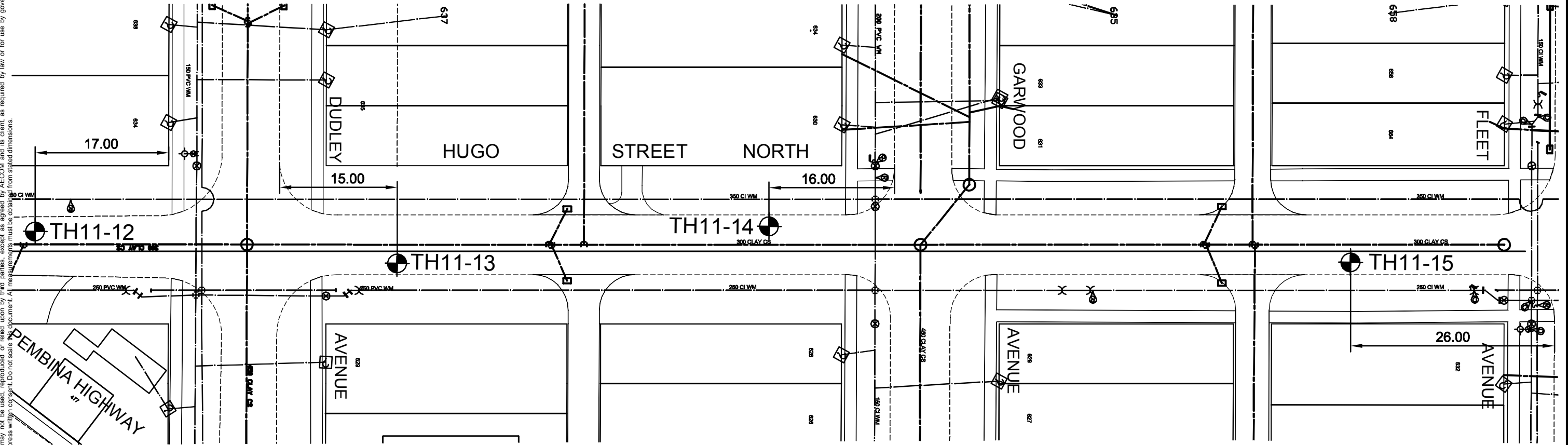


**AECOM**

**APPENDIX B  
HUGO STREET**

AECOM FILE NAME: Figure3-Hugo.dwg  
This drawing has been prepared for the use of AECOM's client and may not be used, reproduced, or relied upon by third parties, except as agreed by AECOM and its client, as required by law or for use by governmental reviewing agencies. AECOM accepts no responsibility, and denies any liability whatsoever, to any party that modifies this drawing without AECOM's express written consent. Do not scale this document. All measurements must be obtained from stated dimensions.



City of Winnipeg  
 2011 Residential Package  
 Test Hole Locations  
**Hugo Street North**  
 Pembina Hwy to Fleet Ave  
**Figure - 4**



PUBLIC WORKS DEPARTMENT • SERVICE DES TRAVAUX PUBLICS

Engineering Division • Division de l'ingénierie

## GEOTECHNICAL INVESTIGATION

### STREET RECONSTRUCTION

Revised October 28<sup>th</sup>, 2008

#### Fieldwork

1. Clear all underground services at each testhole location.
2. Test holes required every 50 m with a minimum of 3 test holes per street.
3. Record location of testhole (offset from curb, distance from cross street and house number).
4. Drill 150 mm-diameter core in pavement.
5. Drill 125 mm-diameter testhole into fill materials and subgrade
6. If a service trench backfilled with granular materials is encountered, another hole shall be drilled to define the existing sub-surface conditions.
7. Testhole to be drilled to depth of 2 m  $\pm$  150 mm below surface of the pavement.
8. Recover pavement core sample and representative samples of soil (fill materials, pavement structure materials and subgrade).
9. Measure and record pavement section exposed in the testhole (thickness of concrete or asphalt and different types of pavement structure materials).
10. Pavement structure materials to be identified as crushed limestone or granular fill and the maximum aggregate size of the material (20 mm, 50 mm or 150 mm).
11. Log soil profile for the subgrade.
12. Representative samples of soil must be obtained at the following depths below the bottom of the pavement structure materials - 0.1 m, 0.4 m, 0.7 m, 1.0 m, 1.3 m, 1.6 m, etc. Ensure a sample is obtained from each soil type encountered in the testhole.
13. Make note of any water seepage into the testhole.
14. Backfill testhole with native materials and additional granular fill, if required. Patch pavement surface with hot mix asphalt or high strength durable concrete mix.
15. Return core sample from the pavement and soil samples to the laboratory.

