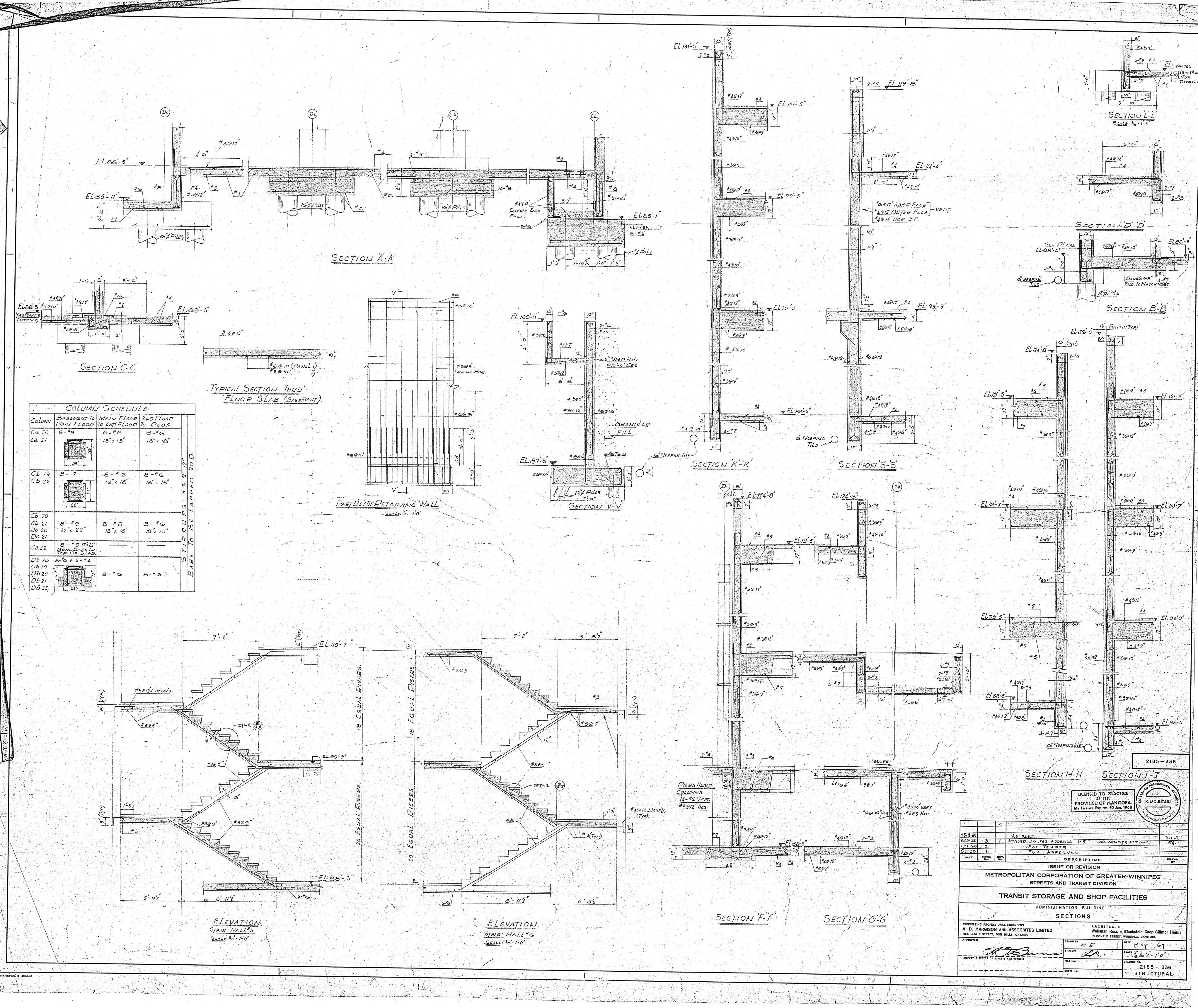
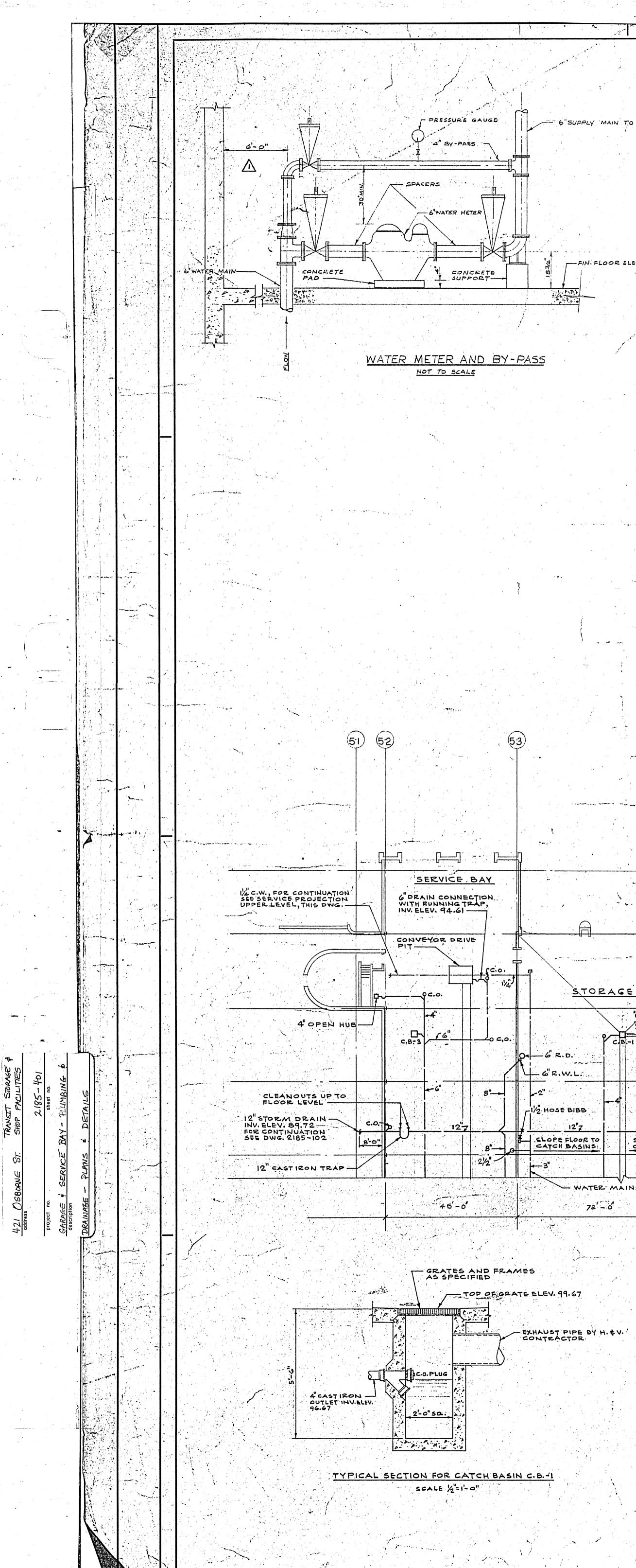


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23 SEC. A-A 6-#10 1 5-#10 #386° #3@12 3-#5 #6@ # 4012 · # 3@12 SECTION D-SECTION'C'-C' SECTION F.F. LICENSED TO PRACTICE IN THE PROVINCE OF MANITOBA My Licence Expires 10/Jan 1968 2185 / 335. EL.85'-11 K-MOUITAIN ----AS BUILT. SUMP PIT ADDED ~ ADDITIONAL REINF ADDED TO PILE-CAPE . R.L.J. TELEPHONE ROOM EXTENDED, Reinf ADDED . Reinf ADDED TO PILE-CAPE . R.L.J. Reinf ADDED . Reinf ADDED TO PILE-CAPE . R.L.J. Reinf ADDED . Reinf ADDED TO PILE-CAPE . R.L.J. Reinf ADDED . Reinf ADDED TO PILE-CAPE . R.L.J. FOR CONSTRUCTION FOR TANDER FOR APPRIVAL DRAWN BY DESCRIPTION ISSUE OR REVISION METROPOLITAN CORPORATION OF GREATER WINNIPEG STREETS AND TRANSIT DIVISION TRANSIT STORAGE AND SHOP FACILITIES ADMINSTRATION BUILDING MECHANICAL ROOM - REINFORCEMENT & DETAILS ARCHITECTS Waisman Ross • Blankstein Coop Gillmor Hanna 10 DONALD STREET, WINNIPEG, MANITOBA DATE MAY 67. DRAWN BY Carrier ? DRAWING No. 2185 - 335 STRUCTURAL





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S. Same

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	LEGEND			
6" SUPPLY MAIN TO BUILDINGS	501L, WASTE OR LEADER A SOIL, WASTE OR LEADER E		-/ M	
	COLD WATER 	IG		
	GAS 	(59)	60	(6)
FIN. FLOOR ELEV. 100'-0"		STORAG	E BAYS BETWEEN COL'S. 59 & 61 NOT IN CO SEE SPECIFICATION	NTRACT
56	<u>57</u>			
-PASS				
1. MINIMUM SLOPE FOR UNDERFLOOR STORM DRAINAGE PIPING - 14 PER LINEAR FOOT 2. MINIMUM SLOPE FOR GARAGE FLOOR DRAINAGE PIPING - 18 PER LINEAR FOOT 3. ALL STORM & SANITARY DRAIN CONNECTIONS			STORAGE BAY # 4	B
3. ALL STORM & SANITARY DRAIN CONNECTIONS LOCATED UNDER BERMS OUTSIDE BUILDING WALLS SHALL BE CONCRETE PIPE ASTM C-14-E.S. 4. IN GARAGE & SERVICE BAY AND OVERHAUL & REPAIR SHOP ALL UNDERFLOOR DRAINAGE PIPING CARRYING WASTES TO OIL INTERCEPTORS SHALL BE AS SPECIFIED FOR UNDERGROUND INDUSTRIAL DRAINAGE PIPING			- 6" R.W.L. - 6" R.W.L. - 6" R.W.L. - 6" R.W.L. - 6" R.W.L. - 6" R.W.L. - 6" R.W.L.	c.o.
		1/2 DOWN, CAP PIPE 4-0" ABOVE FIN. FLOOR FOR UTURE CONNECTION TO 1/2" HOSE BIBB IN STORAGE BAY #4		
$\overline{\Box}$	4" VENT BELOW FLOOR	Τ	-4	-4" -4"
(54) OFFSET IN JOIST SPACE	G"VENT UP THROUGH ROOF	<u>3</u> "	د o.	o C.O.
	-1/2 HOSE BIBB	1/2"HOSE BIBB	6" R.W.L.	
			<u>с.в1</u>	
53)	c.o.?	4		34-
-UNDERFLOOR EXHAUST DUCT BY H. & V. CONTRACTOR, INV. ELEV. 97.5 - TYPICAL FOR ALL LOCATIONS				CLEANOUTS UP TO GRADE
C.O.O G'R.W.L	6" E. D. Q	$\frac{1}{2} = \frac{1}{2} = \frac{1}$	6"R.D.Q - CAP FOR FUTURE "O"CONNECTION "G"R.W:L 10"- G"R.W:L 10"- CONNECTION CONNECTION CONNECTION CONNECTION	LEVEL
SLOPE FLOOR TO SLOPE FLOOR TO SLOPE FLOOR TO CATCH BASINS				12"CASTIRON TRAR 0 C. O.
SLOPE FLOOR TO CATCH BASINS 4"	SLOPE FLOOR TO CATCH BASINS		SLOPE FLOOR TO CATCH BASINS	SLOPE FLOOR TO
	∃ → → → → → → → →	B"	1% C.W. TO WASHROOM,	4"орен нив 4"2
<u>STORAGE BAY #1</u> - 6" R.W.L. 	С.0. 		GR.D.O C.O.	1/2 HOSE BIBB - 2-4" VENTS RUN UP AT WALL
		-6" -6" -6" -6" -6" -6" -6" -6"	+ *	-6" NGIDE THE BUILDING, OFFSET BELOW STEEL BEAM AND UP THROUGH ROOF AS GHOWN. PROVIDE &" SCH. 40 PIPE SLEEVE THROUGH GRADE BEAM FOR EACH VENT 12" HOSE BIBB
		W2" HOSE BIBB	-CAP.FOR FUTURE 6" CONNECTIONS 6" CONNECTIONS	
Lelope FLOOR TO CATCH BASINS 		IN JOIST SPACE	6"R.N.L. 23"	BZ W
WATER MAINS IN JOIST SPACE	<u>FOR CONTINUATION SEF DWG. No 2185-502</u> <u>5 C.B1, ELEV. 99.67</u>	3'	01L INTE DETAIL D 11	RCEPTOR SEE WG. No 2185-402 4"SCH: 40 GALY. BTEEL VENTS, TERMINATE B FT. ABOVE FIN. GRADE. PROVIDE

ويساف فاقعا فالعار والمرابط

والالو مسعة بواريو

GARAGE PLAN SCALE 1/6=1'-0"

TOP OF GRATE ELEVATION AS SHOWN ON PLAN DRA-WINGS GRATES AND FRAMES AS SPECIFIED. PROVIDE 4 KI X 7"LONG STEEL STRAP ANCHORS SPACED AT 2'-G" ON CENTRES AND WELDED TO FRAMES IN ALL TRENCHES

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man francis

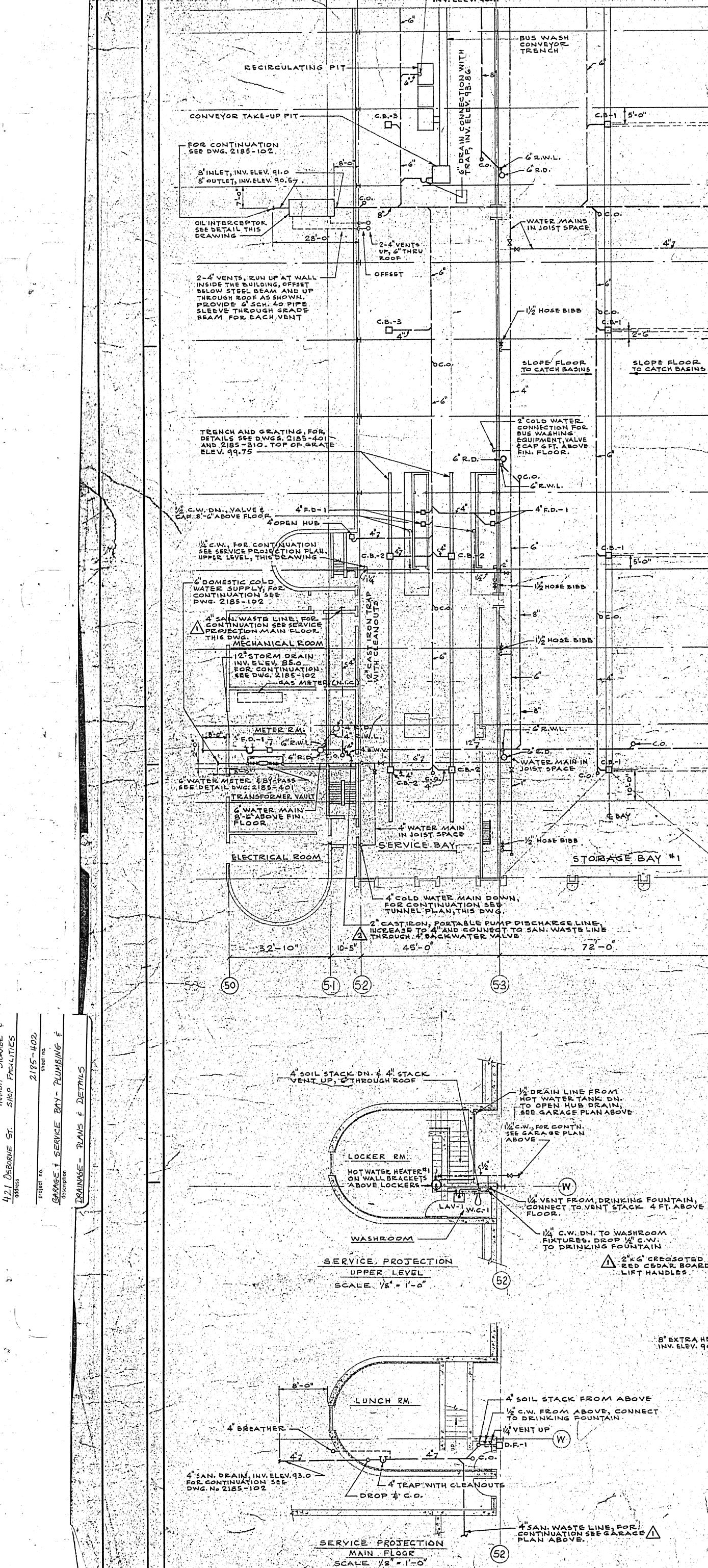
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11 A.		AND WELDED TO FRAMES IN ALL TRENCHES	10
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1	TRENCH	2'-0" TRENCH	<u></u>
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TYPICAL SECTIONS FOR CATCH BASIN C.B-2 SCALE 1/2=1-0"

NOTE: CATCH BASIN C.B.-3 IS SIMILAR BUT WITHOUT TRENCH CONNECTION

	SOIL, WASTE OR LEADER ABON SOIL, WASTE OR LEADER BELC COLD WATER HOT WATER HOT WATER RECIRCULATING VENT GAS GATE VALVE CHECK VALVE		60		61
57	58		ORAGE BAYS BETWEEN COL'S. 5 SEE SPECIFIC		
		DWN, CAP PIPE 4-0" E FIN. FLOOR FOR E CONNECTION TO SE BIBB IN STORAGE BAY #4	<u>STORAGE</u> <u>c.o.0</u> <u>-</u> <u>-</u> <u>-</u> <u>-</u> <u>-</u> <u>6</u> " <u>c.b.1</u> <u>6</u> " <u>R.D.</u> <u>0</u>	R.W.L.	
4" VENT BEL 4" VENT UP C.a. 0 CB-T CB-T 	STORAGE BAY #3		0 c o. 6" R.W.L. 6" R.D. O	β [*] β C.O.	С
	23" 6" e, p, Q		-G" 6"R.D.Q	-10" C.O. C.D. CLEANOUTS UP TO GRADE LEVEL TO"CONNECTION	A A A A A A A A A A A A A A
SLOPE FLOOR TO CATCH BASINS	-O'PE' FLOOR TO CATCH BASINS	$\frac{10^{10}}{10^{10}}$	P PIPE E FIN.	LOPE FLOOR C.B.1	
C:0.7 C:0.7 C:B-1 11/2" HOSE BIBB	23		ON TO IBB IN AY #4 G"R.D.O FIRE FIRE FUTURE DN TO IB IN AY #4	.W. TO WASHEOOM, CONTINUATION SEE VICE PROJETION ER LEVEL, THIS DWG. -8" -8" -2-4" VEN TS UP, C" THEU' ROOF.	
SINS C.B1, ELEV. 99.67	- 4 501L STACK	WATER MAINJ IN JOIST SPACE 3"	G"CONNECTIONS	CAP FOR FUTURE 6"CONNECTIONS B" C.B.T. WATER MAIN IN JOIST SPACE B" OIL INTERCEPTOR SEE DETAIL DWG. No 2185-402	BOR CONTINUATION
To LAY	ATER HI TA DRINKING TA DRINKING TA DRINKING I'' VENT FRO FOUNTAIN, O STACK VEN FLOOR. I''' CRN, FOR CON SEP GARAGE PL IVE'' GAR M KOJTECTION	WASHROOM 200 1/2 C.W. FOUNTAIN M DRINKING ONNECT TO T 4FT. ABOVE STORAGE LOFT AN ABOVE W. FOR. CONT. SEE GE PLAN ABOVE	NOTECTION	2 REVISED PER PROPOSED NOTIC	
4" SAN. DRAIN INV. ELEV. 93 FOR CONTINUATION SEE DWG. N. 2185-102 -4" BREA	THER OP & CLEANOUT 4"Z 5C.O. 1/4" VENT UP 1/4" VENT UP	CK FROM 4" SOIL PIPE ELEV. 93:5 3"F.P 3, 1/2" MASHROOM G-126	DM TO INV AND HIVENTUP	FOR CONSTRUCTION FOR TENDER FOR APPROVAL DESCRIPT ISSUE OR REVIS ETROPOLITAN CORPORATION OF STREETS AND TRANSIT TRANSIT STORAGE AND S GARAGE & SERVICE	ION ION F GREATER WINNIPEG DIVISION HOP FACILITIES



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-						-++				3"
6				-6	-8	B			- 14 - 1	
e S		-		с.	31		CB			<u> </u>
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F				х х						
			3″							
		4 4				¥	0 6 R.D. - 6 R.W.L.			
))	=0.		-1/2 HOSE BIBB	od.		_	8"7			
			1/2" HOSE DIBB				4" 7	I'∕2" HOSE BIBB		
				•					8	
-	6			- 6				6		
20	 0.									
					-1		С.в.			
	SLOPE FLOOR			0 <i>C</i>				ю <i>с.о.</i>		
	TO CATCH BASINS		-3" SLOPE FLOOR TO CATCH BASINS		SLOPE FLOOR T	τ¢	CATCH BASINS	SLOPE FLOOR TO CATCH BASINS		-1/2" H
							-6"R.W.L.			SLOPE To CATO
				- 6	c.o.o/.		О <i> 4</i> " Я. D.			3*
	G	14.94 • •							•	
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D	εο.					4 - 24 - 24 - 24 - 24				
		-	-1/2" HOSE BIBB	b¢				o <i>c.o.</i>		1
4	4							1/2 HOSE BIBB		
				0		= p	0 6" R.D.	OFFSET IN JOIST	et ja artist artist	
	<u> </u>						C.O.	G'VENT UP	Г	
	B)					EX JA	HAUST DUCT BY H. & V. INV. ELEN. 97.5 - TYPICAL TIONS-			4" VEN FLOOR
		1 -1 -					C.B.	Hoc.o. 4"VENTS UP-2	3	
	E BAY				- STORAG	56	E BAY #2	L INV. ELEV. 96.67		INV. EL
			1/2 HOSE BIBB		F BAY					1/2+
R	ASE BAY #1		• •	· · · · · · · · · · · · · · · · · · ·						
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WENTS-8 OUTLET ----4 VENT -4 VENT PLAN

The second secon VENTS-----_____ A 2"KG" CREOSOTED WESTERN RED CEDAR BOARDS WITH LIFT HANDLES 4-0 4-0" _____ i sa internet VENTS 4 VENTS 4 VENTS 4 VENT-⊬8"⊂.1. · ____ · Animal · ~8"C.1.

1 (m. 17)

SECTION A-A

OIL INTERCEPTOR 5 CALE 4 = 1-0"

INLET I STYROFOAM INSULATION /I - 24" & GAS - TIGHT MANHOLE FRAMES AND COVERS, CANADA IRON CAT.

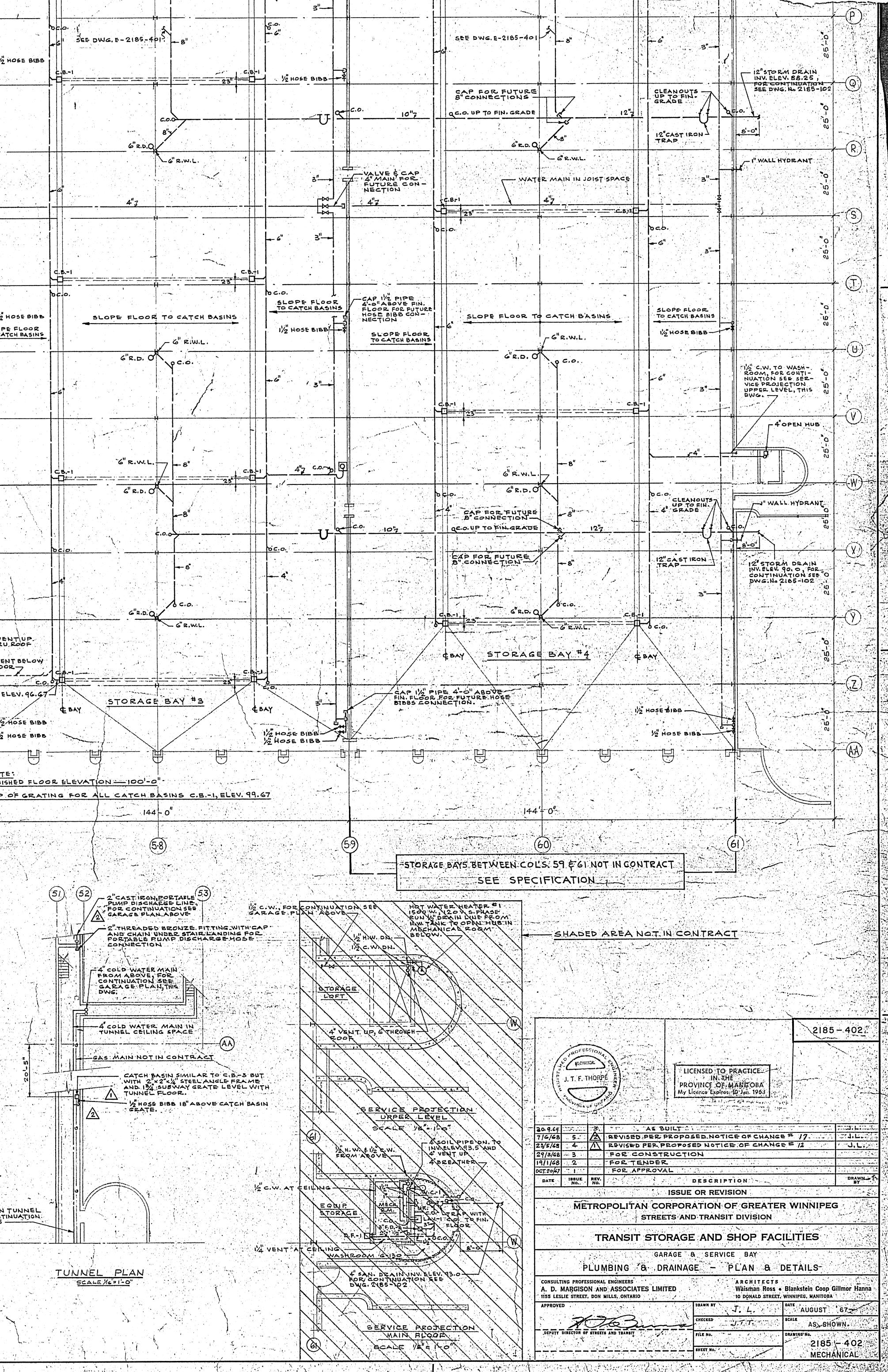
GARAGE PLAN

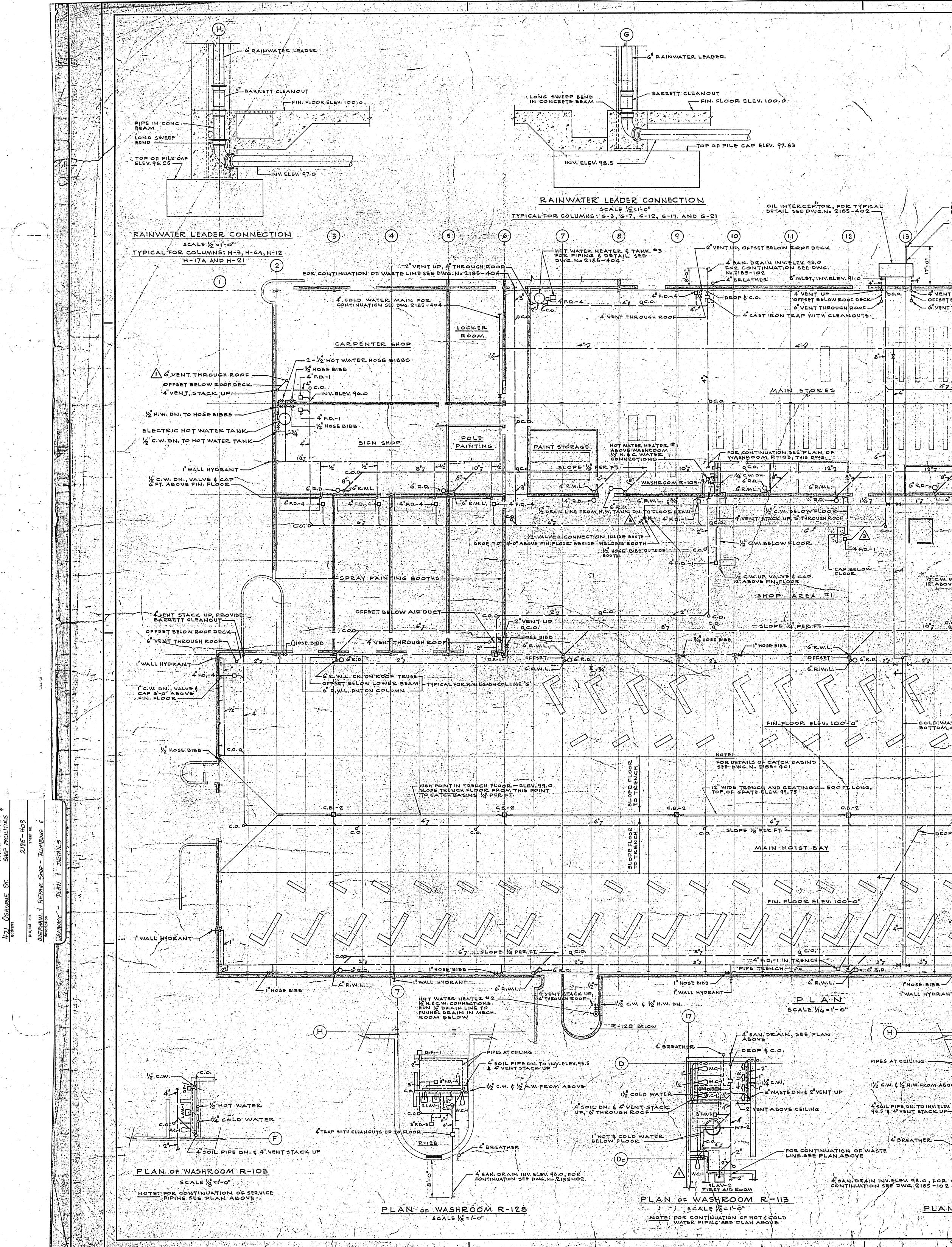
SCALE 116 = 1'- 0"

No 4894 FIN. GRADE 4 VENTS -I"STYROFOAM INSULATION 3/4 STEEL LADDER RUNGS, 12 0, C., CANADA IRON CAT, No 4881 - 2/2 × 2 × 4 STEEL ANGLE FRAME WITH 12 BOLTS AT & ON CENTRES. ANGLES TO BE COATED WITH BITUMASTIC PAINT.

- 8" EXTRA HEAVY CAST IRON INLET, INV. ELEV. 91.0 NOTE: UPPER VENTS FOR OIL INTERCEPTOR LOCATED INSIDE OVERHAUL & REPAIR SHOP ONLY, CREOSOTED WOOD PANELS, STYROFOAM INSULATION AND LOWER VENTS FOR OUTSIDE INTERCEPTORS ONLY

4" COLD WATER MAIN IN TUNNEL CEILING, SPACE, FOR CONTINUATION SEE DWG. No 2185-405





A stand of the second second

1.18

ELECTRIC HOT WATER TANK (I REQUIRED) SUPPLY AND INSTALL FACTORY INSULATED COPPER ELECTRIC HOT WATER TANK RUND MODEL CE 52, 40 IMP. GAL. CAPACITY, COMPLETE WITH TWO (2) 3000 WATTS, 208 V., SINGLE PHASE ELEMENTS, CONTROL THERMOSTATS AND TEMPERATURE AND PRESSURE RELIEF VALVE, PROVIDE DRAIN LINE FROM RELIEF VALVE, TERMINATE 6"ABOVE FIN. FLOOR.

and the second

-FOR CONTINUATION SEE DWG. No 2185-102 - B OUTLET, INV. ELEV. 90.5

(4).		6	١	B	(19)	20
	-11-0.					4 SAN. DRAIN CONTINUATIO	INV. ELEV 93.0, FO SEE DWG, 2185-16	R 2
.0.	-4" VENT UP	W ROOF DECK	4" F.D,4	1/2 COLD WATER	-0 -1/4	-1/4" C W. DN. 14	4 VENT STAC	CK FROM
	G"VENT THR		6" VENT STAC THROUGH R	DN. INTO PIPE SPACE BELOW	<u>R-113</u>	-1" H & C. WAT	R DNCIN PIPE SPA	ATION 55-405 .CE
		SPACE	MAIN IN'JOIST	NG SPACE		1"2 - 34"2	-	05E BIBB
			FOR CONTINUA	TION OF WASTE	-1135 -2	3 F.D.		PIPES IN JOIS
-4	47 47	<u>ос.о.</u>	47	0 co.		1/2 HOSE	BIBB	BASE For 2185
					1.4	<u>3"7</u> D c.o.		O. ELECTRICAL T
					c.o.ơ		G'Z	REA #2
	12"7		12"7		147	مرجنه،،،		
	6" R.D0	2-34 HOSE BIB			W. C.	دی. ۱۰۵ - ۲۰	8	
		C.W. BELOW		C.O. 4" R.D.	<i>c.o.</i> 0		N SVALVE & CAP	
		- 1/2 C.W. UP; VAI 12" ABOVE FIN:	VE & CAP FLOOR 4"F.D.		2*			
-4								
	12" ABOVE F	ALVE & CAP				-12 DNI, VALVE	200 2 САР 6 ВТ. <u>/3)</u> DP, 4". ТНРОЦЕН Р	00F
	c.0.	- V2 C.W. BEL	-4"F.D1 OW FLOOR	C.O.	c.o.o	INTERNAL AND IN	C.W. BELOW FLOOR CONC. BLOCK WAL F1	4 UP
		HOSE BIBB		- 3/4 HOSE BIBB	2=		IGH POINT IN TRENCH	6 R
4	× 27		2-5-3/2	G R. W.L.	C G R.D	ана (рака) 	DE BIBB	F
							WIDE TRENCH AND O DP OF GRATE ELEV 9 LOPE TRENCH FLOO	RATING 1.
	COLD WATER BOTTOM_CHO	MAIN ABOVE						
			FLOOR NCH R					INV.
			SLOPE SLOPE				FLO	REASING ROOM
	DROP. EC	<u>č'7 </u>		6'7 . Jc.o.				<u> </u>
			PE FLOO					
/			14r 2			<u> </u>		
				4".F.D1 OFGRA	IN PIT, TOP	0	0 -4"ED	-1 IN PIT TOP OF
7 4•	AN	Ant			A		GRATE	ELEV. 95.0
	-3"2	10"7 C	P. Q	2"			Q. c.o	12 ⁶ 7
-14-	HOSE BIBB			-1/2		LI"HOSE BIBI		RANT - G"R.U
1 ^{**}	WALL HYDRANT		(17)			G" ROOF DR G" R.W.L. CUP, G" THROU	AIN GH ROOF B" SA	N: DRAIN INV. EL
)—) 			WATER HEA C:W. CONNE 地 DRAIN LI NEL DRAIN I M BELOVI	CTIONS. NE TO		
T CI	EILING	[D.F1		24 BELOW			
¢ 1/2	H:W. FROM ABOVE	3"F.D,-4	2 3 3					
1PE 4" VI	DN: TO INV. ELEV.		c.o.					
B	LEATHER	4-1 -4"TRAP -4"TRAP -4"TRAP		SUP TO FLOOR				OT TESTON
								J. T. F. THORPE

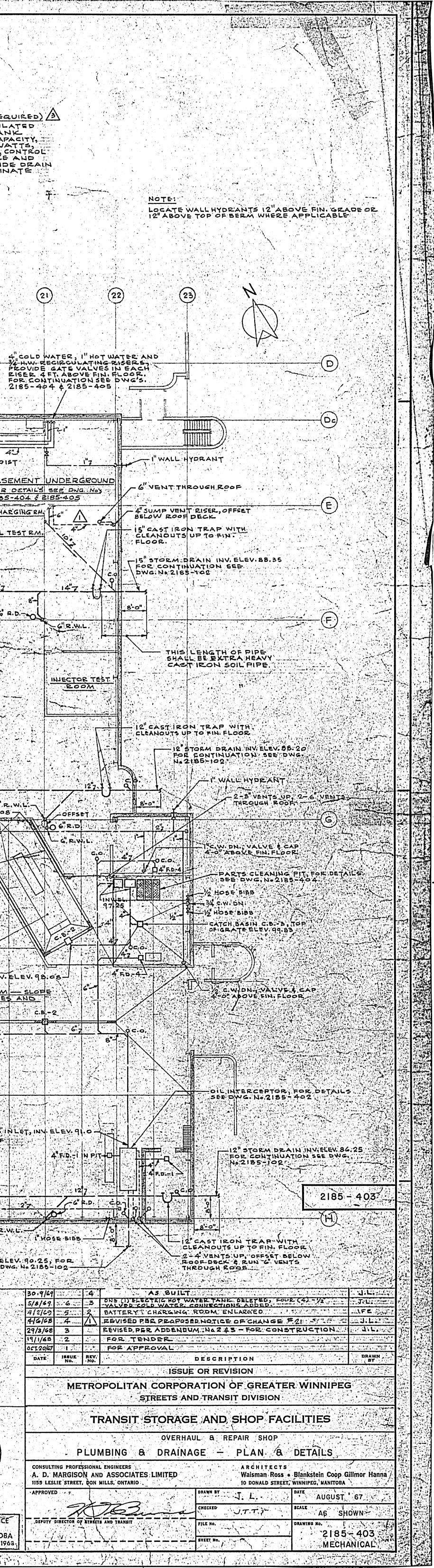
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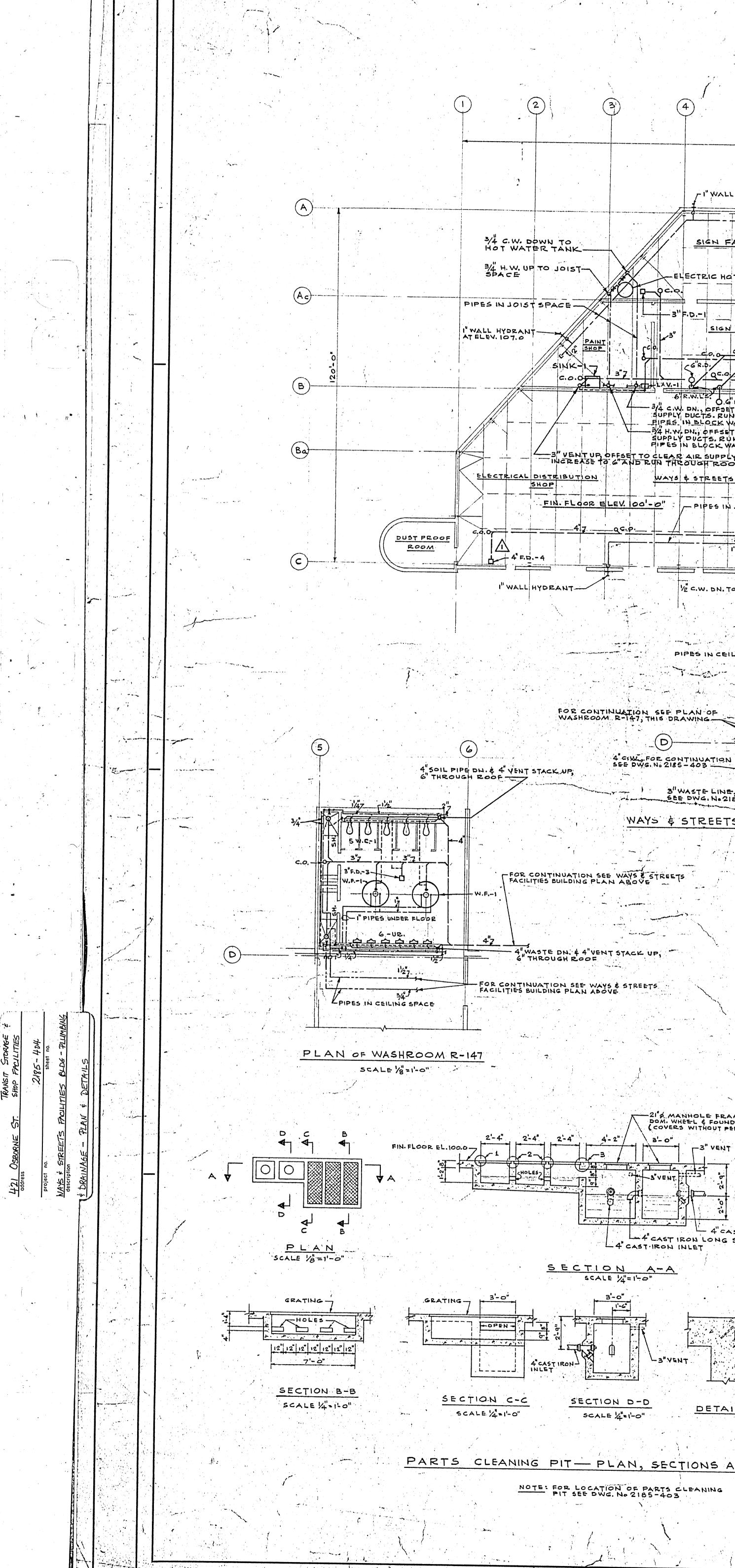
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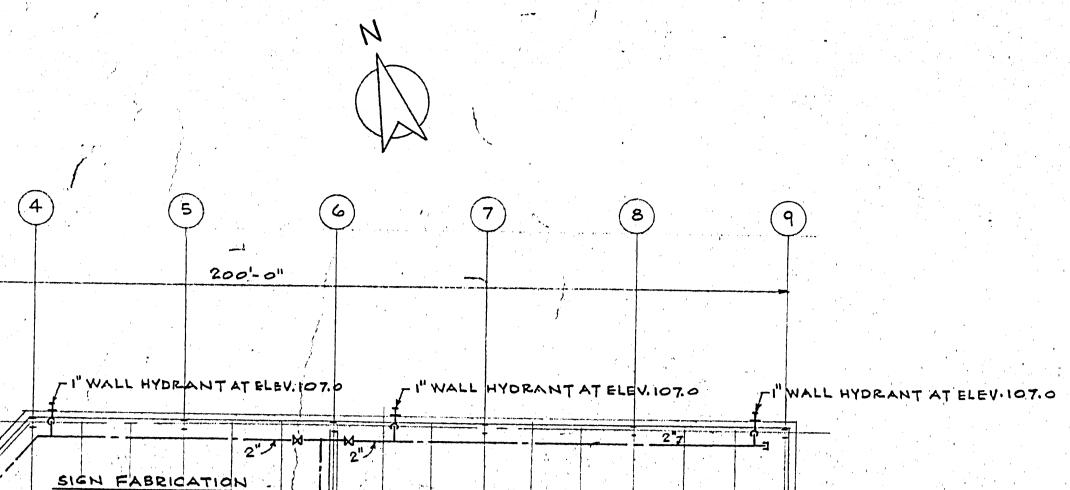
PLAN OF WASHROOM R-124 SCALE 1/4 = 1-0"

Set 1 Sumar

T' F. THORPE LIGENSED TO PRACTICE IN THE PROVINCE OF MANITOBA 12 Licence Expires: 10 Jan. 1968







-ELECTRIC HOT WATER TANK STORAGE & HANDLING AREA SIGN STORAGE 10 7 ~6 R.D 195.0/) *C.O*.

- OTTALAV.-1 6 R.W.LS. O.G.R.D. 3/4 C.W. DN., DEFSET TO CLEAR AIR SUPPLY DUCTS. RUN 2 BRANCH PIPES IN BLOCK WALL TO FIXTURES 6"R.D.-06 R.D. -6"R.W.L'S. TEAP NOT REQ'D. FOR THIS DRAIN - 34 H.W. DN., OFFSET TO CLEAR AIR SUPPLY DUCTS. RUN 1/2 BRANCH FIRES IN BLOCK WALL TO FIXTURES TRUCK STORAGE AREA FIN. FLOOR ELEV. 97.0 -3" VENT UP, OFFSET TO CLEAR AIR SUPPLY DUCTS,

WAYS & STREETS SHOP

- 2"VENT UP, 4"VENT THROUGH ROOF FIN. FLOOR ELEV. 100'-0" - PIPES IN JOIST SPACE -12 HOT & COLD WATER DN. TO LAVATORY ,] ###wite a mini o as a manuf [minimum hand as any hims 95.0. 47 21 C.O. L 3/4 HOSE BIBE -LAV.-I L.C.O. O. C"R.W.L. 4" F.D. -4 PARKING METERS D.F.-1 06 R.D.

4----

12 C.W. DN. TO DRINKING FOUNTAIN LOCKER ELEV. 100-0 ROOM 00.0. FOR CONTINUATION SEE PIPES IN CEILING SPACE

LUNCH RM. a second 4 SAN. DRAIN INV. ELEV. 93.0 FOR CONTINUATION SEE DWG. N. 2185-102 WASHROON FOR CONTINUATION SEE PLAN OF WASHROOM R-147, THIS DRAWING R-147 DROP & C.O.-

GAS PRESSURE REGULATOR 5 PSI TO II"WIC., PROVIDE "VENT THROUGH ROOF THE SALE HEATER "GAS DN. , CONNECT TO HEATER 4 CIW FOR CONTINUATION SEE DWG. No 2185 - 403 the part tors tors -543 U.S.G. HOT WATER 3"WASTE LINE, FOR CONTINUATION A GEE DWG. N. 2185-403 SEE DWG. No 2185-603 WAYS & STREETS FACILITIES BUILDING PLAN

FOR CONTINUATION SEE WAYS & STREETS

SCALE 116=1-0"

-21 & MANHOLE FRAME & COVER DOM. WHEEL & FOUNDRIES D.S. 1565 (COVERS WITHOUT PERFORATIONS)

- 4" CAST IRON OUTLET L. 4" CAST IRON LONG SWEEP BEND -4 CAST IRON INLET

SECTION A-A SCALE 1/4=1-0" 7 14 RECTANGULAR SUBWAY GRATING 7 FLOOR - 2 × 2 × 3 L FRAME A ANCHORED TO CONCRETE WITH X × 1" STEEL STRAP ANCHORS 2'-6 -3"VENT ON CENTRES.

1. 1. 1. 1.