#### Lab Work

1. Test all soil samples for moisture content.
2. Photograph core samples recovered from the pavement surface.
3. Conduct tests for plasticity index and hydrometer analysis on selected soil samples which are between 0.5 m and 1 m below top of pavement (this is the sub-grade on which the pavement and sub-base will be built). The selection will be based upon visual classification and moisture content test results, with a minimum of one sample of each soil type per street to be tested.
4. Prepare testhole logs and classify subgrade (based on hydrometer) as follows;
  - < 30% silt - classify as clay
  - 30% - 50% silt - classify as silty clay
  - 50% - 70% silt - classify as clayey silt
  - > 70% silt - classify as silt

Prepared by: The National Testing Laboratories Limited and Eng-Tech Consulting

*Embrace the Spirit • Vivez l'esprit*

106 – 1155 Pacific Avenue • 1155, avenue Pacific, bureau 106 • Winnipeg • Manitoba • R3E 3P1  
Fax/télec. (204) 986-5302 • [www.city.winnipeg.mb.ca](http://www.city.winnipeg.mb.ca)

AECOM Canada Ltd.

## GENERAL STATEMENT

### NORMAL VARIABILITY OF SUBSURFACE CONDITIONS

The scope of the investigation presented herein is limited to an investigation of the subsurface conditions as to suitability for the proposed project. This report has been prepared to aid in the evaluation of the site and to assist the engineer in the design of the facilities. Our description of the project represents our understanding of the significant aspects of the project relevant to the design and construction of earth work, foundations and similar. In the event of any changes in the basic design or location of the structures as outlined in this report or plan, we should be given the opportunity to review the changes and to modify or reaffirm in writing the conclusions and recommendations of this report.

The analysis and recommendations presented in this report are based on the data obtained from the borings and test pit excavations made at the locations indicated on the site plans and from other information discussed herein. This report is based on the assumption that the subsurface conditions everywhere are not significantly different from those disclosed by the borings and excavations. However, variations in soil conditions may exist between the excavations and, also, general groundwater levels and conditions may fluctuate from time to time. The nature and extent of the variations may not become evident until construction. If subsurface conditions differ from those encountered in the exploratory borings and excavations, are observed or encountered during construction, or appear to be present beneath or beyond excavations, we should be advised at once so that we can observe and review these conditions and reconsider our recommendations where necessary.

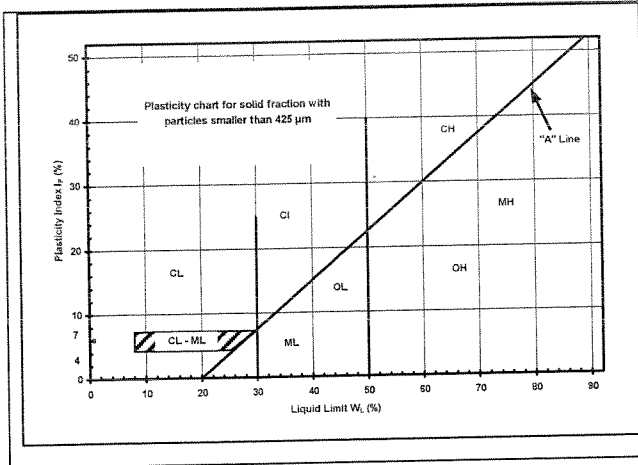
Since it is possible for conditions to vary from those assumed in the analysis and upon which our conclusions and recommendations are based, a contingency fund should be included in the construction budget to allow for the possibility of variations which may result in modification of the design and construction procedures.

In order to observe compliance with the design concepts, specifications or recommendations and to allow design changes in the event that subsurface conditions differ from those anticipated, we recommend that all construction operations dealing with earth work and the foundations be observed by an experienced soils engineer. We can be retained to provide these services for you during construction. In addition, we can be retained to review the plans and specifications that have been prepared to check for substantial conformance with the conclusions and recommendations contained in our report.