SECTION D-D DETAIL DETAIL 2 SCALE 4=1-0"

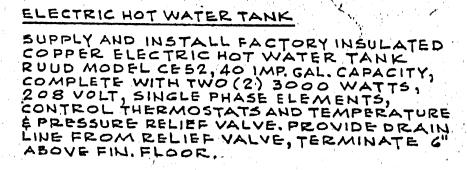
PARTS CLEANING PIT -- PLAN, SECTIONS AND DETAILS

NOTE: FOR LOCATION OF PARTS CLEANING PIT SEE DWG. No 2185-403

DETAIL 3

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OPT FOR



SINK-I

SUPPLY AND INSTALL STAINLESS STEEL SINK, SIZE 60"LONG X 48"WIDEX 35"HIGH, SINK TUB -12" DEEP. MATERIAL - STAINLESS STEEL TYPE 316, 14 GAUGE. SINK CONSTRUCTION - ALL WELDED, TO CONFORM TO CSA SPECIFICATIONS, ALL CORNERS COVED. TOP EDGES - ROLLED ON 34 RADIUS. TOP CORNERS - RADIUSED. SADDLES - 12 GAUGE GALVANIZED IRON, ENDS CUT BACK. LEGS & BRACES - 15% O.D STAINLESS STEEL TUBING - SIX REQUIRED. FEET - STERLING OR HARALSON WITH BEVELLED TUBING AND STAINLESS STEEL STUD SLEEVE. DRAIN - 1% SIZE, COMPLETE WITH STAINLESS STEEL TAILPIECE, STANDING OVERFLOW AND 16 GAUGE PERFORATED STRAINER, SINK BOTTOM SHALL SLOPE TO DRAIN-DO NOTCREASE, AND DRAIN SHALL BE LOCATED IN CORNER AT LOWEST POINT OF BOTTOM.

SINK SUPPLIER - HOSPITAL & KITCHEN EQUIPMENT COMPANY, TORONTO. SUPPLY FITTING - CRANE CH-8556 MOUNTED ON BLOCK WALL ABOVE SINK, 12" FROM RIGHT HAND CORNER. TRAP - CRANE C-5103 CAST BRASS ADJUSTABLE P TRAP WITH

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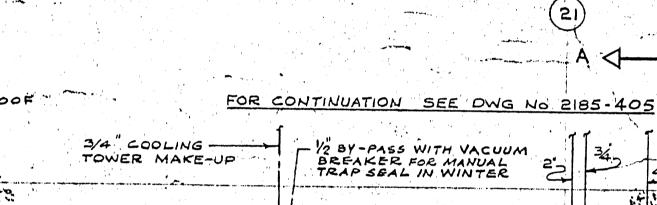
12-

UP TO FINISHED FLOOR

- 10"STORM DRAIN INV. ELEV. 92.0 FOR CONTINUATION SEE DWG. No 2185-102

TWO (2) INLET AND ONE (1) OUTLET DIP TRAPS,





TRAP PRIMER VALVE & LINE CHIMNEY----3/4 VALVED & CAPPED -----10"I.D. TYPE B GAS VENT. GAS WATER HEATER #4 -RUUD MODEL 500B

> G-00 ----HOT WATER TANK 4-

BOILER FIN. FLOOR ELEV. 85.92

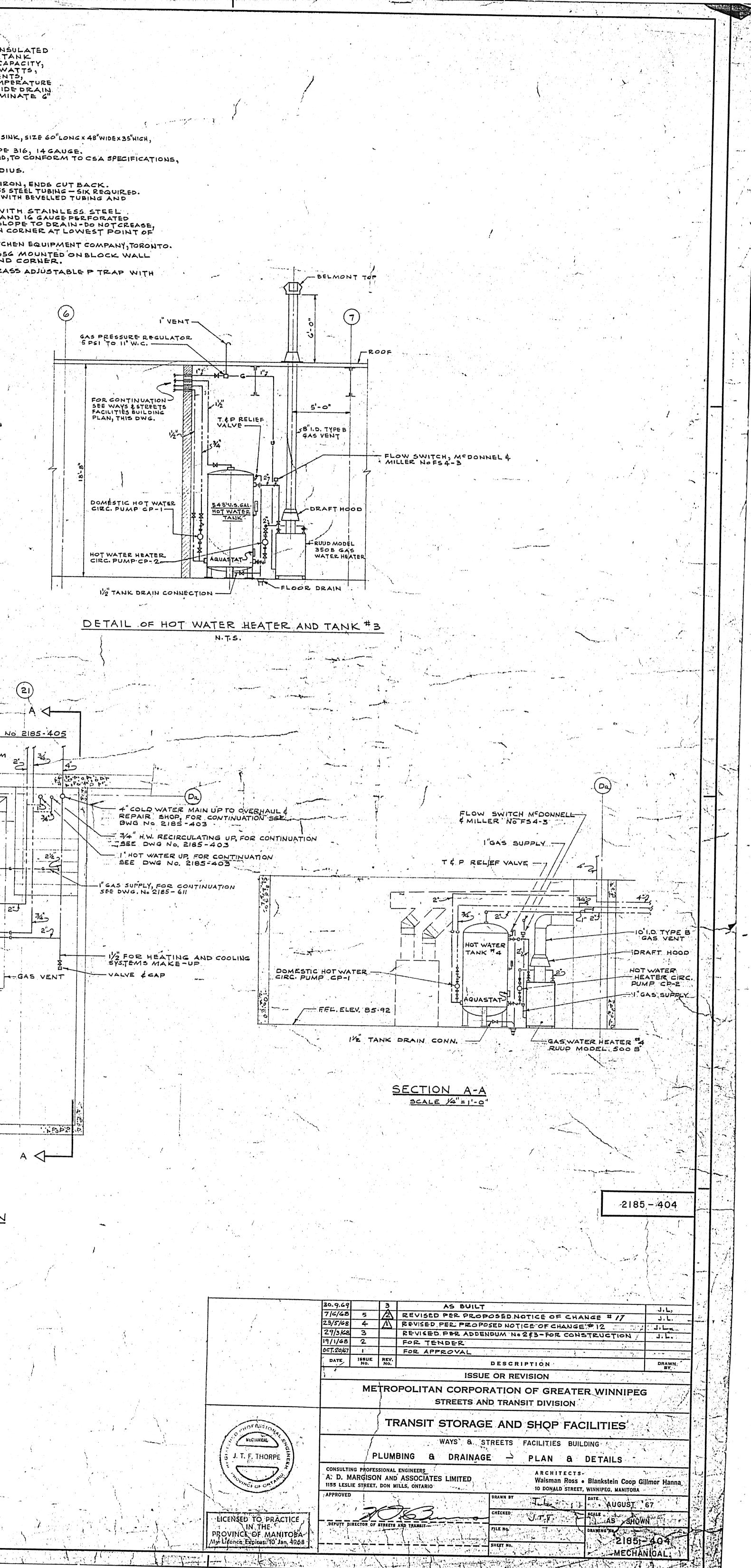
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MECHANICAL ROOM PLAN

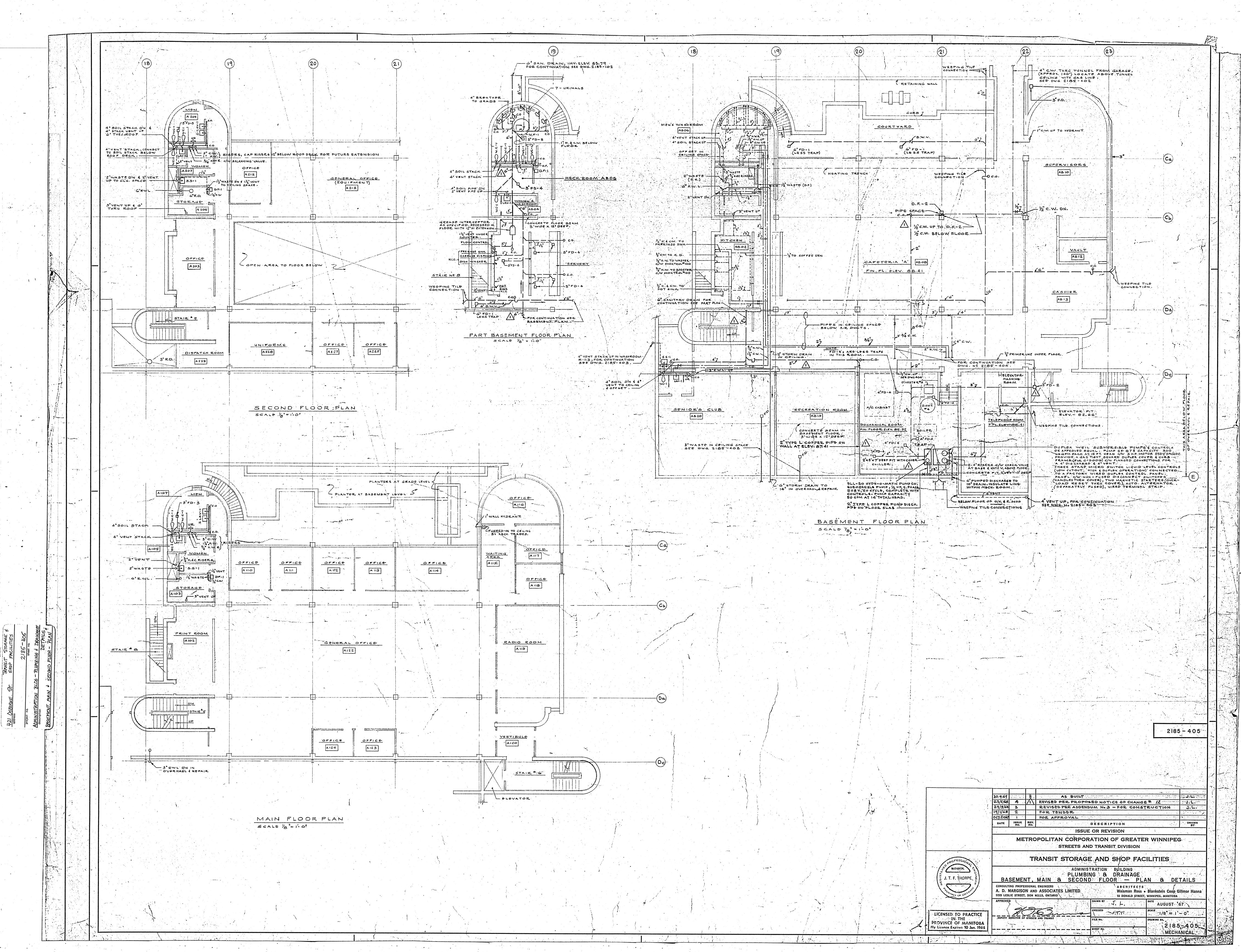
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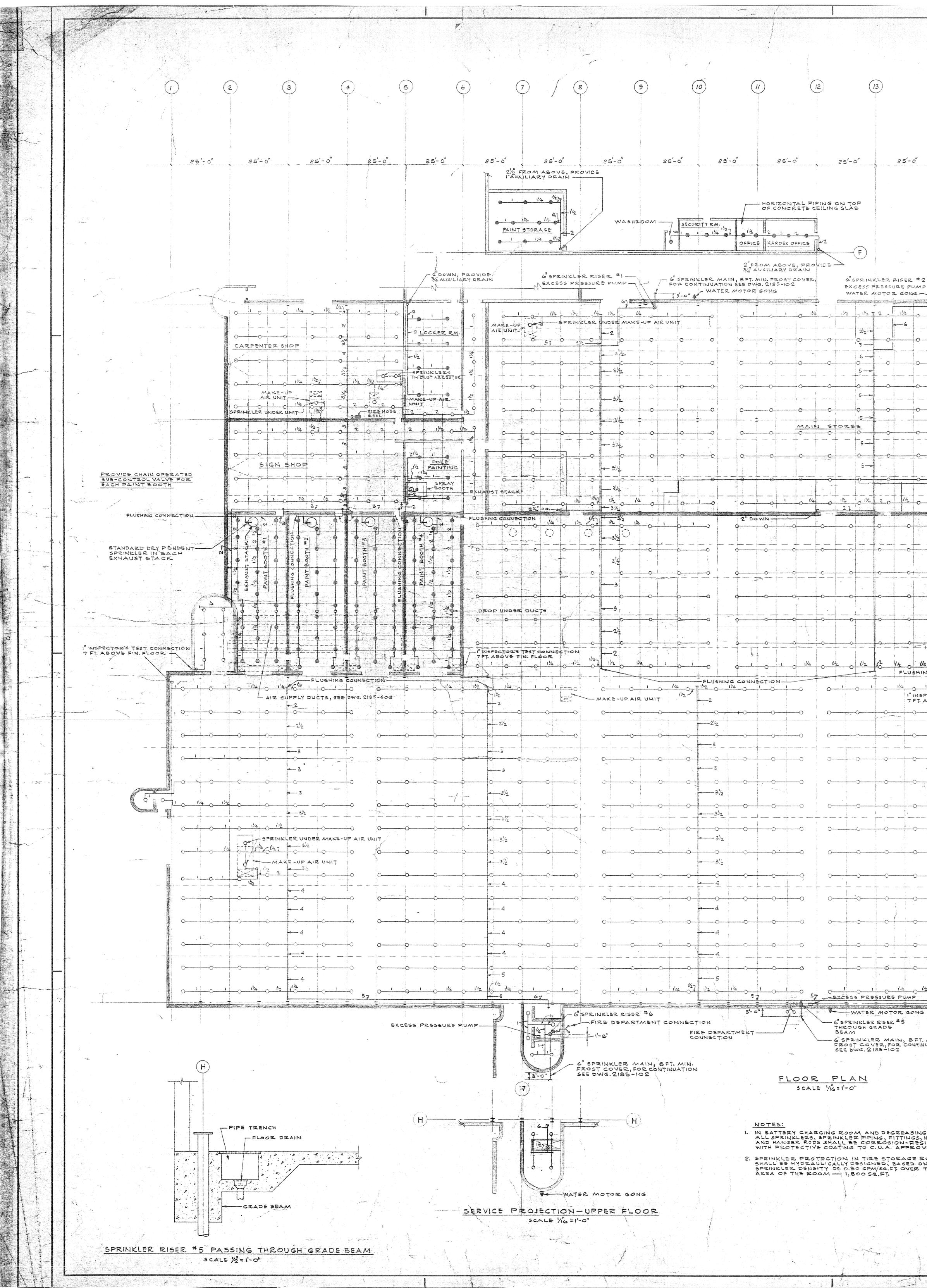
SCALE 14"=1'-0"