## EXPLANATION OF FIELD & LABORATORY TEST DATA

Description		UMA Log Symbols	USCS Classification	Laboratory Classification Criteria					
				Fines (%)	Grading	Plasticity	Notes		
COARSE GRAINED SOILS	GRAVELS (More than 50% of coarse fraction of gravel size)	CLEAN GRAVELS (Little or no fines)	Well graded gravels, sandy gravels, with little or no fines		GW	0-5	$C_u > 4$ $1 < C_c < 3$	Dual symbols if 5-12% fines. Dual symbols if above "A" line and $4 < W_p < 7$  $C_u = \frac{D_{60}}{D_{10}}$ $C_c = \frac{(D_{30})^2}{D_{10} \times D_{60}}$	
			Poorly graded gravels, sandy gravels, with little or no fines		GP	0-5	Not satisfying GW requirements		
		DIRTY GRAVELS (With some fines)	Silty gravels, silty sandy gravels		GM	> 12			Atterberg limits below "A" line or $W_p < 4$
			Clayey gravels, clayey sandy gravels		GC	> 12			Atterberg limits above "A" line or $W_p < 7$
	SANDS (More than 50% of coarse fraction of sand size)	CLEAN SANDS (Little or no fines)	Well graded sands, gravelly sands, with little or no fines		SW	0-5	$C_u > 6$ $1 < C_c < 3$		
			Poorly graded sands, gravelly sands, with little or no fines		SP	0-5	Not satisfying SW requirements		
		DIRTY SANDS (With some fines)	Silty sands, sand-silt mixtures		SM	> 12			Atterberg limits below "A" line or $W_p < 4$
			Clayey sands, sand-clay mixtures		SC	> 12			Atterberg limits above "A" line or $W_p < 7$
FINE GRAINED SOILS	SILTS (Below 'A' line negligible organic content)	$W_L < 50$	Inorganic silts, silty or clayey fine sands, with slight plasticity		ML		Classification is Based upon Plasticity Chart		
		$W_L > 50$	Inorganic silts of high plasticity		MH				
	CLAYS (Above 'A' line negligible organic content)	$W_L < 30$	Inorganic clays, silty clays, sandy clays of low plasticity, lean clays		CL				
		$30 < W_L < 50$	Inorganic clays and silty clays of medium plasticity		CI				
		$W_L > 50$	Inorganic clays of high plasticity, fat clays		CH				
	ORGANIC SILTS & CLAYS (Below 'A' line)	$W_L < 50$	Organic silts and organic silty clays of low plasticity		OL				
		$W_L > 50$	Organic clays of high plasticity		OH				
	HIGHLY ORGANIC SOILS		Peat and other highly organic soils		Pt	Von Post Classification Limit		Strong colour or odour, and often fibrous texture	
	Asphalt		Till			<b>AECOM</b>			
	Concrete		Bedrock (Undifferentiated)						
	Fill		Bedrock (Limestone)						

When the above classification terms are used in this report or test hole logs, the designated fractions may be visually estimated and not measured.



FRACTION	SEIVE SIZE (mm)		DEFINING RANGES OF PERCENTAGE BY WEIGHT OF MINOR COMPONENTS	
	Passing	Retained	Percent	Identifier
Gravel	Coarse	76	19	35-50 and
	Fine	19	4.75	
Sand	Coarse	4.75	2.00	20-35 "y" or "ey" *
	Medium	2.00	0.425	
	Fine	0.425	0.075	
Silt (non-plastic) or Clay (plastic)	< 0.075 mm		1-10	trace

\* for example: gravelly, sandy clayey, silty

Definition of Oversize Material  
COBBLES: 76mm to 300mm diameter  
BOULDERS: >300mm diameter

**LEGEND OF SYMBOLS**

Laboratory and field tests are identified as follows:

- $q_u$  - undrained shear strength (kPa) derived from unconfined compression testing.
- $T_v$  - undrained shear strength (kPa) measured using a torvane
- $pp$  - undrained shear strength (kPa) measured using a pocket penetrometer.
- $L_v$  - undrained shear strength (kPa) measured using a lab vane.
- $F_v$  - undrained shear strength (kPa) measured using a field vane.
- $\gamma$  - bulk unit weight ( $kN/m^3$ ).
- SPT - Standard Penetration Test. Recorded as number of blows (N) from a 63.5 kg hammer dropped 0.76 m (free fall) which is required to drive a 51 mm O.D. Raymond type sampler 0.30 m into the soil.
- DPPT - Drive Point Pentrometer Test. Recorded as number of blows from a 63.5 kg hammer dropped 0.76 m (free fall) which is required to drive a 50 mm drive point 0.30 m into the soil.
- w - moisture content ( $W_L, W_P$ )

The undrained shear strength ( $S_u$ ) of a cohesive soil can be related to its consistency as follows:

$S_u$ (kPa)	CONSISTENCY
<12	very soft
12 - 25	soft
25 - 50	medium or firm
50 - 100	stiff
100 - 200	very stiff
200	hard

The resistance (N) of a non-cohesive soil can be related to compactness condition as follows

N - BLOWS/0.30 m	COMPACTNESS
0 - 4	very loose
4 - 10	loose
10 - 30	compact
30 - 50	dense
50	very dense

PROJECT: 2011 Residential Street Renewal      CLIENT: City of Winnipeg      TESTHOLE NO: TH11-12  
 LOCATION: Hugo St. N., Southbound Lane, 17 m South of Dudley Ave., 2.2 m East of curb.      PROJECT NO.: 60212233  
 CONTRACTOR: Paddock Drilling Ltd.      METHOD: 125 mm SSA with 150 mm Coring      ELEVATION (m):

SAMPLE TYPE    GRAB    SHELBY TUBE    SPLIT SPOON    BULK    NO RECOVERY    CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	DEPTH
					SPT (Standard Pen Test) (Blows/300mm)	Total Unit Wt (kN/m <sup>3</sup> )	+ Torvane +	X QU X		
0		ASPHALT (thickness = 25 mm) CONCRETE (thickness = 185 mm)								
		CLAY - trace organics - black - high plasticity	GRAB	G95						
		SILTY CLAY - some sand - dark brown - frozen, moist when thawed - high plasticity	GRAB	G96					Gradation: Sand = 19.8%, Silt = 31.2%, Clay = 49.1%	
		SILT - light brown - frozen, moist when thawed - low plasticity	GRAB	G97						1
		- sandy at 1.2 m	GRAB	G98						
		CLAY - some silt, trace gypsum - dark brown - frozen to 2.0 m, moist when thawed	GRAB	G99						
			GRAB	G100						
		- below 2.0 m, firm	GRAB	G101						2
		END OF TEST HOLE AT 2.1 m in clay. NOTES: 1. No sloughing observed. 2. No seepage observed. 3. Test hole backfilled with auger cuttings, sand and asphalt cold patch to surface. 2. Drilled with 150 mm diamond core to 0.21 m, solid stem augers to 2.1 m.								3
										4

LOG OF TEST HOLE HUGO STREET, HOSMER BLVD, ACADIA BAY LOGS.GPJ, UMA WINN.GDT, 4/29/11



LOGGED BY: Stephen Petsche      COMPLETION DEPTH: 2.10 m  
 REVIEWED BY: Faris Khalil      COMPLETION DATE: 4/18/11  
 PROJECT ENGINEER: Faris Khalil      Page 1 of 1

PROJECT: 2011 Residential Street Renewal	CLIENT: City of Winnipeg	TESTHOLE NO: TH11-13
LOCATION: Hugo St. N., Northbound Lane, 15 m North of Dudley Ave., 2.1 m West of curb.		PROJECT NO.: 60212233
CONTRACTOR: Paddock Drilling Ltd.	METHOD: 125 mm SSA with 150 mm Coring	ELEVATION (m):