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HORIZONTAL PIPING ON TOP OF CONCRETE CEILING SLAB

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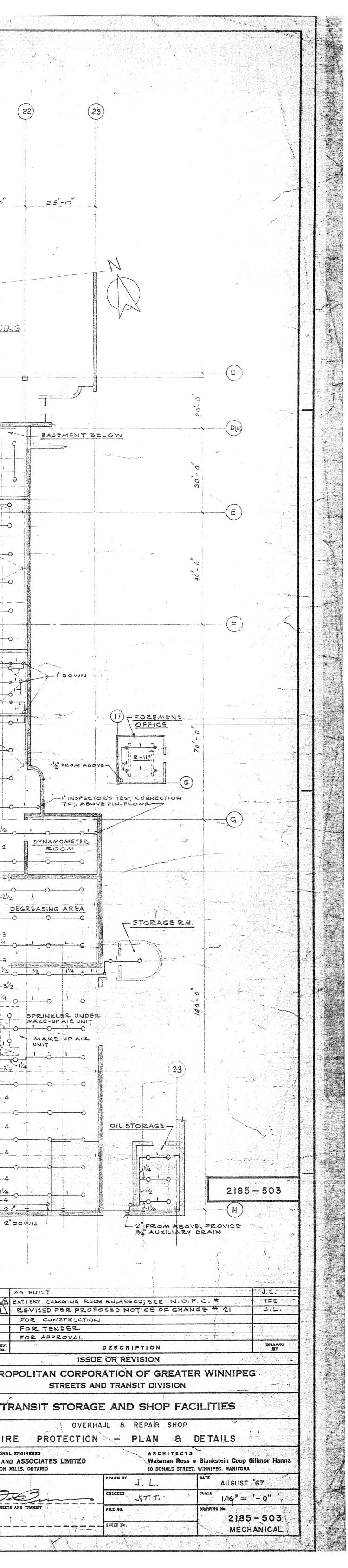
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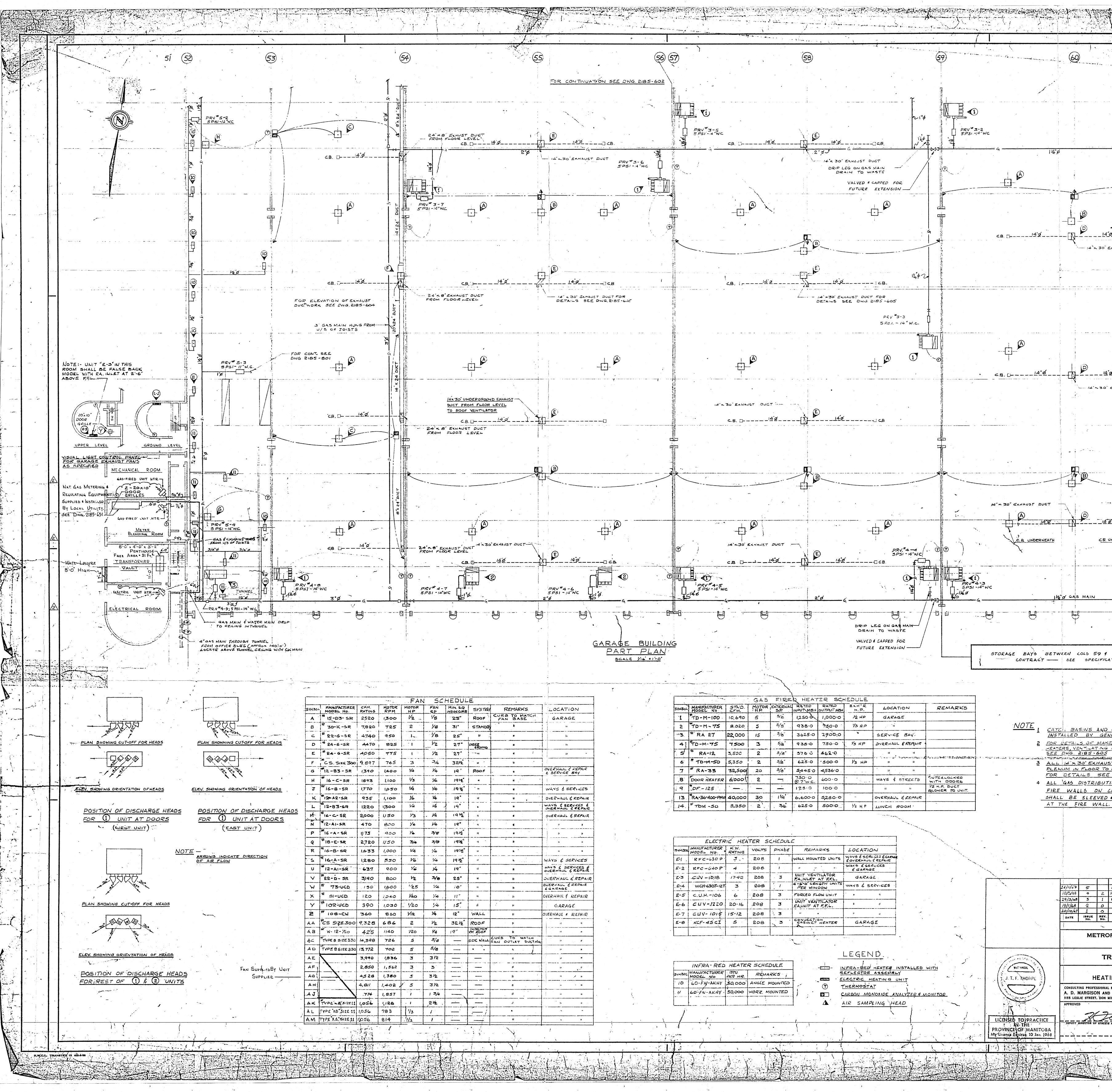
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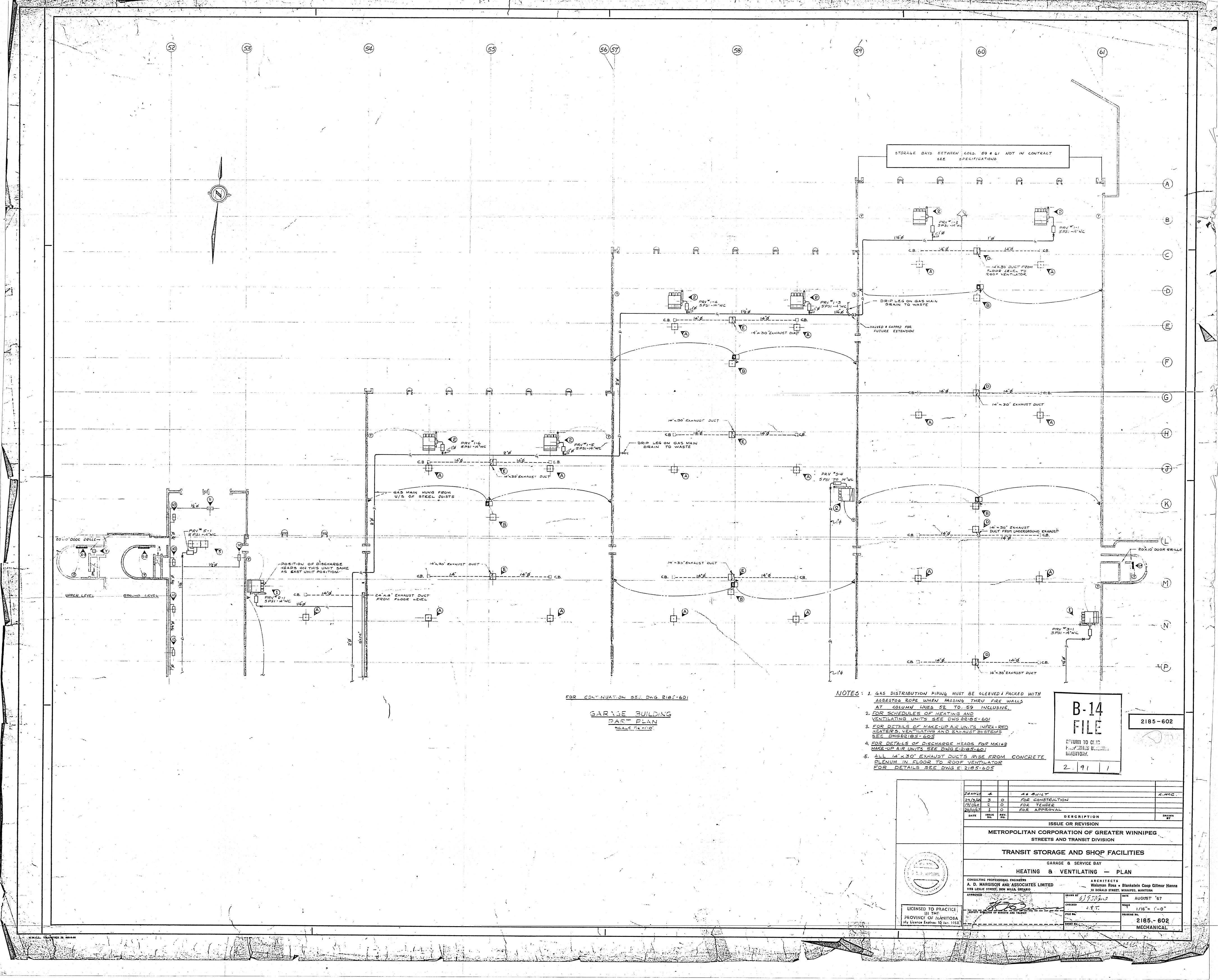
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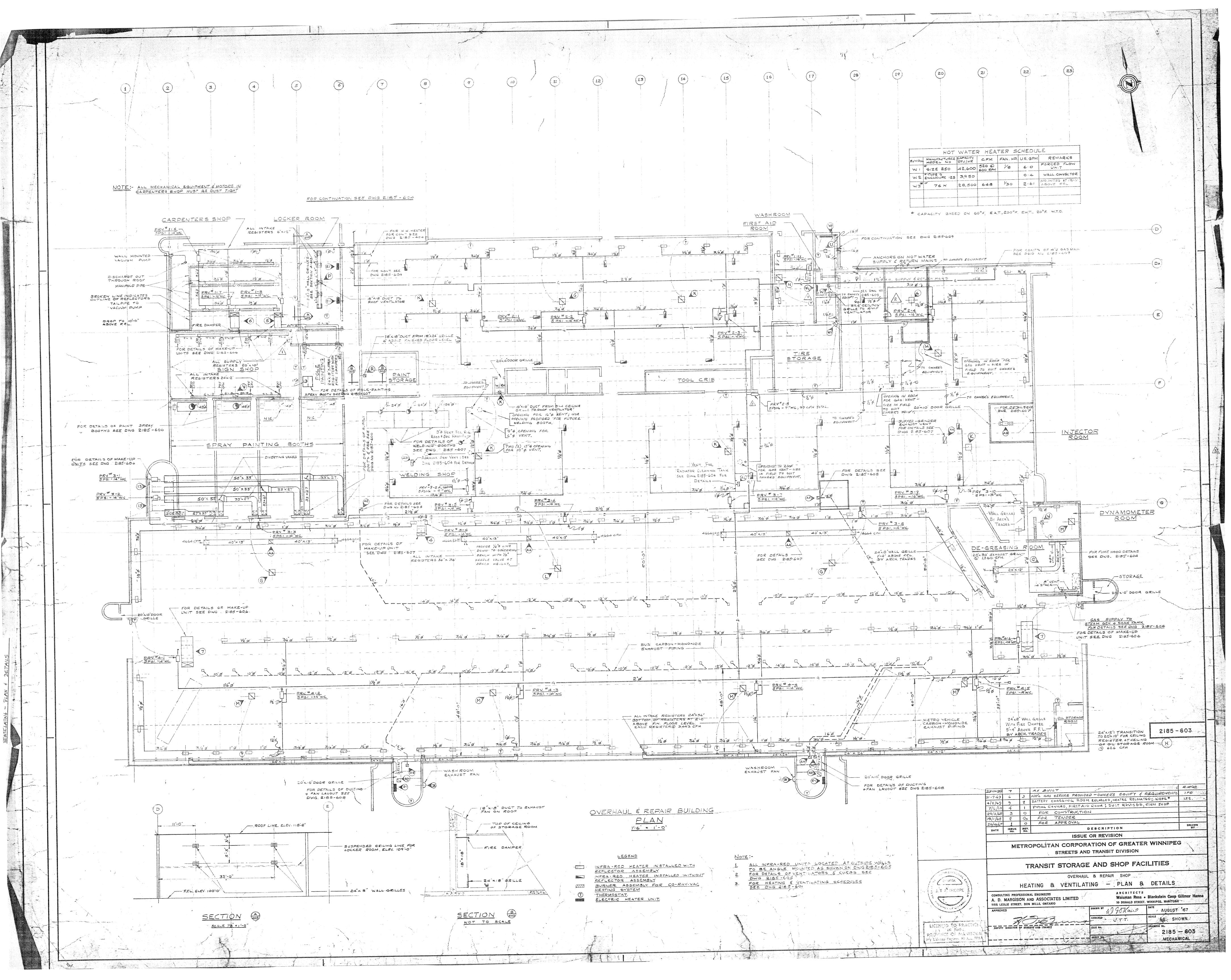
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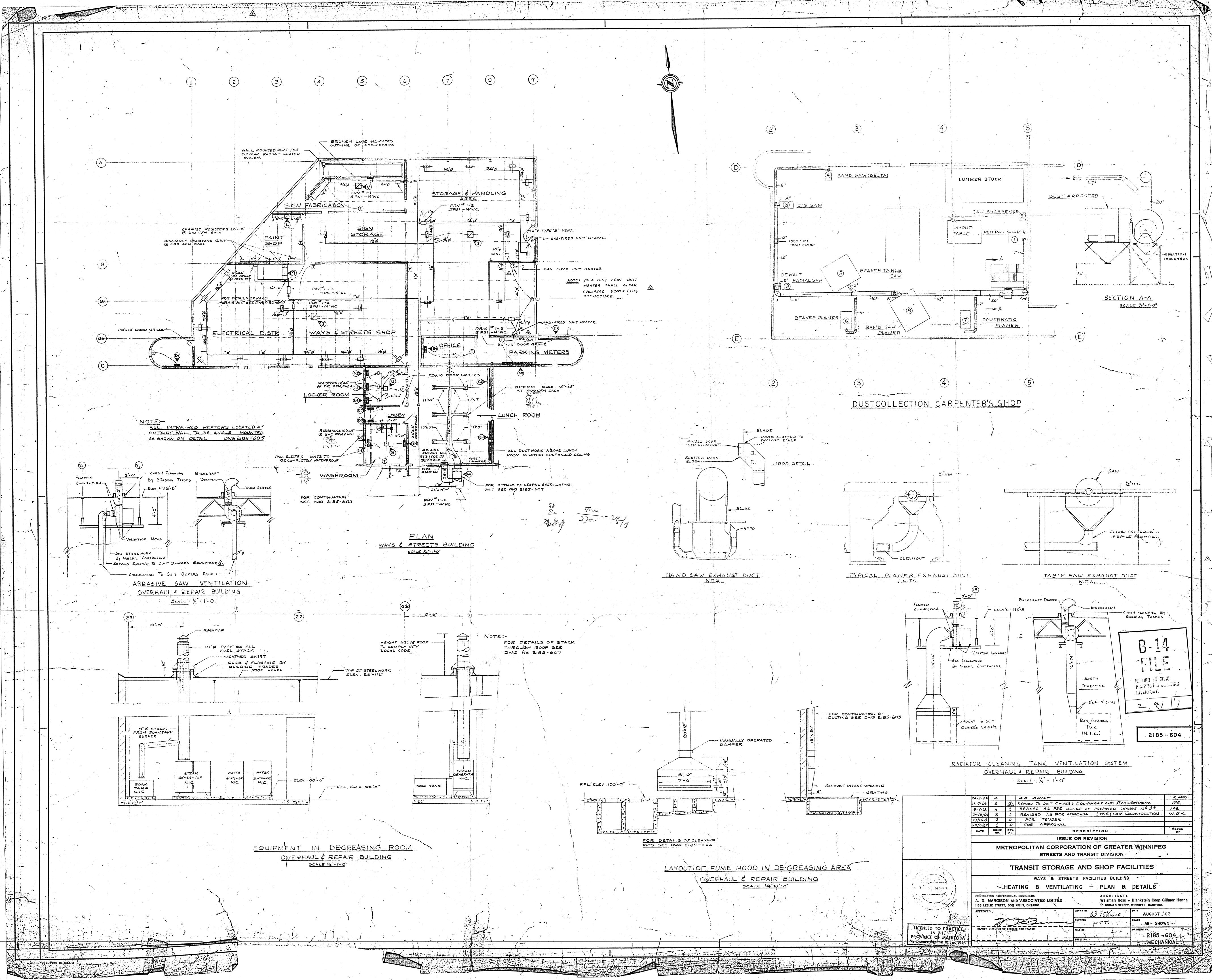
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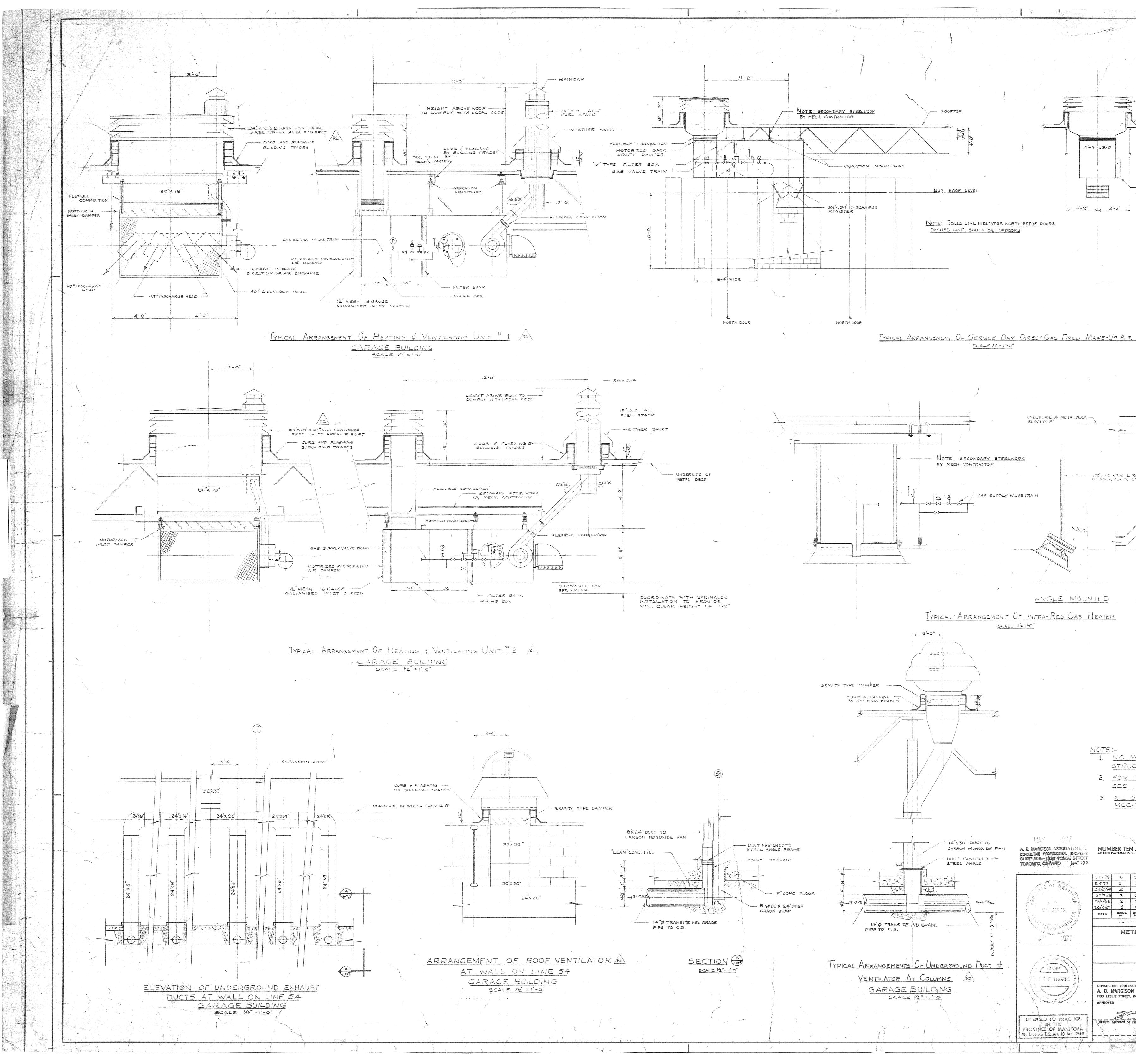
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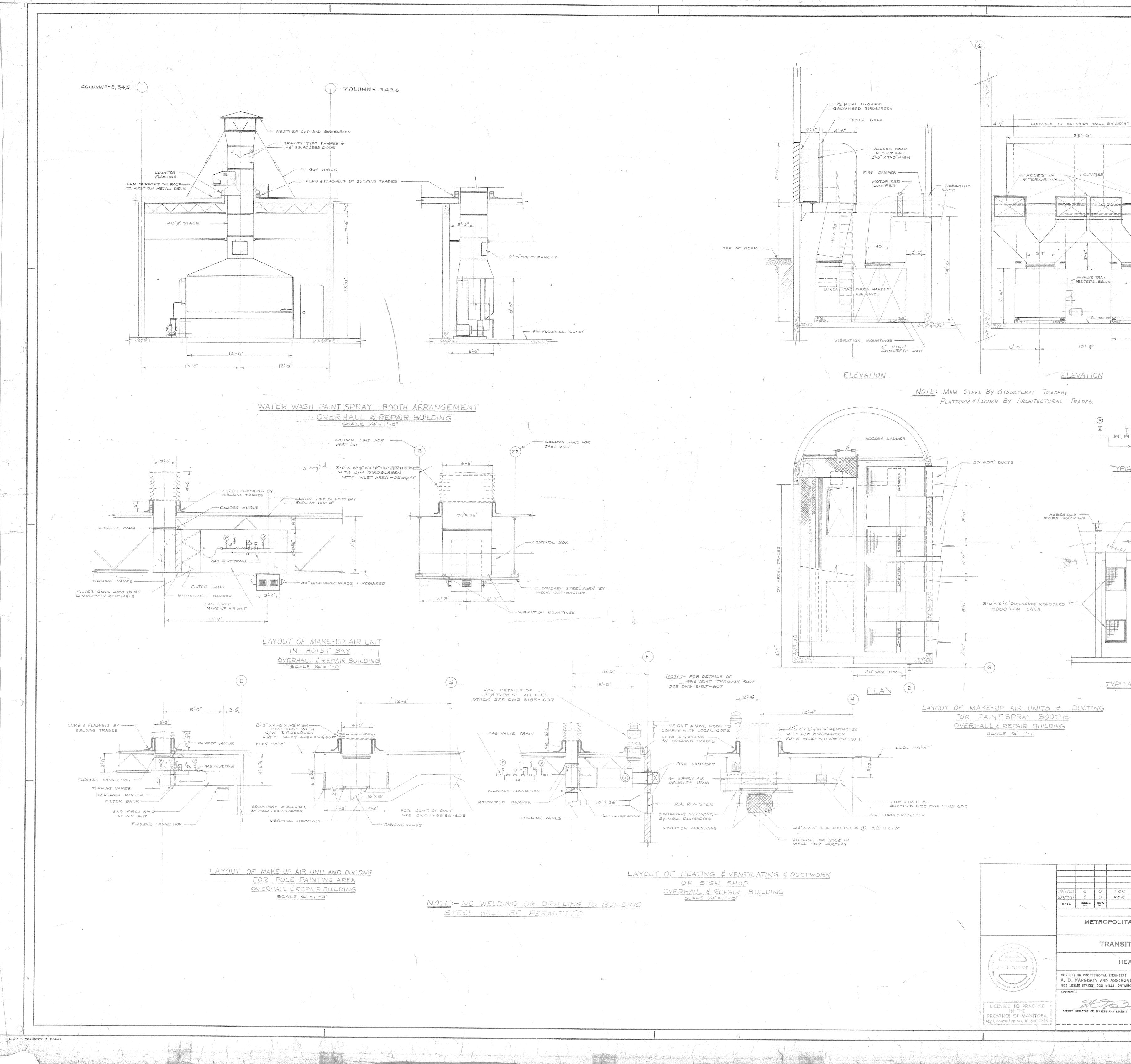




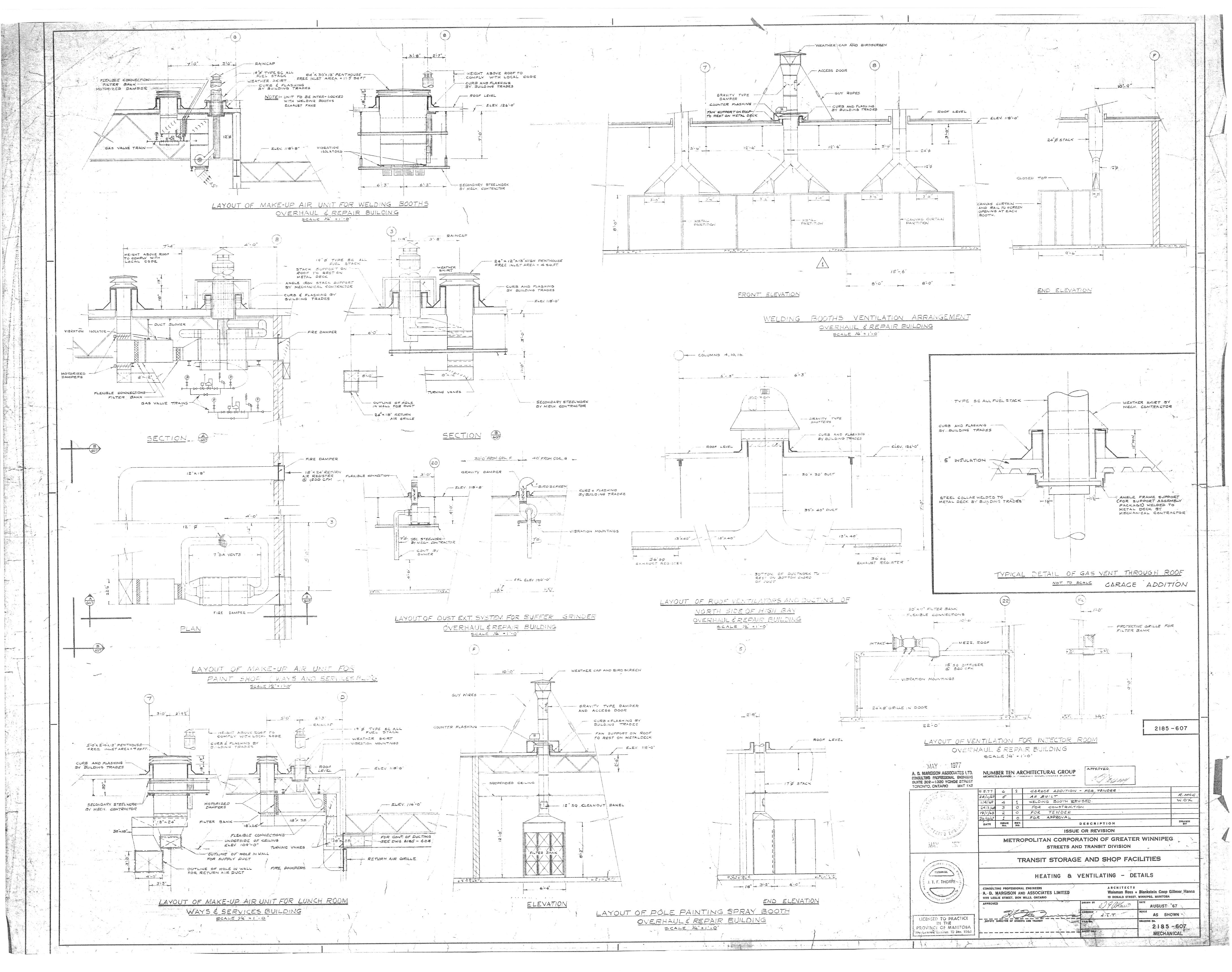


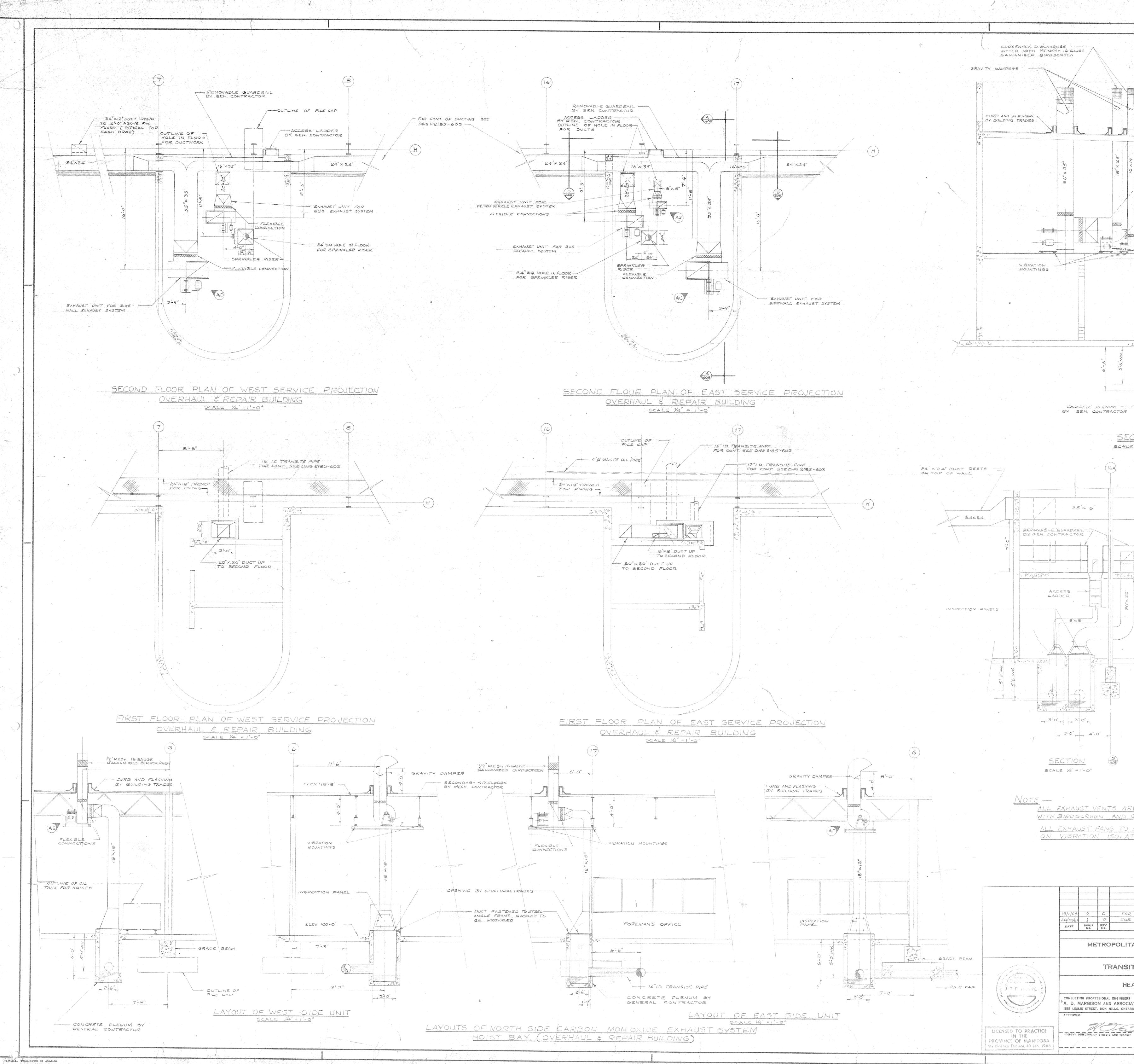


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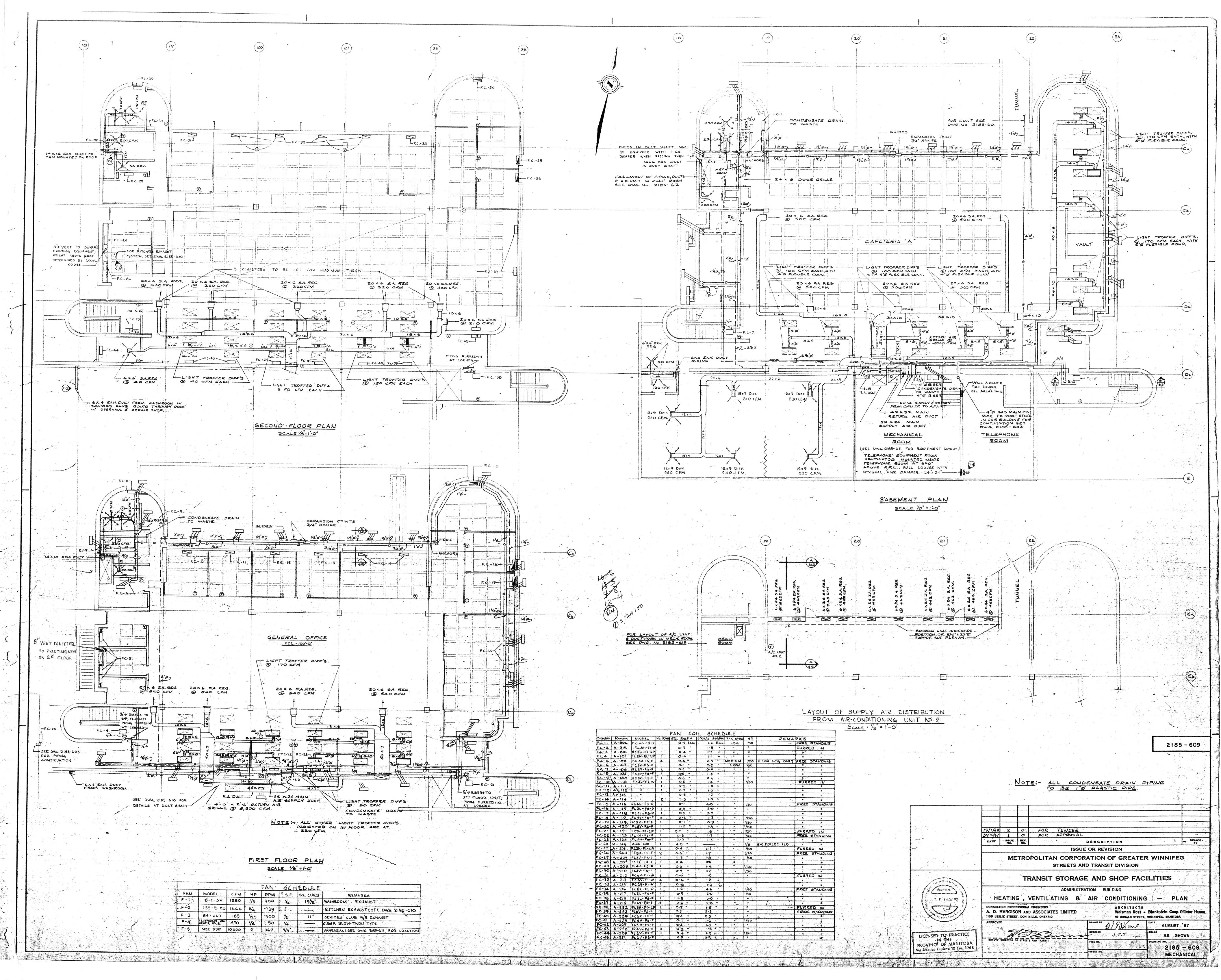


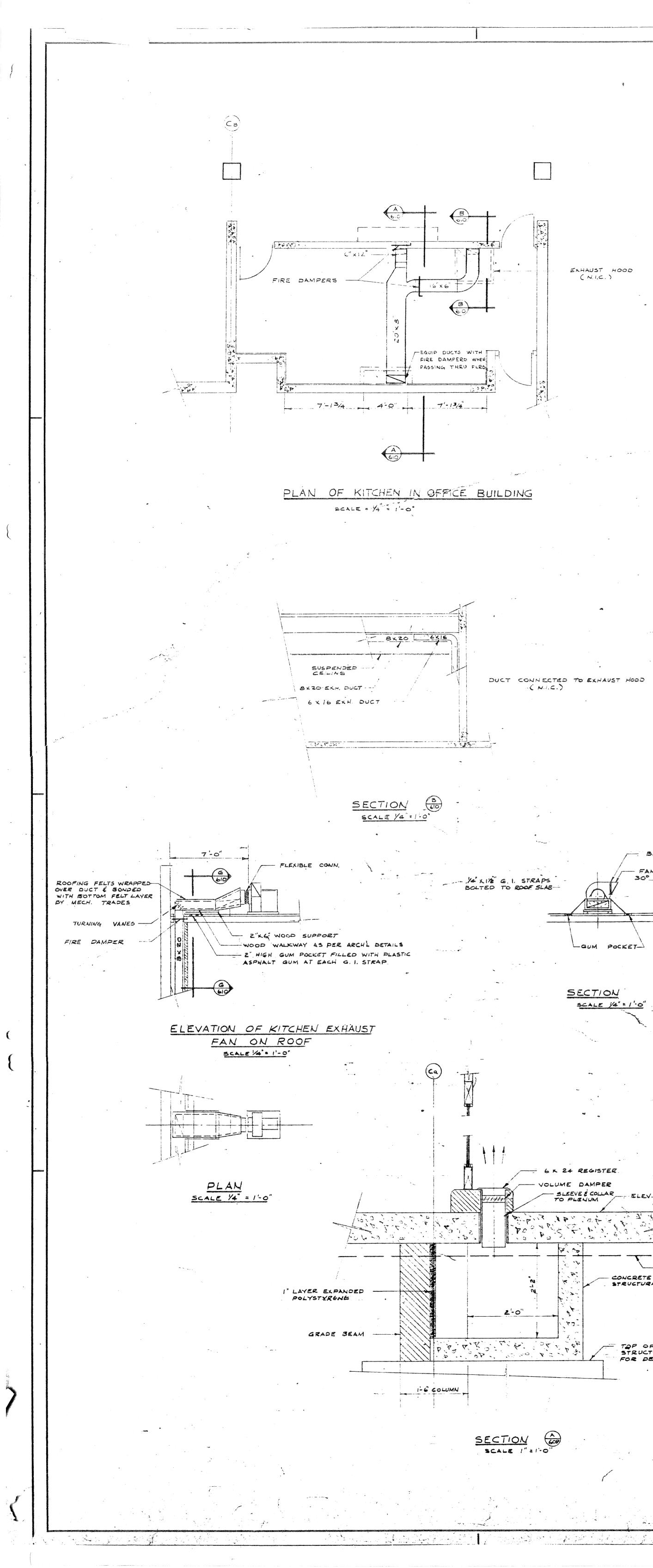


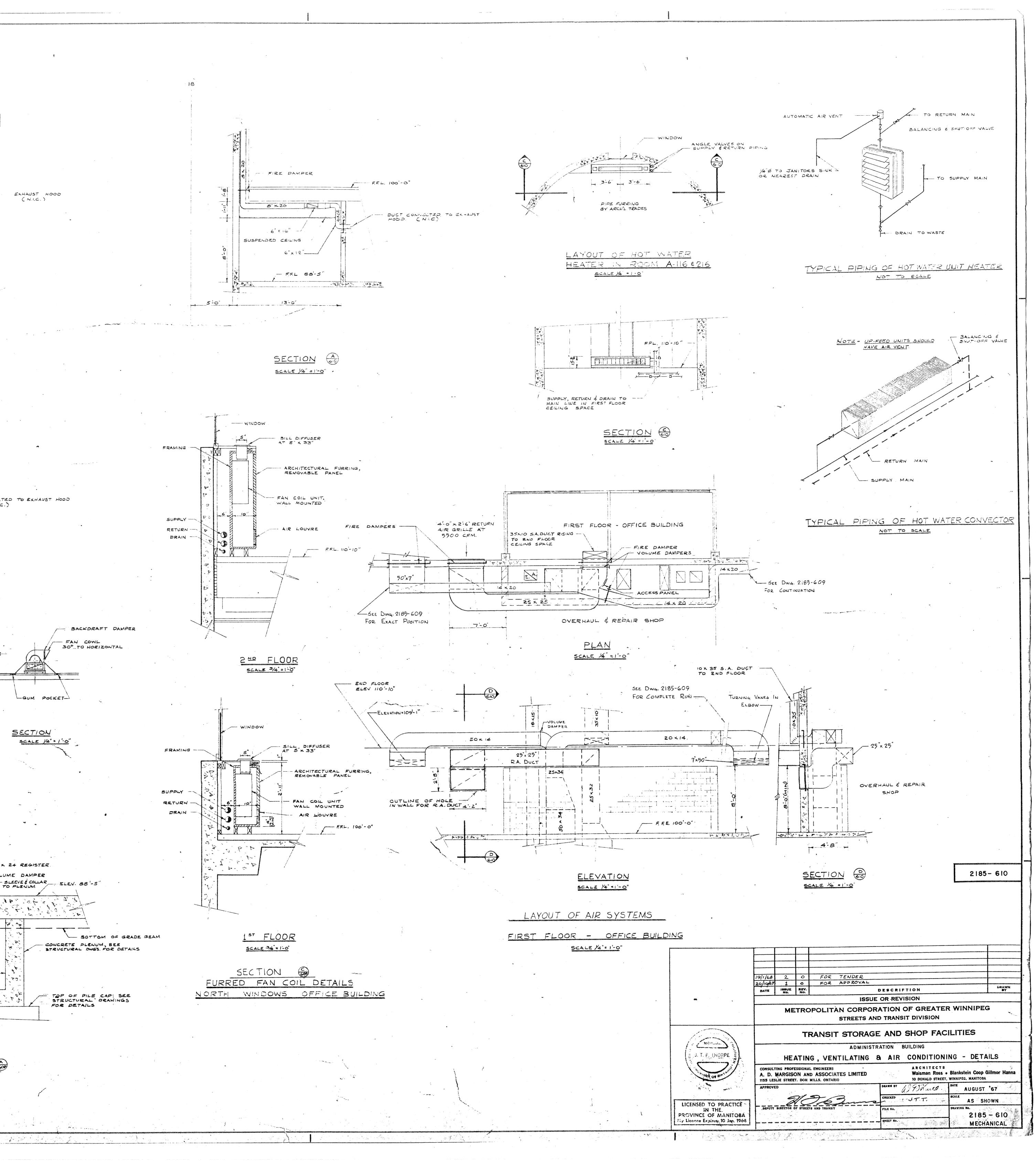
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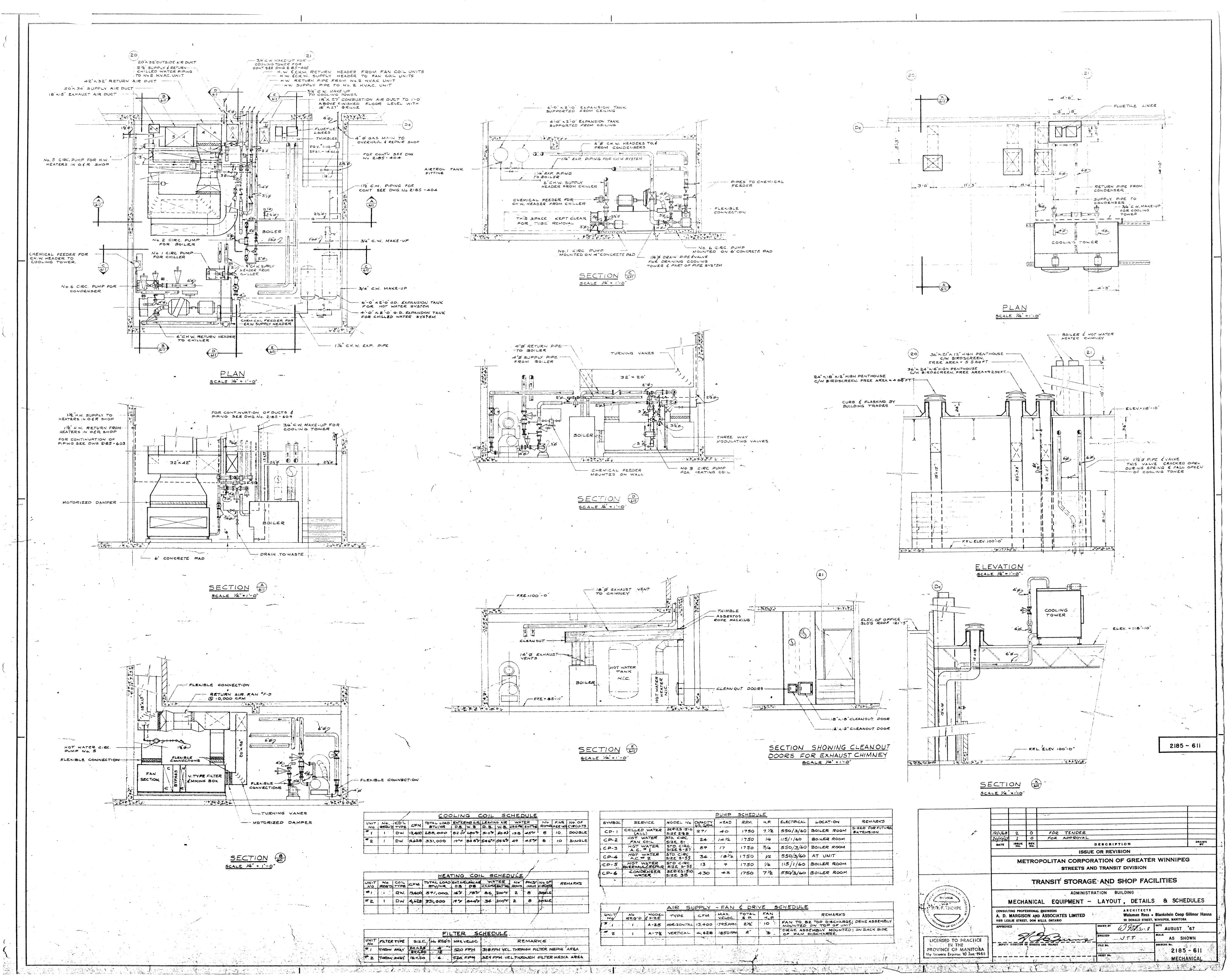
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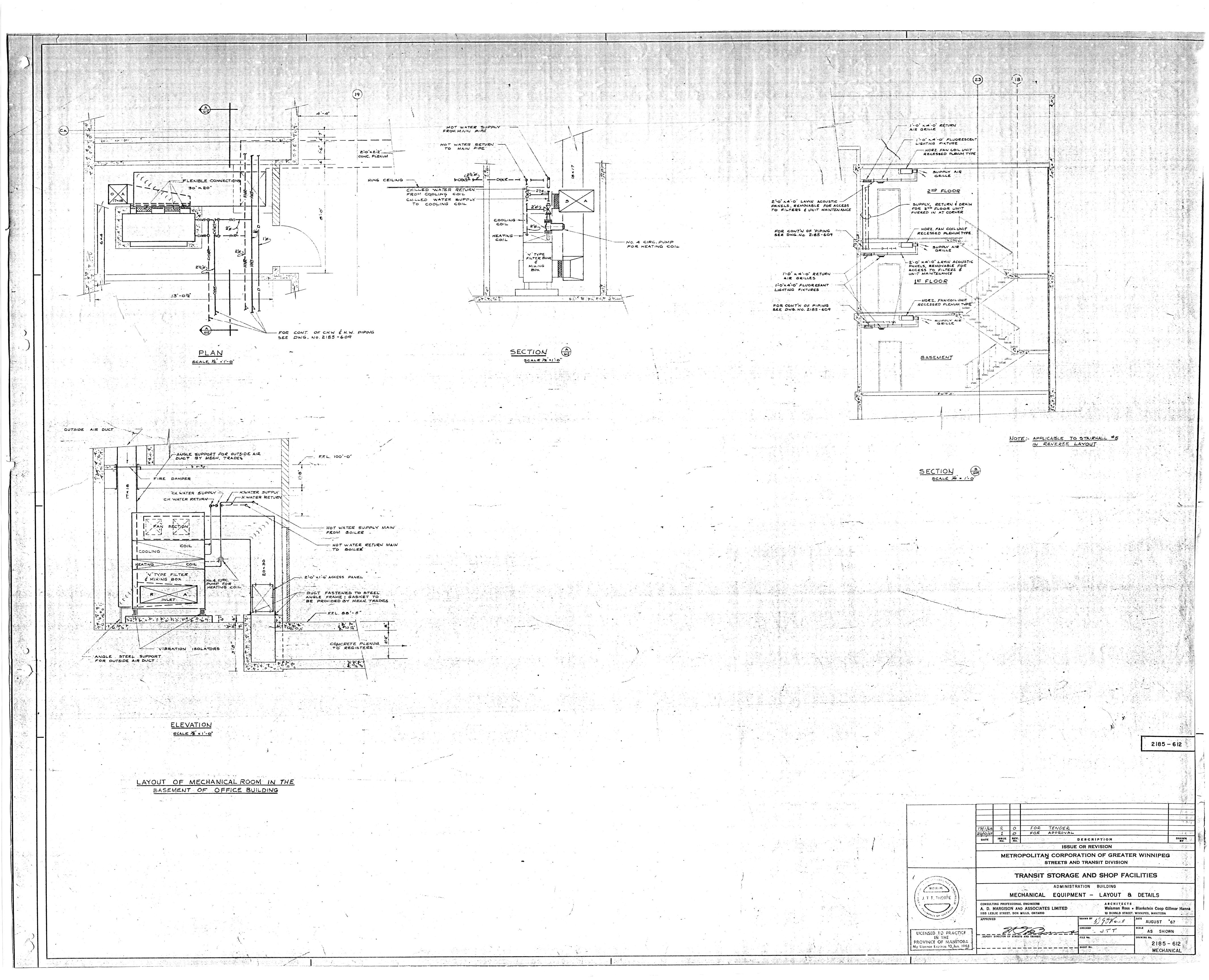
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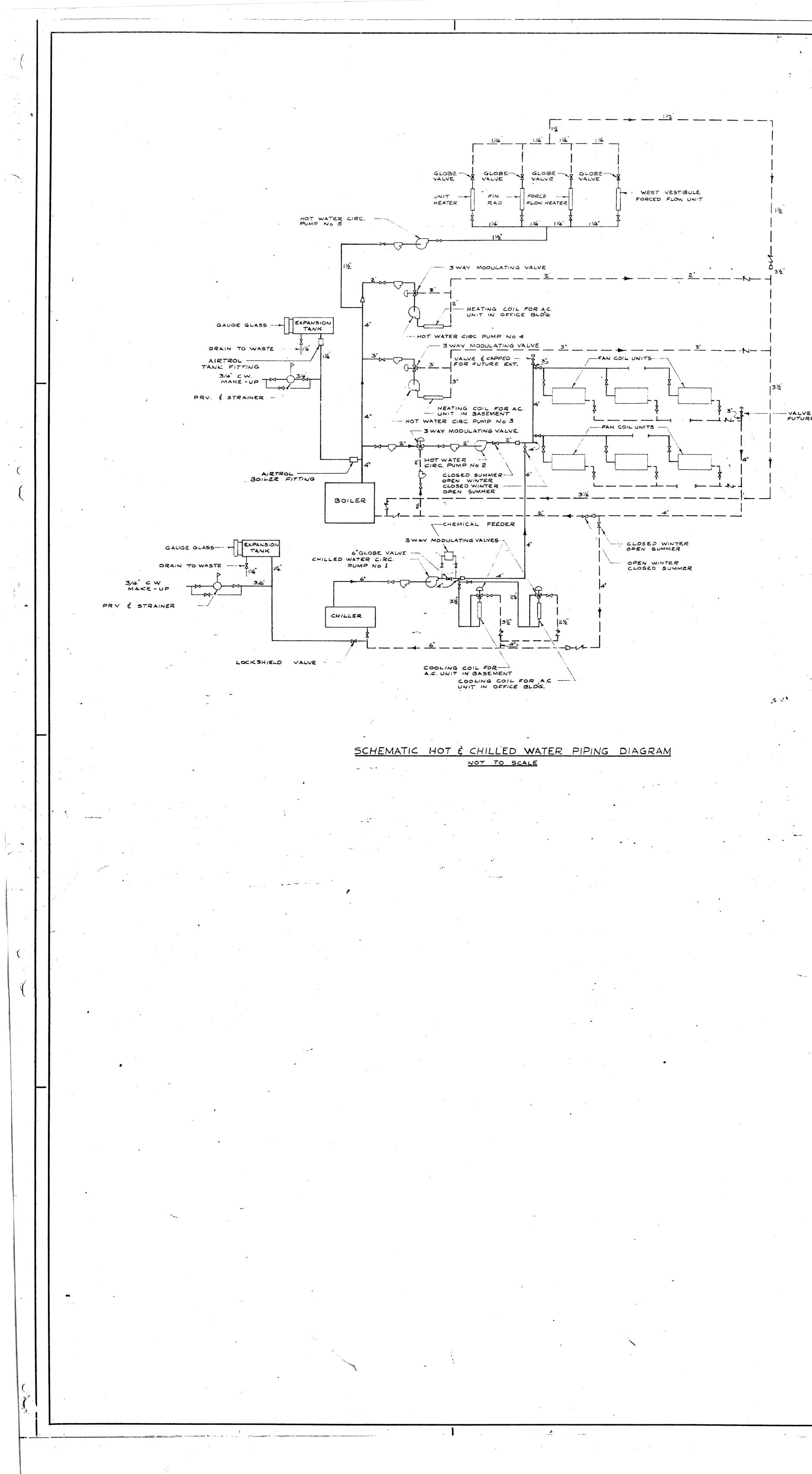