SAMPLE TYPE  GRAB  SHELBY TUBE  SPLIT SPOON  BULK  NO RECOVERY  CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	PENETRATION TESTS	UNDRAINED SHEAR STRENGTH	COMMENTS	DEPTH
0		ASPHALT (thickness = 30 mm) CONCRETE (thickness = 160 mm)						
		CLAY - dark brown - moist, soft - high plasticity  - below 0.5 m, frozen		G88	●			
				G89	●			
		SILT - light brown - frozen, moist when thawed - low plasticity		G90	●			1
		SITLY CLAY - brown - frozen, moist when thawed - intermediate to high plasticity		G91	●			
		CLAY - trace silt, trace gypsum - brown - frozen to 2.0 m, moist when thawed - high plasticity		G92	●			
				G93	●			2
		- below 2.0 m, firm to soft		G94	●			2
		END OF TEST HOLE AT 2.1 m in clay. NOTES: 1. No sloughing observed. 2. No seepage observed. 3. Test hole backfilled with auger cuttings, sand and asphalt cold patch to surface. 2. Drilled with 150 mm diamond core to 0.19 m, solid stem augers to 2.1 m.						3

LOG OF TEST HOLE: HUGO STREET, HOSMER BLVD, ACADIA BAY LOGS.GPJ, UMA WINN.GDT 4/29/11

LOGGED BY: Stephen Petsche	COMPLETION DEPTH: 2.10 m
REVIEWED BY: Faris Khalil	COMPLETION DATE: 4/18/11
PROJECT ENGINEER: Faris Khalil	Page 1 of 1





PROJECT: 2011 Residential Street Renewal	CLIENT: City of Winnipeg	TESTHOLE NO: TH11-14
LOCATION: Hugo St. N., Southbound Lane, 16 m South of Garwood Ave., 2.2 m East of curb.		PROJECT NO.: 60212233
CONTRACTOR: Paddock Drilling Ltd.	METHOD: 125 mm SSA with 150 mm Coring	ELEVATION (m):
SAMPLE TYPE	<input checked="" type="checkbox"/> GRAB <input type="checkbox"/> SHELBY TUBE <input checked="" type="checkbox"/> SPLIT SPOON <input type="checkbox"/> BULK <input checked="" type="checkbox"/> NO RECOVERY <input type="checkbox"/> CORE	

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	DEPTH
					* Becker * ◇ Dynamic Cone ◇ ◆ SPT (Standard Pen Test) ◆ (Blows/300mm) Total Unit Wt (kN/m³)	+ Torvane + X QU X □ Lab Vane □ △ Pocket Pen. △ ● Field Vane ● (kPa)				
0		ASPHALT (thickness = 25 mm) CONCRETE (thickness = 170 mm)								
		CLAY - trace sand, trace rootlets - black - frozen, moist when thawed - high plasticity		G81	●					
				G82	●					
		CLAYEY SILT - some sand - light brown - frozen, moist when thawed - low plasticity		G83	●				Gradation: Sand = 15.9%, Silt = 64.3%, Clay = 19.8%	
		SILTY CLAY - brown - frozen, moist when thawed - intermediate plasticity		G84	●					
		CLAY - trace silt - brown - frozen, moist when thawed - high plasticity		G85	●					
				G86	●					
		- trace gypsum at 1.8 m								
		SILTY CLAY - light brown - soft, moist - intermediate plasticity		G87	●					
		END OF TEST HOLE AT 2.3 m in silty clay. NOTES: 1. No sloughing observed. 2. No seepage observed. 3. Test hole backfilled with auger cuttings, sand and asphalt cold patch to surface. 2. Drilled with 150 mm diamond core to 0.195 m, solid stem augers to 2.3 m.								

LOG OF TEST HOLE - HUGO STREET, HOSMER BLVD, ACADIA BAY LOGS, GP J, UMA WINN GDT 4/29/11

LOGGED BY: Stephen Petsche	COMPLETION DEPTH: 2.30 m
REVIEWED BY: Faris Khalil	COMPLETION DATE: 4/18/11
PROJECT ENGINEER: Faris Khalil	Page 1 of 1



PROJECT: 2011 Residential Street Renewal      CLIENT: City of Winnipeg      TESTHOLE NO: TH11-15  
 LOCATION: Hugo St. N., Northbound Lane, 26 m South of Fleet Ave., 2.0 m West of curb.      PROJECT NO.: 60212233  
 CONTRACTOR: Paddock Drilling Ltd.      METHOD: 125 mm SSA with 150 mm Coring      ELEVATION (m):