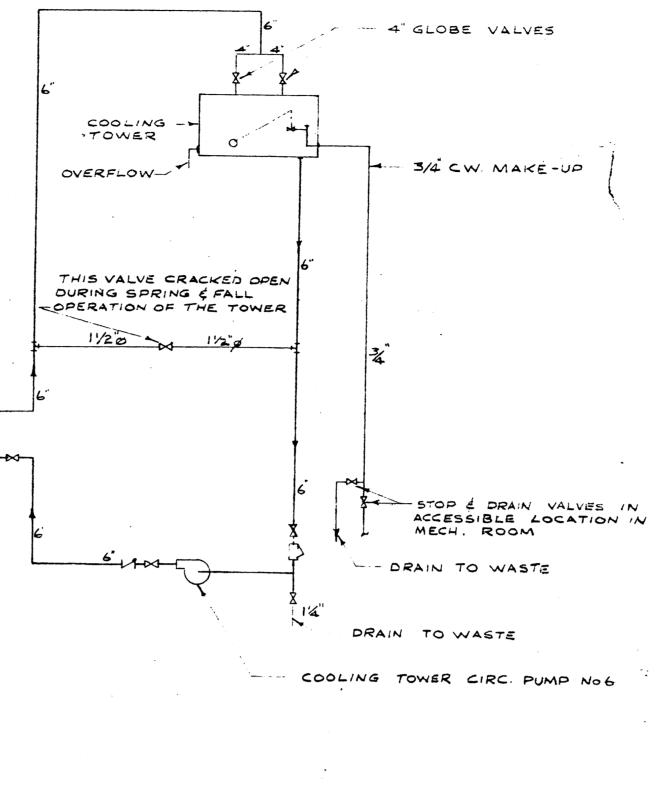






CHEMICAL FEEDER 6"GLOBE VALVE -CONDENSER

---- VALVE ÉCAPPED FOR FUTURE EXTENSION

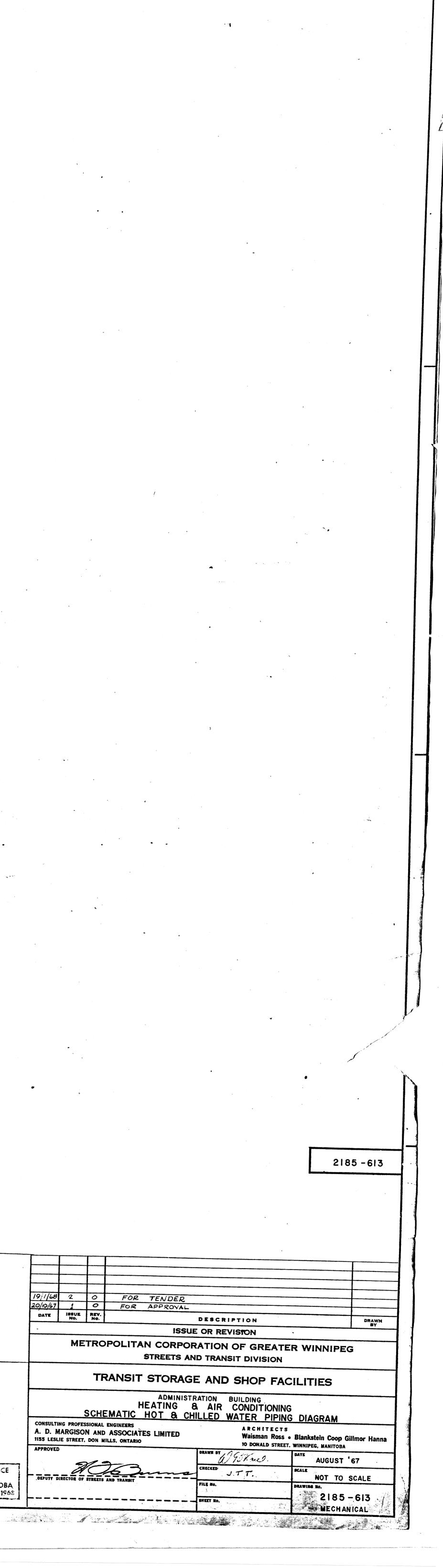


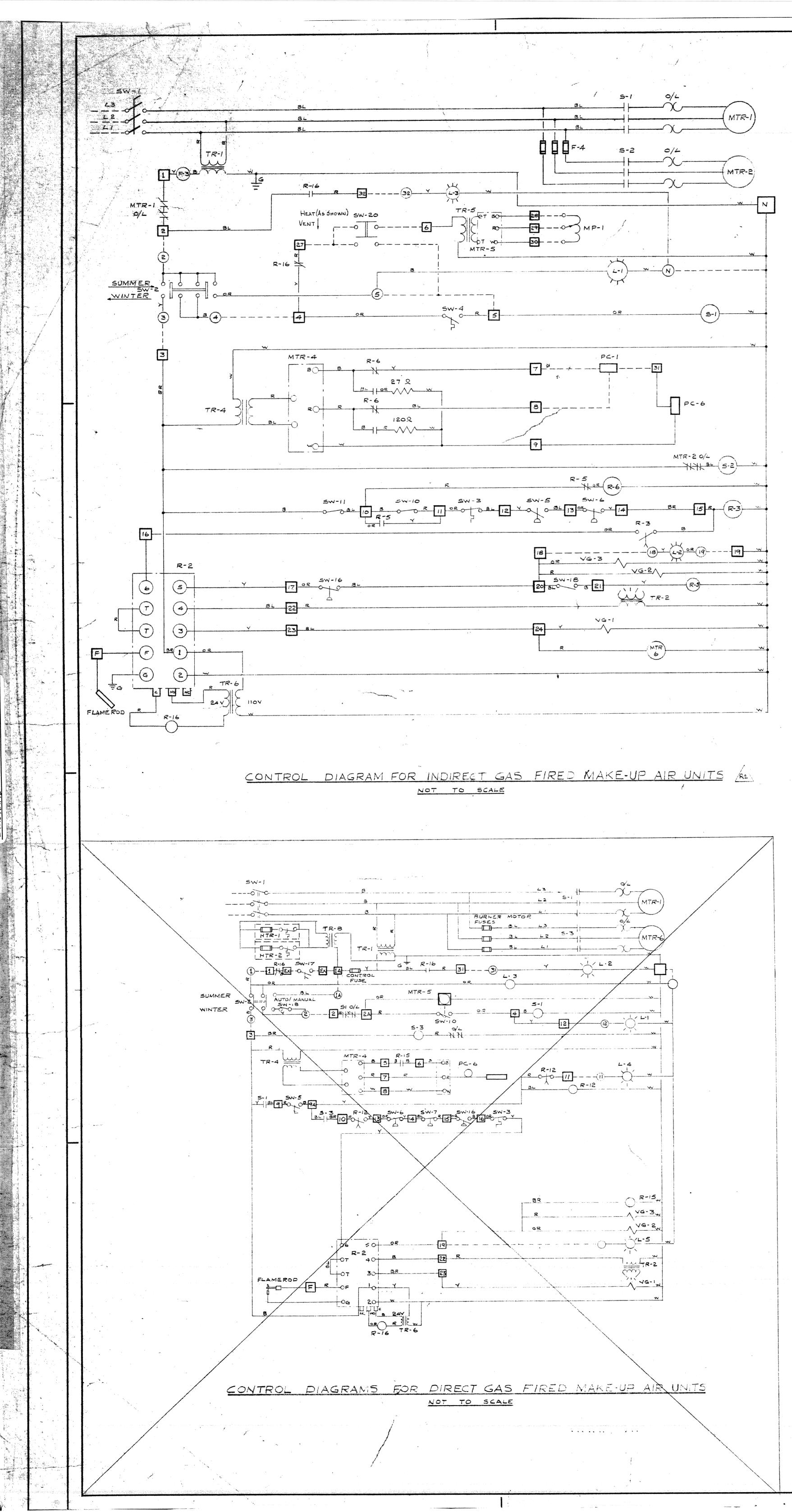
SCHEMATIC COOLING TOWER PIPING DIAGRAM

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19/1/68 2 0 FOR TENDER 20/10/67 1 0 FOR APPROVAL DATE ISSUE REV. No. No. A FOUTHART -----J. T. F. THORPE CONSULTING PROFESSIONAL ENGINEERS A. D. MARGISON AND ASSOCIATES LIMITED 1155 LESLIE STREET, DON MILLS, ONTARIO APPROVED LICENSED TO PRACTICE IN THE PROVINCE OF MANITOBA My Licence Expires: 10 Jan. 1968 DEPUTY DIRECTOR OF STREETS AND TRANSIT