SAMPLE TYPE     GRAB     SHELBY TUBE     SPLIT SPOON     BULK     NO RECOVERY     CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	DEPTH
					* Becker * ◇ Dynamic Cone ◇ ◆ SPT (Standard Pen Test) ◆ (Blows/300mm) ■ Total Unit Wt. ■ (kN/m <sup>3</sup> )	+ Torvane + X QU X □ Lab Vane □ △ Pocket Pen. △ ● Field Vane ● (kPa)				
0		ASPHALT (thickness = 30 mm) CONCRETE (thickness = 190 mm)								
		CLAY - dark brown - moist, firm - high plasticity		G74	●					
		SILT - trace clay, trace sand - light brown - frozen, moist when thawed - low plasticity		G75	●					
				G76	●					
		CLAY - trace silt, trace gypsum - brown - frozen to 1.7 m, moist when thawed - high plasticity		G77	●					
				G78	●					
		- below 1.7 m, firm		G79	●					
				G80	●					
		CLAYEY SILT - light brown - moist, soft - intermediate plasticity								
		END OF TEST HOLE AT 2.3 m in clayey silt. NOTES: 1. No sloughing observed. 2. No seepage observed. 3. Test hole backfilled with auger cuttings, sand and asphalt cold patch to surface. 2. Drilled with 150 mm diamond core to 0.22 m, solid stem augers to 2.3 m.								

LOG OF TEST HOLE - HUGO STREET, HOSMER BLVD, ACADIA BAY LOGS.GPJ, UMA WINN GDT, 4/29/11

LOGGED BY: Stephen Petsche      COMPLETION DEPTH: 2.30 m  
 REVIEWED BY: Faris Khalil      COMPLETION DATE: 4/18/11  
 PROJECT ENGINEER: Faris Khalil      Page 1 of 1





**Photograph 1. Hugo Street North – TH11-12**



**Photograph 2. Hugo Street North – TH11-13**





**Photograph 3. Hugo Street North – TH11-14**



**Photograph 4. Hugo Street North – TH11-15**

City of Winnipeg  
 2011 Residential Street Renewal – Hosmer, Hugo and Acadia  
 Geotechnical Investigation

Test Hole No.	Testhole Location	Pavement Surface		Pavement Structure Material		Subgrade Description	Sample Depth (m)	Moisture Content (%)	Hydrometer Analysis				Atterberg Limits				
		Type	Thickness (mm)	Type	Thickness (mm)				Gravel (%)	Sand (%)	Silt (%)	Clay (%)	Plastic Limit	Liquid Limit	Plasticity Index		
TH11-12	Hugo Street N., Southbound Lane, 17 m S of Dudley Ave., 2.2 m E of Curb	Asphalt	25	None	n/a	Clay	0.3	21.1									
						Silty Clay	0.6	28.3	0.0	19.8	31.2	49.1	58.4	23.9	34.5		
						Silt	0.9	27.4									
		Concrete	185			Silt	1.2	20.5									
						Clay	1.5	32.2									
						Clay	1.8	37.6									
						Clay	2.1	40.9									
TH11-13	Hugo Street N., Northbound Lane, 15 m N of Dudley Ave., 2.1 m W of Curb	Asphalt	30	None	n/a	Clay	0.3	27.3									
						Clay	0.6	32.2									
						Silt	0.9	27.9									
		Concrete	160			Silty Clay	1.2	25.3									
						Clay	1.5	30.5									
						Clay	1.8	37.5									
						Clay	2.1	42.2									
TH11-14	Hugo Street N., Southbound Lane, 16 m S of Garwood Ave., 2.2 m E of Curb	Asphalt	25	None	n/a	Clay	0.3	19.6									
						Clay	0.6	35.5									
						Clayey Silt	0.9	26.4	0.0	15.9	64.3	19.8	28.5	16.0	12.6		
		Concrete	170			Silty Clay	1.2	27.5									
						Clay	1.5	30.8									
						Clay	1.8	36.7									
						Silty Clay	2.1	38.5									
TH11-15	Hugo Street N., Northbound Lane, 26 m S of Fleet Ave., 2.0 m W of Curb	Asphalt	30	None	n/a	Clay	0.3	29.7									
						Silt	0.6	27.1									
						Silt	0.9	23.0									
		Concrete	190			Clay	1.2	26.9									
						Clay	1.5	36.6									
						Clay	1.8	40.2									
						Clayey Silt	2.1	43.9									