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SYMBOL	COMPONENT
F-3	CONTROL FUSE
F-4	INDUCED DRAFT FUSE
MTR-1	MAIN SUPPLY FAN MOTOR
MTR-2 MTR-4	MODUTROL MOTOR
MTR-5	DAMPER MOTOR BURNER MOTOR
MTR-6	DURNER MOTOR
5-1	MAIN FAN MOTOR STARTER
5-6	
R-2	BURNER RELAY
R-3	PRE-PURGE RELAY
R-5	LOW FIRE RELAY
R-6	LOW FIRE HOLD RELAY
R -16	ALARM CIRCUIT RELAY
	, ROOM THERMOSTAT
PC-1	ROOM THERMOSTAT
PC-6	DUCTSTAT
F 6	
TR-1 TR-2	CONTROL TRANSFORMER
TR-4 TR-5	DAMPER MOTOR TRANSFORMER
TR-6	ALARM CIRCUIT TRANSFORMER
5W-1	MAIN DISCONNECT SWITCH
5-WE	FAN SELECTOR SWITCH
5W-3 5W-4	HIGH LIMIT SWITCH FAN SWITCH
5W-5	DRAFT PROVING SWITCH
5w-6	LO-GAS CUTOUT SWITCH
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SW -10 SW -11	AUXILIARY END SWITCH NO 1 AUXILIARY END SWITCH NO 2
5w-16	DIFFERENTIAL SWITCH
5W-18	LOW FIRE TEST SWITCH
SW-20	HEAT VENT SWITCH (LOCATE IN RU
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VG-I	PILOT GAS VALVE
VG-2	MAIN GAS VALVE
VG-2 VG-3	MAIN GAS VALVE AUXILIARY MAIN GAS VALVE
VG-3	
VG-3 L-1 L-2	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE)
VG-3 L-1	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN)
VG-3 L-1 L-2	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE)
VG-3 L-1 L-2 L-3	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED)
VG-3 L-1 L-2 L-3	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETER DENOTES WIRING BY OTHERS
VG-3 L-1 L-2 L-3	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETER DENOTES WIRING BY OTHERS DENOTES TERMINALS IN REMOTE CONTRO DENOTES TERMINALS IN REMOTE CONTRO DENOTES TERMINALS IN MAIN PANEL
VG-3 L-1 L-2 L-3	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETER DENOTES WIRING BY OTHERS DENOTES TERMINALS IN REMOTE CONTRA DENOTES TERMINALS IN REMOTE CONTRA DENOTES TERMINALS IN MAIN PANEL (BR-BROWN Y-YELLOW OR-ORA
VG-3 L-1 L-2 L-3 MP-1 B-BLACH BL-BLUE	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETER DENOTES WIRING BY OTHERS DENOTES TERMINALS IN REMOTE CONTRA DENOTES TERMINALS IN REMOTE CONTRA DENOTES TERMINALS IN MAIN PANEL (BR-BROWN Y-YELLOW OR-ORA W-WHITE R-RED VENT IDENTIFICATION FOR DIRE
VG-3 L-1 L-2 L-3 MP-1 B-BLACH BL-BLUE	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETER DENOTES WIRING BY OTHERS DENOTES TERMINALS IN REMOTE CONTRO DENOTES TERMINALS IN REMOTE CONTRO DENOTES TERMINALS IN MAIN PANEL (BR-BROWN Y-YELLOW OR-ORA W-WHITE R-RED NENT IDENTIFICATION FOR DIRE FIRED MAKE-UP AIR UNITS COMPONENT
VG-3 L-1 L-2 L-2 MP-1 B-BLACH BL-BLUE COMPON SYMBOL MTR-1	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETER DENOTES WIRING BY OTHERS DENOTES TERMINALS IN REMOTE CONTRI DENOTES TERMINALS IN REMOTE CONTRI DENOTES TERMINALS IN MAIN PANEL (BR-BROWN Y-YELLOW OR-ORA W-WHITE R-RED VENT IDENTIFICATION FOR DIRE FIRED MAKE-UP AIR UNITS COMPONENT MAIN SUPPLY FAN MOTOR
VG-3 L-1 L-2 L-3 MP-1 B-BLACH BL-BLUE COMPON SYMBOL MTR-1 MTR-4 MTR-6	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETER DENOTES WIRING BY OTHERS DENOTES TERMINALS IN REMOTE CONTRO DENOTES TERMINALS IN REMOTE CONTRO DENOTES TERMINALS IN MAIN PANEL (BR-BROWN Y-YELLOW OR-ORA W-WHITE R-RED NENT IDENTIFICATION FOR DIRE FIRED MAKE-UP AIR UNITS COMPONENT MAIN SUPPLY FAN MOTOR MODUTROL MOTOR DAMPER MOTOR
VG-3 L-1 L-2 L-2 MP-1 B-BLACH BL-BLUE COMPON SYMBOL MTR-1 MTR-4	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETER DENOTES WIRING BY OTHERS DENOTES TERMINALS IN REMOTE CONTRO DENOTES TERMINALS IN REMOTE CONTRO DENOTES TERMINALS IN MAIN PANEL (BR-BROWN Y-YELLOW OR-ORA W-WHITE R-RED NENT IDENTIFICATION FOR DIRE FIRED MAKE-UP AIR UNITS COMPONENT MAIN SUPPLY FAN MOTOR MODUTROL MOTOR DAMPER MOTOR
VG-3 L-1 L-2 L-3 MP-1 B-BLACH BL-BLUE COMPON SYMBOL MTR-1 MTR-4 MTR-6 MTR-6 MTR-6 S-1	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETER DENOTES WIRING BY OTHERS DENOTES WIRING BY OTHERS DENOTES TERMINALS IN REMOTE CONTRI DENOTES TERMINALS IN MAIN PANEL (BR-BROWN Y-YELLOW OR-ORA W-WHITE R-RED VENT IDENTIFICATION FOR DIRE FIRED MAKE-UP AIR UNITS COMPONENT MAIN SUPPLY FAN MOTOR DAMPER MOTOR DAMPER MOTOR DAMPER MOTOR MAIN FAN MOTOR STARTER
VG-3 L-1 L-2 L-3 MP-1 B-BLACH BL-BLUE COMPON SYMBOL MTR-1 MTR-4 MTR-6 MTR-6	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETER DENOTES WIRING BY OTHERS DENOTES TERMINALS IN REMOTE CONTRI DENOTES TERMINALS IN REMOTE CONTRI DENOTES TERMINALS IN MAIN PANEL (BR-BROWN Y-YELLOW OR-ORA W-WHITE R-RED NENT IDENTIFICATION FOR DIRE FIRED MAKE-UP AIR UNITS COMPONENT MAIN SUPPLY FAN MOTOR MODUTROL MOTOR DAMPER MOTOR PREMIX BURNER MOTOR
VG-3 L-1 L-2 L-3 MP-1 B-BLACH BL-BLUE COMPON SYMBOL MTR-1 MTR-4 MTR-6 MTR-6 MTR-6 S-1	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETER DENOTES WIRING BY OTHERS DENOTES WIRING BY OTHERS DENOTES TERMINALS IN REMOTE CONTRI DENOTES TERMINALS IN MAIN PANEL (BR-BROWN Y-YELLOW OR-ORA W-WHITE R-RED VENT IDENTIFICATION FOR DIRE FIRED MAKE-UP AIR UNITS COMPONENT MAIN SUPPLY FAN MOTOR DAMPER MOTOR DAMPER MOTOR DAMPER MOTOR MAIN FAN MOTOR STARTER
VG-3 $L-1$ $L-2$ $L-3$ $MP-1$ $B-BLACH$ $BL-BLUE$ $COMPON$ $SYMBOL$ $MTR-1$ $MTR-4$ $MTR-6$ $MTR-6$ $MTR-6$ $R-2$ $R-2$ $R-2$	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETER DENOTES WIRING BY OTHERS DENOTES TERMINALS IN REMOTE CONTRI DENOTES TERMINALS IN REMOTE CONTRI DENOTES TERMINALS IN MAIN PANEL (BR-BROWN Y-YELLOW OR-ORA W - WHITE R-RED VENT IDENTIFICATION FOR DIRE FIRED MAKE-UP AIR UNITS COMPONENT MAIN SUPPLY FAN MOTOR MODUTROL MOTOR DAMPER MOTOR PREMIX BURNER MOTOR MAIN FAN MOTOR STARTER BURNER RELAY PURGING TIMING RELAY
VG-3 $L-1$ $L-2$ $L-3$ $MP-1$ $B-BLACH$ $BL - BLUE$ $COMPON$ $SYMBOL$ $MTR-1$ $MTR-4$ $MTR-6$ $MTR-6$ $MTR-6$ $R-2$ $R-2$	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETER DENOTES WIRING BY OTHERS DENOTES TERMINALS IN REMOTE CONTRI DENOTES TERMINALS IN REMOTE CONTRI DENOTES TERMINALS IN MAIN PANEL (BR-BROWN Y-YELLOW OR-ORA W-WHITE R-RED NENT IDENTIFICATION FOR DIRE FIRED MAKE-UP AIR UNITS COMPONENT MAIN SUPPLY FAN MOTOR MODUTROL MOTOR DAMPER MOTOR PREMIX BURNER MOTOR MAIN FAN MOTOR STARTER BURNER RELAY
VG-3 $L-1$ $L-2$ $L-3$ $MP-1$ $B-BLACH$ $B-BLACH$ $BL-BLUE$ $COMPOIN$ $SYMBOL$ $MTR-1$ $MTR-6$ $MTR-6$ $MTR-6$ $MTR-6$ $R-2$ $R-2$ $R-2$ $R-2$ $R-2$ $R-2$ $R-2$	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETER DENOTES WIRING BY OTHERS DENOTES WIRING BY OTHERS DENOTES TERMINALS IN REMOTE CONTRI DENOTES TERMINALS IN MAIN PANEL (BR-BROWN Y - YELLOW OR - ORA W - WHITE R - RED VENT IDENTIFICATION FOR DIRE FIRED MAKE-UP AIR UNITS COMPONENT MAIN SUPPLY FAN MOTOR MODUTROL MOTOR DAMPER MOTOR PREMIX BURNER MOTOR MAIN FAN MOTOR STARTER BURNER RELAY PURGING TIMING RELAY ALARM CIRCUIT RELAY
VG-3 $L-1$ $L-2$ $L-3$ $MP-1$ $B-BLACH$ $BL - BLUE$ $COMPON$ $SYMBOL$ $MTR-1$ $MTR-4$ $MTR-6$ $MTR-6$ $MTR-6$ $R-2$ $R-2$ $R-2$ $R-2$ $R-15$	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETER DENOTES WIRING BY OTHERS DENOTES TERMINALS IN REMOTE CONTRI DENOTES TERMINALS IN REMOTE CONTRI DENOTES TERMINALS IN MAIN PANEL (BR-BROWN Y-YELLOW OR-ORA W - WHITE R - RED NENT IDENTIFICATION FOR DIRE FIRED MAKE-UP AIR UNITS COMPONENT MAIN SUPPLY FAN MOTOR MODUTROL MOTOR DAMPER MOTOR PREMIX BURNER MOTOR MAIN FAN MOTOR STARTER BURNER RELAY PURGING TIMING RELAY LOW FIRE HOLD RELAY
VG-3 $L-1$ $L-2$ $L-3$ $MP-1$ $B-BLACH$ $MTR-1$ $MTR-1$ $MTR-6$ $MTR-6$ $MTR-6$ $S-1$ $S-1$ $S-2$ $R-2$ $R-2$ $R-2$ $R-2$ $R-2$ $R-2$ $R-2$ $R-2$ $R-2$ <th>AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETERS DENOTES WIRING BY OTHERS DENOTES TERMINALS IN REMOTE CONTRI- DENOTES TERMINALS IN REMOTE CONTRI- DENOTES TERMINALS IN MAIN PANEL (BR - BROWN Y - YELLOW OR - ORA W - WHITE R - RED NENT IDENTIFICATION FOR DIRE FIRED MAKE-UP AIR UNITS COMPONENT MAIN SUPPLY FAN MOTOR MODUTROL MOTOR DAMPER MOTOR PREMIX BURNER MOTOR MAIN FAN MOTOR STARTER BURNER RELAY BURNER RELAY ALARM CIRCUIT RELAY AIR DISCHARGE THERMOSTAT PILOT GAS VALVE</th>	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETERS DENOTES WIRING BY OTHERS DENOTES TERMINALS IN REMOTE CONTRI- DENOTES TERMINALS IN REMOTE CONTRI- DENOTES TERMINALS IN MAIN PANEL (BR - BROWN Y - YELLOW OR - ORA W - WHITE R - RED NENT IDENTIFICATION FOR DIRE FIRED MAKE-UP AIR UNITS COMPONENT MAIN SUPPLY FAN MOTOR MODUTROL MOTOR DAMPER MOTOR PREMIX BURNER MOTOR MAIN FAN MOTOR STARTER BURNER RELAY BURNER RELAY ALARM CIRCUIT RELAY AIR DISCHARGE THERMOSTAT PILOT GAS VALVE
VG-3 $L-1$ $L-2$ $L-3$ $MP-1$ $B-BLACH$ $B-BLACH$ $BL-BLUE$ $COMPOIN SYMBOL MTR-1 MTR-6 MTR-6 S-1 S-1 S-2 R-2 R-2$	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETER DENOTES WIRING BY OTHERS DENOTES WIRING BY OTHERS DENOTES TERMINALS IN REMOTE CONTRI- DENOTES TERMINALS IN MAIN PANEL C BR - BROWN Y - YELLOW OR - ORA W - WHITE R - RED NENT IDENTIFICATION FOR DIRE FIRED MAKE-UP AIR UNITS COMPONENT MAIN SUPPLY FAN MOTOR MODUTROL MOTOR DAMPER MOTOR DAMPER MOTOR DAMPER MOTOR DAMPER MOTOR MAIN FAN MOTOR STARTER BURNER RELAY PURGING TIMING RELAY ALARM CIRCUIT RELAY AIR DISCHARGE THERMOSTAT
VG-3 $L-1$ $L-2$ $L-3$ $MP-1$ $B-BLACH$ $MTR-1$ $MTR-1$ $MTR-6$ $MTR-6$ $MTR-6$ $R-2$	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETER DENOTES WIRING BY OTHERS DENOTES TERMINALS IN REMOTE CONTRI- DENOTES TERMINALS IN REMOTE CONTRI- DENOTES TERMINALS IN MAIN PANEL (BR-BROWN Y - YELLOW OR - ORA W - WHITE R - RED WENT IDENTIFICATION FOR DIRE FIRED MAKE-UP AIR UNITS COMPONENT MAIN SUPPLY FAN MOTOR MODUTROL MOTOR DAMPER MOTOR PREMIX BURNER MOTOR MODUTROL MOTOR DAMPER MOTOR STARTER BURNER MOTOR STARTER BURNER RELAY PURGING TIMING RELAY ALARM CIRCUIT RELAY ALARM CIRCUIT RELAY PILOT GAS VALVE MAIN GAS VALVE MAIN GAS VALVE AUXILARY MAIN GAS VALVE
VG-3 L-1 L-2 L-3 MP-1 B-BLACH BL-BLUE COMPON SYMBOL MTR-1 MTR-4 MTR-6 MTR-6 S-1 S-2 R-2 R-3 PC-6 VG-1 VG-2	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETERS DENOTES WIRING BY OTHERS DENOTES TERMINALS IN REMOTE CONTRI- DENOTES TERMINALS IN REMOTE CONTRI- DENOTES TERMINALS IN MAIN PANEL C BR - BROWN Y - YELLOW OR - ORA W - WHITE R - RED WENT IDENTIFICATION FOR DIRE FIRED MAKE-UP AIR UNITS COMPONENT MAIN SUPPLY FAN MOTOR MODUTROL MOTOR DAMPER MOTOR DAMPER MOTOR PREMIX BURNER MOTOR MAIN FAN MOTOR STARTER BURNER RELAY PURGING TIMING RELAY ALARM CIRCUIT RELAY AIR DISCHARGE THERMOSTAT PILOT GAS VALVE MAIN GAS VALVE
VG-3 L-1 L-2 L-3 MP-1 B-BLACK BL-BLUE COMPON SYMBOL MTR-1 MTR-4 MTR-6 MTR-6 S-1 S-2 R-2 R-2 R-6 VG-1 VG-2 VG-3 TR-1 TR-2 TR-4	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETER DENOTES WIRING BY OTHERS DENOTES WIRING BY OTHERS DENOTES TERMINALS IN REMOTE CONTR DENOTES TERMINALS IN MAIN PANEL C BR-BROWN Y-YELLOW OR-ORA W - WHITE R-RED WENT IDENTIFICATION FOR DIRE FIRED MAKE-UP AIR UNITS COMPONENT MAIN SUPPLY FAN MOTOR MODUTROL MOTOR DAMPER MOTOR DAMPER MOTOR PREMIX BURNER MOTOR MAIN FAN MOTOR STARTER BURNER RELAY PURGING TIMING RELAY LOW FIRE HOLD RELAY ALARM CIRCUIT RELAY ALARM CIRCUIT RELAY PILOT GAS VALVE MAIN GAS VALVE MAIN GAS VALVE AUXILARY MAIN GAS VALVE CONTROL VOLTAGE TRANSFORMER MODUTROL MOTOR TRANSFORMER MODUTROL MOTOR TRANSFORMER
VG-3 L-1 L-2 L-3 MP-1 B-BLACH BL-BLUE COMPON SYMBOL MTR-1 MTR-6 MTR-6 MTR-6 MTR-6 MTR-6 MTR-6 MTR-7 MTR-6 MTR-6 MTR-6 MTR-7 MTR-6 MTR-6 MTR-7 MTR-7 MTR-8 S-1 S-2 R-2 R-3 PC-6 VG-1 VG-2 VG-3 TR-1 TR-2	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETER DENOTES WIRING BY OTHERS DENOTES TERMINALS IN REMOTE CONTRI- DENOTES TERMINALS IN REMOTE CONTRI- DENOTES TERMINALS IN MAIN PANEL (BR-BROWN Y-YELLOW OR-ORA W - WHITE R-RED NENT IDENTIFICATION FOR DIRE FIRED MAKE-UP AIR UNITS COMPONENT MAIN SUPPLY FAN MOTOR DAMPER MOTOR DAMPER MOTOR DAMPER MOTOR DAMPER MOTOR DAMPER MOTOR DAMPER MOTOR STARTER BURNER RELAY MAIN FAN MOTOR STARTER BURNER RELAY PURGING TIMMG RELAY ALARM CIRCUIT RELAY ALARM CIRCUIT RELAY AUXILARY MAIN GAS VALVE MODUTROL MOTOR TRANSFORMER ALARM CIRCUIT TRANSFORMER ALARM CIRCUIT TRANSFORMER ALARM CIRCUIT TRANSFORMER ALARM CIRCUIT TRANSFORMER ALARM CIRCUIT TRANSFORMER
VG-3 L-1 L-2 L-3 MF-1 B-BLACH BL-BLUE COMPON SYMBOL MTR-1 MTR-4 MTR-6 MTR-6 S-1 S-2 R-2 R-3 PC-6 VG-1 VG-2 VG-3 TR-4 TR-6 TR-8	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETICA DENOTES TERMINALS IN REMOTE CONTR DENOTES TERMINALS IN MAIN PANEL C BR - BROWN Y - YELLOW OR - ORA W - WHITE R - RED VENT IDENTIFICATION FOR DIRE FIRED MAKE-UP AIR UNITS COMPONENT MAIN SUPPLY FAN MOTOR MODUTROL MOTOR DANIPER MOTOR PREMIX BURNER MOTOR MAIN FAN MOTOR STARTER BURNER RELAY PURGING TIMING RELAY LOW FIRE HOLD RELAY ALARM CIRCUIT RELAY ALARM CIRCUIT RELAY PILOT GAS VALVE MAIN GAS VALVE
VG-3 L-1 L-2 L-3 MP-1 B-BLACH B-BLACH B-BLACH B-BLACH SYMBOL MTR-1 MTR-4 MTR-6 MTR-7 MTR-6 MTR-7 MTR-8 TR-8 R-12 R-12 R-12 R-2 R-12 R-14 TR-1 TR-2 TR-1 TR-2 TR-4 TR-6	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETER DENOTES WIRING BY OTHERS DENOTES WIRING BY OTHERS DENOTES TERMINALS IN REMOTE CONTRI- DENOTES TERMINALS IN REMOTE CONTRI- DENOTES TERMINALS IN RAIN PANEL (BR-BROWN Y-YELLOW OR-ORA W - WHITE R-RED NENT IDENTIFICATION FOR DIRE FIRED WAKE-UP AIR UNITS COMPONENT MAIN SUPPLY FAN MOTOR MODUTROL MOTOR DAMPER MOTOR PREMIX BURNER MOTOR
VG-3 L-1 L-2 L-3 MP-1 B-BLACH B-BLACH BL-BLUE COMPON SYMBOL MTR-1 MTR-4 MTR-6 MTR-6 S-1 S-2 R-2 R-3 SW-1 SW-1 SW-3 SW-5	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETER DENOTES WIRING BY OTHERS DENOTES WIRING BY OTHERS DENOTES TERMINALS IN REMOTE CONTRE DENOTES TERMINALS IN MAIN PANEL (BR-BROWN Y-YELLOW OR-ORA W-WHITE R-RED NENT IDENTIFICATION FOR DIRE FIRED WAKE-UP AIR UNITS COMPONENT MAIN SUPPLY FAN MOTOR MODUTROL MOTOR DAMPER MOTOR PREMIX BURNER MOTOR
VG-3 L-1 L-2 L-3 MP-1 B-BLACH B-BLACH B-BLACH B-BLACH B-BLACH COMPON SYMBOL MTR-1 MTR-4 MTR-6 MTR-6 S-1 S-2 R-2 R-3 SW-3 SW-3 SW-5 SW-7	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETER DENOTES TERMINALS IN REMOTE CONTRI- DENOTES TERMINALS IN MAIN PANEL C BR-BROWN Y-YELLOW OR-ORA W - WHITE R-RED VENT IDENTIFICATION FOR DIRE FIRED MAKE-UP AIR UNITS COMPONENT MAIN SUPPLY FAN MOTOR MODUTROL MOTOR DAMPER MOTOR DAMPER MOTOR DAMPER MOTOR PREMIX BURNER MOTOR MAIN FAN MOTOR STARTER BURNER RELAY PURGING TIMING RELAY LOW FIRE HOLD RELAY ALARM CIRCUIT RELAY ALARM CIRCUIT RELAY ALARM CAS VALVE MAIN GAS VALVE MAIN FAN PROVING SWITCH HIGH LIMIT SWITCH MAIN FAN PROVING SWITCH HIGH-GAS CUTOUT SWITCH
VG-3 L-1 L-2 L-3 MF-1 B B-BLACK BL-BLUE COMPON SVMBOL MTR-1 MTR-4 MTR-6 MTR-6 MTR-6 S-1 S-2 R-2 R-2 R-2 R-6 VG-1 VG-2 VG-3 TR-4 TR-6 TR-7 SW-1 SW-3 SW-1 SW-3 SW-5 SW-6	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETIC DENOTES TERMINALS IN REMOTE CONTR DENOTES TERMINALS IN REMOTE CONTR DENOTES TERMINALS IN MAIN PANEL (BR-BROWN Y-YELLOW OR-ORA W - WHITE R - RED VENT IDENTIFICATION FOR DIRE FIRED MAKE-UP AIR UNITS COMPONENT MAIN SUPPLY FAN MOTOR MODUTROL MOTOR DAMPER MOTOR MAIN FAN MOTOR STARTER BURNER RELAY PURGING TIMING RELAY ALARM CIRCUIT RELAY ALARM CIRCUIT RELAY ALARM CIRCUIT RELAY MAIN GAS VALVE MAIN FAN MOTOR TRANSFORMER ALARM CIRCUIT TRANSFORMER ALARM CIRCUIT TRANSFORMER ALARM CIRCUIT TRANSFORMER MAIN DISCONNECT SWITCH HIGH LIMIT SWITCH MAIN FAN PROVING SWITCH HIGH-GAS CUTOUT SWITCH HIGH-GAS CUTOUT SWITCH
VG-3 L-1 L-2 L-3 MP-1 B-BLACK MTR-1 MTR-1 MTR-6 S-1 B-2 R-2 VG-2 VG-2 VG-3	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETER DENOTES TERMINALS IN REMOTE CONTRI- DENOTES TERMINALS IN MAIN PANEL C BR - BROWN Y - YELLOW OR - ORA W - WHITE R - RED VENT IDENTIFICATION FOR DIRE FIRED MAKE-UP AIR UNITS COMPONENT MAIN SUPPLY FAN MOTOR MODUTROL MOTOR DAMPER MOTOR PREMIX BURNER MOTOR MAIN FAN MOTOR STARTER BURNER RELAY PURGING TIMING RELAY LOW FIRE HOLD RELAY ALARM CIRCUIT RELAY ALARM CIRCUIT RELAY ALARM CAS VALVE MAIN GAS VALVE MAIN GAS VALVE MAIN GAS VALVE AUXILARY MAIN GAS VALVE CONTROL VOLTAGE TRANSFORMER MODUTROL MOTOR TRANSFORMER MODUTROL MOTOR TRANSFORMER MAIN FAN PROVING SWITCH MAIN FAN PROVING SWITCH
VG-3 L-1 L-2 L-3 MF-1 B-BLACH BL-BLUE COMPON SYMBOL MTR-1 MTR-4 MTR-6 MTR-6 MTR-6 S-1 S-2 R-2 R-2 R-2 R-6 VG-1 VG-2 VG-3 TR-6 TR-7 SW-1 SW-3 SW-5 SW-5 SW-7 SW-7 SW-7 SW-7	AUXILIARY MAIN GAS VALVE FAN ON LIGHT (GREEN) BURNER ON LIGHT (WHITE) ALARM LIGHT (RED) DAMPER MOTOR POTENTIOMETER DENOTES WIRING BY OTHERS DENOTES TERMINALS IN REMOTE CONTRI- DENOTES TERMINALS IN REMOTE CONTRI- DENOTES TERMINALS IN MAIN PANEL (BR-BROWN Y-YELLOW OR-ORA W - WHITE R-RED NENT IDENTIFICATION FOR DIRE FIRED MAKE-UP AIR UNITS COMPONENT MAIN SUPPLY FAN MOTOR MODUTROL MOTOR DAMPER MOTOR PREMIX BURNER MOTOR MAIN FAN MOTOR STARTER BURNER RELAY PURGING TIMING RELAY ALARM CIRCUIT RELAY ALARM CIRCUIT RELAY ALARM CIRCUIT RELAY ALARM CAS VALVE MAIN GAS VALVE MAIN FAN PROVING SWITCH HIGH LIMIT SWITCH MAIN FAN PROVING SWITCH
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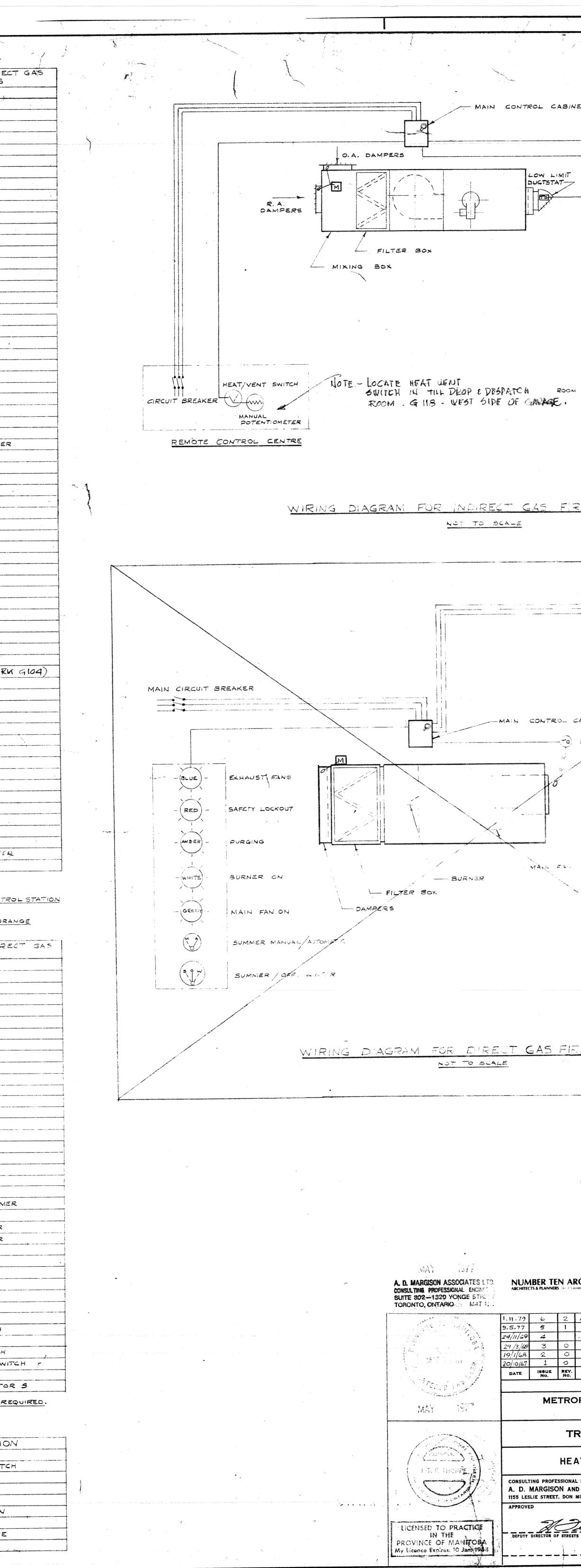
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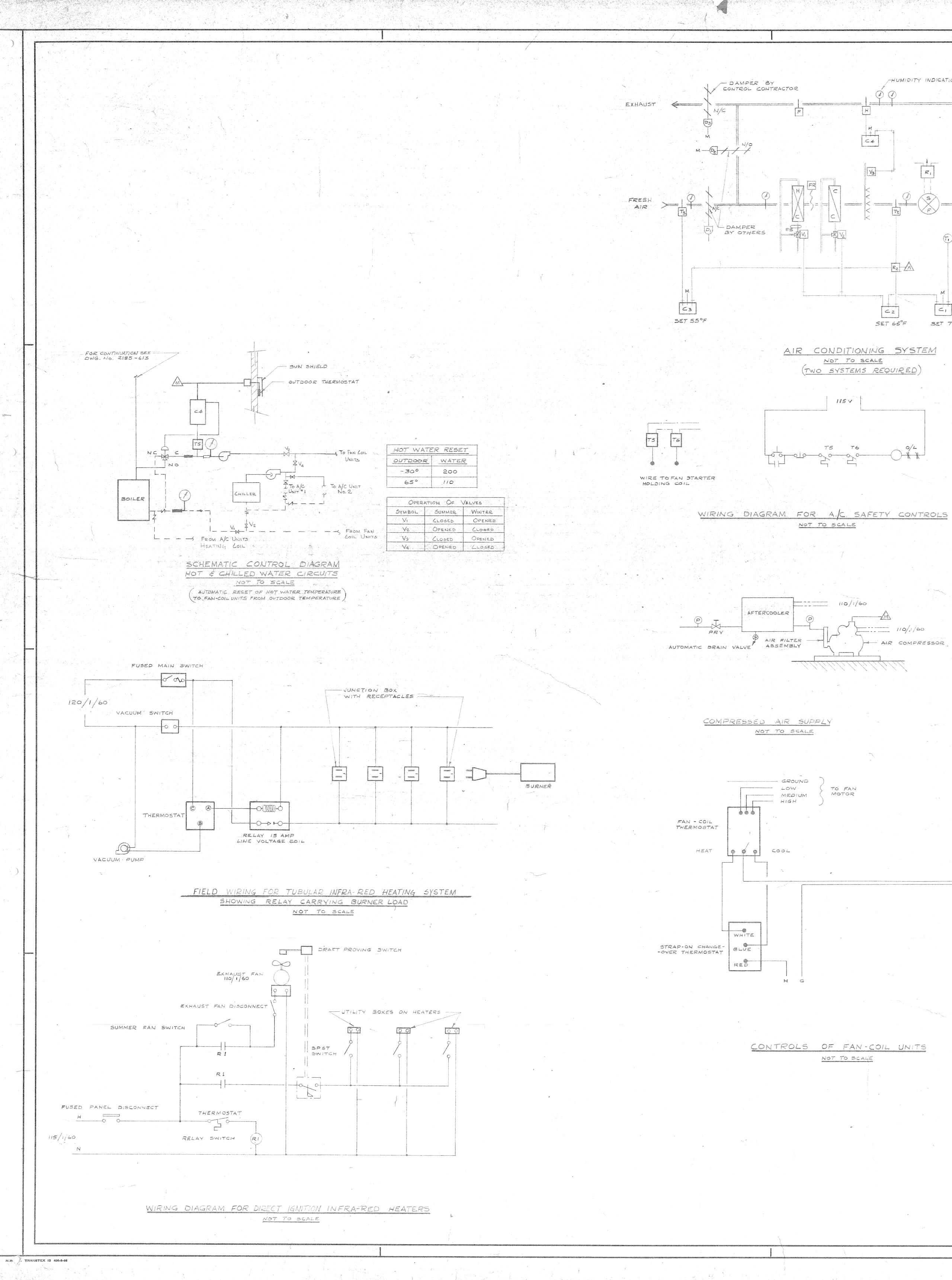
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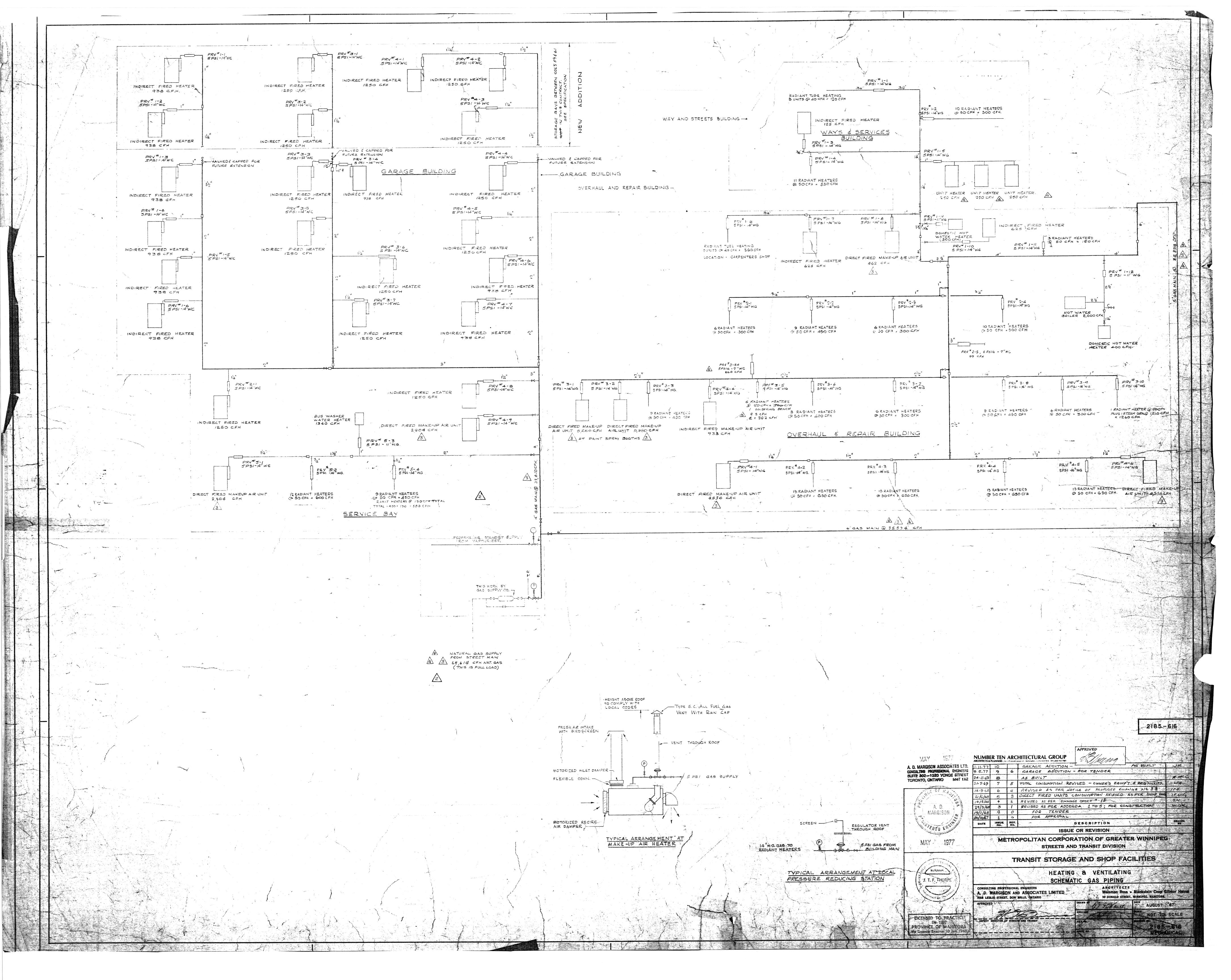
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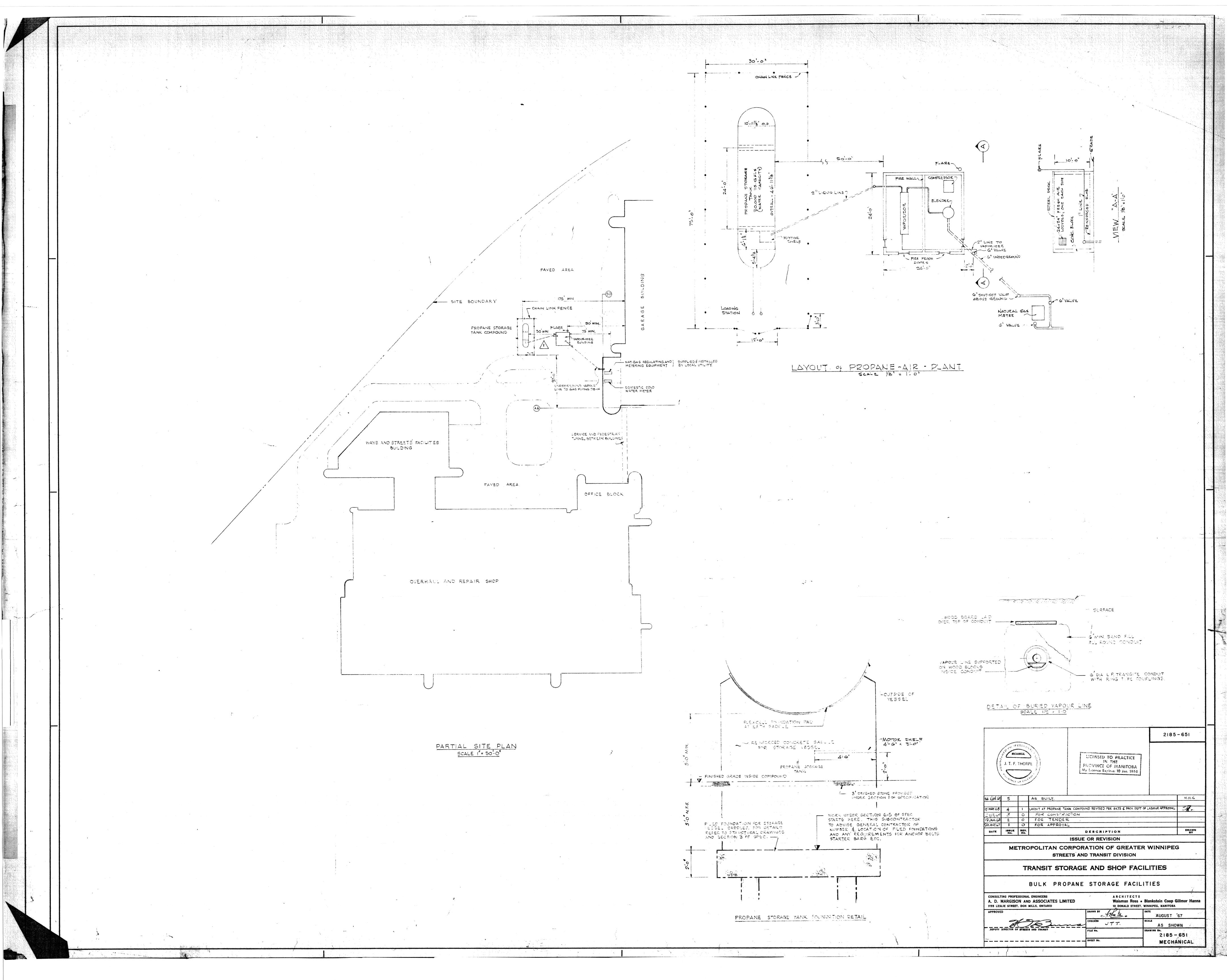
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MECHANICAL





Generic input/output for Metasys Control.

- 1. Controls must be able to interface to MSEA technology on the field device network using either the N2Open or BACnet Protocols. See note 2.
- 2. No LON protocols are to be accepted.
- 3. Controls contractor to provide commissioning sheets for all points on field devices as well as head end equipment.
- 4. Controls contractor to communicate with equipment provider to ensure proper field point integration as well as controllability of the equipment, if not package controls.
- 5. If not a Metasys product installed, the controls contractor must show seamless integration into the exiting Metasys Extended Architecture Operator Interface that is acceptable to City Staff prior to the award of the contract. See note 2.
- 6. Controls contractor to supply all drawings/graphics/sequence of operations in both a hard and soft copy. Drawings and graphics to be able to be read and modified by City of Winnipeg Staff. User interface graphics to be completed using *Graphic Generation Tool* software. Graphics must use City of Winnipeg graphic templates. Contractor to supply As-Built drawings in an editable format, able to be easily edited by City of Winnipeg Staff.
- 7. The use of either N2Open or BACnet to be determined based on type of building where the work is being performed. If the construction is a brand new facility, then BACnet can be used. The term BACnet should then be defined properly in it's use, see note 1 below. If the work is an addition to and the new work is to be tied into the existing controls, then the contractor should contact City of Winnipeg technical staff to determine the best protocol to use based on existing equipment.
- 8. If Other vendor (non-JCI) controls are to be used then a seamless integration must be proven before approval will be given.
- 9. Design Engineer must detail a complete sequence of operations for each controlled device. This is so the marriage of controls and mechanical equipment meets the design intent of the mechanical engineer.
- 10. A complete list of setpoints for all controlled equipment must be provided.
- 11. A points list is to be provided for all controlled objects.
- 12. The controls spec must be complete so that there is no interpretation required on behalf of the controls contractor so that the control system is built to meet the specific needs of the complete mechanical plan and design.
- Alarm Messages. All objects that must be alarmed will have in the alarm message text the following information as per the included example. Alarm Message: Building Address, What is in alarm, see graphic for Instruction Example: 251 Donald SF-1 VFD Common Alarm, see graphic for Instruction

Rooftop Units, Make-Up Air / Air Handling Unit (MUA/AHU):

1. Where possible, the manufacturer of the equipment should be contacted to see if an N2Open or BACnet protocol equipped package controller is available from the factory.

- 2. If no interface from the factory is available then we would as a minimum expect the following points to monitor:
 - a. Start/Stop
 - b. Fan Status
 - c. Economizer Status, command in on/off or % open
 - d. Cooling Mode
 - e. Heating Mode
 - f. Supply Air Temperature
 - g. Room Temperature for Single Zone Unit
 - h. Return Air Temperature for Multizone Unit
 - i. Supply Air Low Limit Status (Freeze Stat)

Exhaust Fans:

1. Exhaust fans will have start/stop/status points.

Boilers:

- 1. Boilers to come with own package controls and outdoor air temperature for reset control.
- 2. A Metasys Interface for the controls to be part of the package for direct connection on either the N2Bus or BACnet.
- 3. If no interface package exists, the following points are required as a minimum:
 - a. Hot Water Supply Temperature
 - b. Hot Water Return Temperature
 - c. Boiler Status
 - d. Boiler Alarm, this is to be a generic alarm for all mechanical safeties or other related devices, which would cause the boiler to be shut down.

Chillers:

- 1. Chillers to come with own package controls and outdoor air temperature for reset control.
- 2. A Metasys Interface for the controls to be part of the package for direct connection on either the N2Bus or BACnet.
- 3. If no interface package exists, the following points are required as a minimum:
 - a. Chilled Water Supply Temperature
 - b. Chilled Water Return Temperature
 - c. Chiller Status
 - d. Chiller Alarm, this is to be a generic alarm for all mechanical safeties or other related devices, which would cause the chiller to be shut down.
 - e. Condenser Water Supply Temperature
 - f. Condenser Water Return Temperature
 - g. Water Tower fans/pumps Status

Pumps:

1. Pumps will have a start/stop/status as a minimum.

Variable Speed/Frequency drives:

1. All VFD/VSD to have N2/BACnet interface built into the device. If the manufacturer is not able to provide this, get another manufacturer. ABB would be the acceptable standard here.

Lighting Controls:

1. No LON lighting controls are to be accepted. No exceptions.

VAV boxes:

1. VAV boxes to have digital controller mounted directly to the VAV box actuator. This is to have a digital room thermostat and proportional control on the damper. This controller to use either N2Open or BACnet.

Sump Pits:

- 1. Sump pits to have high alarm status installed.
- 2. If lead/stby pumps are present, then sensing of the lead pump is required.

Generic Inputs from the Facility:

1. Room temperatures in corner office/rooms on each floor, especially if there are windows present

Notes:

- 1. The term BACnet refers to an industry standard protocol that basically states that all devices using the BACnet technology will be able to communicate to each other. This is not necessarily the case. The BACnet protocol is comprised of several layers of interoperability and intercommunications. The controls contractor performing the supervisory controller installation should confirm that all devices specified are able to communicate to the proposed devices using the BACnet PIC statement and then supply documentation such that all devices supplied will communicate to each other as required for proper operation of the system. This includes integration into the ADX server.
- 2. If Metasys Network Automation Engines (NAE/NIE/NCE) are to be installed on the project then the version of these devices and their software must be such that the City of Winnipeg does not be required to update/upgrade the existing ADX server in order for all user views, alarms, and point monitoring to occur. The contractor must co-ordinate with City staff to determine the correct version to be installed. All user views and graphics must not be installed in the local supervisory controller (NAE/NIE/NCE). All such items must be programmed into the existing ADX server. User views and graphics must be approved for use by City staff before implementation of such items.
- 3. All monitored points that have alarms must have operating instructions and alarm messages. These will be co-ordinated with the tech shop and operations supervisor.



Phuzion[™]

LED High Bay





DesignLights Consortium[®] (DLC) qualified product. Not all versions of this product may be DLC qualified. Please check the DLC Qualified Products List at www.designlights.org to confirm which versions are qualified.

ORDERING INFORMATION

Catalog Number

Notes

Description

The Phuzion LED luminaire takes high-bay lighting to new levels of lumen output and temperature tolerance. By marrying the latest in LED technology with the legendary illuminating dynamics of Holophane's prismatic glass, the Phuzion high bay brings to the industrial environment LED lighting of unparalleled performance and reliability.

Optics

- Prismatic borosilicate glass maintains highest levels of luminosity over time.
- Glass doesn't fade, discolor or otherwise degrade in harsh environments.
- Three distributions (narrow, medium and wide) available to maximize versatility.
- Highly engineered LED system ensures superior uniformity and maximizes spacing.
- IP65 rated optics.

Mechanical

- Robust cast aluminum housing with low copper content (0.6% CU content) withstands hot and dirty environments.
- Pendant mount standard.
- Achieves up to 149°F (65°C) ambient rating.

Electrical

- 0-10V dimming driver is standard (must specify the D option to enable dimming), 2kV/1kA level of surge protection provided by driver.
- An added 6kV/3kA level of surge protection is an option on 120-277 and is a standard option on 347/480V.

Typical Applications

- Heavy industrial
- Light manufacturing
- Warehousing
- Large indoor

- An added 20kA in-line surge protection is also an option on 120-277.
- CRI > 70 (nominal) is standard.
- 3000K, 4000K or 5000K CCT available.
- Fault-tolerant LED light engine continues to provide light even in the failure of one LED.
- Aluminum core printed circuit board.
- For AS (120-277V), dimming source current = 300 micro amps (18L, 24L, 27L) and 150 micro amps (12L).
- For AH (347/480V), dimming source current = 2000 micro amps (18L, 24L, 27L) and 1000 micro amps (12L).

Listings

- CSA Certified for use in damp locations, $65^\circ\!C$ ambient environments.
- DesignLights Consortium[®] (DLC) qualified product. Not all versions of this product may be DLC qualified. Please check the DLC Qualified Products List at <u>www.designlights.org</u> to confirm which versions are qualified.

Warranty

5-year limited warranty. Complete warranty terms located at:

www.acuitybrands.com/CustomerResources/Terms_and_Conditions.aspx

Actual performance may differ as a result of end-user environment and application.

Actual wattage may differ by +12%/-12% when operating between 120-480V +/- 10%.

NOTE: Specifications subject to change without notice.

Dimensions: Inches (millimeters) unless otherwise noted.

Diameter: 21.22 (538.99) Height: 19.02-23.46 (483.11-595.88) Weight: 33-38 lbs. (15.0-17.2 kg)

Example: PHZ 18L 4K AS P G W

Series	Lumens		Color temperature ¹	Voltage			Mou	nting		Finis	h	Opti	cs
PHZ	18L 18,00 24L 24,00	00 nominal lumens 00 nominal lumens 00 nominal lumens 00 nominal lumens	3K 3000K CCT 4K 4000K CCT 5K 5000K CCT	AS Auto (120- 12 120V 20 208V 24 240V	-277)	7 277V HH Auto sensing (347/480) ² 4 347V ² 8 480V ²	P Q N QR NR	Quick disc	onnect nnect thru-wirin onnect retrofit nnect thru-wirin	L	White Gray Black paint Satin nickel paint Tiger Drylac paint	N M W	Narrow Mediur Wide
Options													
MSE6NDI		360° motion sensor on/off. ³	r embedded, high bay 15	-45 ft.,	CDP-L5-15-2	1.5			C6 CX	6 ft. Safet X ft. Safet	•		
MSE62L3	VDL	360° motion sensor embedded, high bay 15-45 ft., on/off with second time-out period, goes to a		CDP-L6-15-X 208V/240V cord and plug ^{8,9} CDP-L7-15-X 277V cord and plug ^{8,9}		3,9		SPAS		, tector, 120V-277V , add	ed 6kV/	/3kA level	
		dim setting. ^{3,4}	re turning off max./ 3vol		CDP-L24-20 CDP-L8-20-						tector, 347V-480V , add rotection, STANDARD 0		/3kA level
MSE6NDI	LDSCNDL		selectable modes of ope node. Photocell has full o ccupancy. ³		CDP-5-15-X PF-129	Straight blade 120V Anti-rotational hool	JIAJ201 .		Surge prot	ector, 120V-277V , adde ection	d 20kA	in-line	
AXA10		XPoint Wireless ena	abled 4,5		PF-105	Loop, 3/4" male			D	Dimming	terminal ¹⁰		
MSE6XAD	OL DSCXA	XPoint Wireless ena occupancy sensor ⁴	abled with photocell sen	sor &	PF-121-A CD-3	Safety hook, 3/4" m 3 ft. cord ⁸	ale		PHCB PHCB-L8-480		k cord for 120V-277V, 3 k cord for 480V ¹²	47V ^{11,12}	
F1		Single fusing ⁶			CD-6	6 ft. cord ⁸			WG	Wire guar	d installed		
F2		Double fusing ⁷			CD-X	X ft. cord ^{8,9}			FR	Frosted gla			
					G	3 ft. Safety chain			80CRI	80 CRI CCT			
									BSL722	Remote en	nergency battery pack, st	tandard	version ¹³
									BSL722C	Remote er	nergency battery pack, o	cold ver	rsion ^{13,14}

For accessories and footnotes, see page 2.



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Туре

LED High Bay

ORDERING INFORMATION (cont'd.)

Accessories: Order as separate catalog number.										
PHZCHAIN3	3 ft. safety chain	UPH-35-L8-480-WH	Thru-way powerhook for 480V	PF-122-A	Safety hook, 3/4" female					
PHZCHAIN6 PHZCHAINX	6 ft. safety chain X ft. safety chain ⁹	UPH-36-***-WH	Powerhook for 120V, 208V, 240V, 277V and 347V ¹²	PF-129-A PF-105-B	Anti-rotational hook, 3/4" male Loop, 3/4" male					
UPH-35-***-WH	Thru-way powerhook for 120V, 208V, 240V, 277V and 347V ¹²	UPH-36-L8-480-WH PF-116-A	Pendant powerhook for 480V Loop, 3/4" female	PF-121-A WGLED	Safety hook, 3/4" male Wire guard					

Notes

70 CRI standard. 1

60° C max. ambient. 2

3 Not available with XPoint, 50°C max. ambient.

4 Not available with D option.

AS voltage not available; 120V 50°C rated; 208, 240 and 277V 60°C rated only. 5

6 For 120V, 240V, 277V and 347V units; factory installed.

For 208V, 240V and 480V units; factory installed. 7

8 Order PF also; 3ft to 6ft standard cord length.

9 X = length of cord/chain in feet; 6 feet is standard.

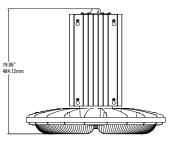
10 Not available with MSE62L3VDL, AXA10, MSE6XADL DSCXA. 11 Order UPH also, PF-105 installed.

12 *** = voltage.

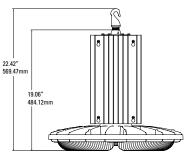
13 P mount only, 120-277V only, not available with F2 fusing. Not available with CDP options. Battery pack ships separate. Max 50°C listed.

14 Un-switched supply power must be provided. To switch emergency fixture, controls must be used (sensor, X-point, etc.). Remote emergency battery pack provided with 20-ft flex conduit.

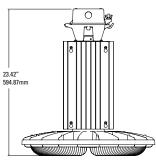
DIMENSIONAL DATA



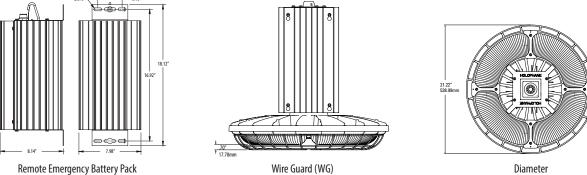
Pendant (P)



Hook (PF-129)



Quick Disconnect (Q)





LED High Bay



OPERATIONAL DATA

Ambient Temperature Ratings

Mounting	Thru-wire	Fuse, Surge	Occupancy Sensor	QDH or Non-disconnect	Voltage	Ambient C° 18L, 24L, 27L ^{1,2}	Ambient C° 12L ^{3,4}	Ambient C° 12L, 18L, 24L, 27L with Emergency option	Supply Wire Temperature
Ceiling	Yes	Yes	Yes	Yes	120-277 347/480	50	60	NA	194°F (90°C)
Ceiling	Yes	Yes	No	Yes	120-277 347/480	55	55	NA	194°F (90°C)
Ceiling	Yes	Yes	No	Yes	120-277	65	65	NA	221°F (105°C)
Ceiling	Yes	Yes	No	Yes	347/480	60	60	NA	221°F (105°C)
Ceiling	No	Yes	No	Yes	120-277	65	65	NA	194°F (90°C)
Ceiling	No	Yes	No	Yes	347/480	60	60	NA	194°F (90°C)
Pendant	No	Yes	Yes	No	120-277 347/480	50	60	50	194°F (90°C)
Pendant	No	Yes	No	No	120-277	65	65	50	194°F (90°C)
Pendant	No	Yes	No	No	347/480	60	60	50	194°F (90°C)

Notes

1 For Xpoint option with 18L, 24L, 27L no sensor = 50C (120V only), 60C (208V, 240V, 277V only). Above ambient values over-ride this ambient if lower. -20°C.

2 For Xpoint option with 18L, 24L, 27L with sensor = 50C (120-277V only), -20°C.

3 For Xpoint option with 12L, no sensor = 65C (120-277V only). Above ambient values over-ride this ambient if lower, -20°C.

4 For Xpoint option with 12L with sensor = $60C (120-277V \text{ only}), -20^{\circ}C.$

Operating Characteristics

Lumen Package	Ambient Rating (120V-277V)	Ambient Rating (347V-480V)	Distribution	Delivered Lumens, 3000K CCT, 70 CRI @25°C ¹	Delivered Lumens, 4000K CCT, 70 CRI @25°C1	Delivered Lumens, 5000K CCT, 70 CRI @25°C1	Delivered Lumens, 3000K CCT, 80 CRI @25°C1	Delivered Lumens, 4000K CCT, 80 CRI @25°C ¹	Delivered Lumens, 5000K CCT, 80 CRI @25°C1	Frosted Lens Multiplier
12L	-40°F to 149°F (-40°C-65°C)	-40°F to 140°F (-40°C-60°C)		11129	12310	12278	10314	11409	11380	0.92
18L	-40°F to 149°F (-40°C-65°C)	-40°F to 140°F (-40°C-60°C)		16918	18713	18665	15680	17344	17299	0.92
24L	-40°F to 149°F (-40°C-65°C)	-40°F to 140°F (-40°C-60°C)	N	22143	24493	24430	20523	22701	22642	0.92
27L	-40°F to 149°F (-40°C-65°C)	-40°F to 140°F (-40°C-60°C)		23331	25808	25741	21624	23919	23858	0.92
12L	-40°F to 149°F (-40°C-65°C)	-40°F to 140°F (-40°C-60°C)		11136	12318	12286	10321	11416	11387	0.92
18L	-40°F to 149°F (-40°C-65°C)	-40°F to 140°F (-40°C-60°C)		16928	18725	18676	15689	17355	17310	0.92
24L	-40°F to 149°F (-40°C-65°C)	-40°F to 140°F (-40°C-60°C)	M	22157	24508	24445	20535	22715	22656	0.92
27L	-40°F to 149°F (-40°C-65°C)	-40°F to 140°F (-40°C-60°C)		23346	25824	25757	21638	23934	23872	0.92
12L	-40°F to 149°F (-40°C-65°C)	-40°F to 140°F (-40°C-60°C)		11151	12334	12302	10335	11432	11402	0.91
18L	-40°F to 149°F (-40°C-65°C)	-40°F to 140°F (-40°C-60°C)		16951	18750	18702	15711	17378	17333	0.91
24L	-40°F to 149°F (-40°C-65°C)	-40°F to 140°F (-40°C-60°C)	W	22187	24542	24478	20563	22746	22687	0.91
27L	-40°F to 149°F (-40°C-65°C)	-40°F to 140°F (-40°C-60°C)		23377	25859	25792	21667	23967	23905	0.91

Notes

1 Absolute photometry calculated in accordance with IESNA LM-79-08



Phuzion™

LED High Bay



OPERATIONAL DATA CONTINUED

Emergency Lumens

Package	Narrow	Medium	Wide	Frosted Lens Multiplier	
PHZ 12L, 18L, 24L, 27L	1666 Lumens	1706 Lumens	1691 Lumens	.92	

Projected Lumen Maintenance (TM-21)¹

Package	0 Hours	15,000 Hours	30,000 Hours	45,000 Hours	60,000 Hours	100,000 Hours
PHZ 12L, 18L, 24L, 27L @ 25C	1.00	0.99	0.98	0.98	0.97	0.96
PHZ 12L, 18L, 24L, 27L @ 40C	1.00	0.98	0.97	0.96	0.96	0.94
PHZ 12L, 18L, 24L, 27L @ 55C	1.00	0.98	0.96	0.95	0.94	0.91
PHZ 12L, 18L, 24L, 27L @ 65C	1.00	0.96	0.94	0.93	0.91	0.88

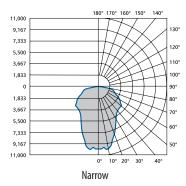
Notes

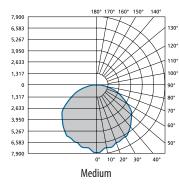
1 Calculated using data collected according to LM-80 and represents lumen maintenance of the LED package.

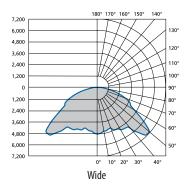
Wattage

Lumen Package	120V	277V	347V	480V	C omparable Light Source
12L	120	118.8	121.0	120.3	4-lamp T8, 250W HID
18L	185	183.1	186.6	185.4	4-lamp T5HO, 6-lamp T8
24L	238	235.6	240.1	238.5	6-lamp T5HO, 8-lamp T8, 400W HID
27L	255	252.4	257.2	255.6	8-lamp T5HO, 8-lamp T8

DISTRIBUTION DATA







Phuzion™

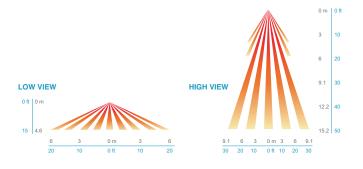
LED High Bay



CONTROLS



- MSE6NDL, MSE62L3VDL, MSE6NDL DSCNDL, AXA10, MSE6XADL DSCXA; Sensor Coverage Data
- Best choice for 15 to 45 ft. (4.57 to 13.72 m) mounting heights
- 15 to 20 ft. (4.57 to 6.10 m) radial coverage overlaps area lit by a typical high bay fixture
- Large motion (e.g., walking) detection up to a 35-ft. (10.76 m) mounting height
- Extra large motion (e.g., forklifts) detection up to a 45-ft. (13.72 m) mounting height



COMPONENTS & OPTIONS DATA



XPoint wireless

Integrated wireless control technology connecting fixtures, sensors, and other modules together.



Surge protection

Phuzion drivers provide 2kV of surge protection as standard. The optional (SPAS or SPAH) provides 10kV of protection while the SPAS20 provides 20kV of protection.



Wireguard

Steel wireguard available to further protect fixture from impact.



Sensors

Occupancy-only mode that controls on/off and dimming of the fixture. Photocell option reads daylight levels to dim lights or prevent start-up.



Fusing

Integrated internal fast-blow fusing is available for all configurations.



Hook and cord 3/4" hub standard. Multiple hooks and other mountings available. Cord sets can be specified with or without plug.



Dimming drivers Drivers use 0-10V protocol with dimming down to 10% power / 30% lumen output.



Optics

Standard prismatic, borosilicate glass that doesn't fade or degrade. Optional frosted optics provide even greater visual comfort.



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B Series Quick Reference Guide

Intrusion – Small Commercial/Retail/Banking



Enclosures



D138 D137

B10 Medium Enclosure



D8103

Enclosure

D8108A

ICP-EZTS Universal Tamper



D8108A Enclosure

Credentials

RFID Tags for B942 Kepads



ACD-ATR11ISO ACD-ATR14CS ACA-ATR13

N COL

D5500CU **RPS** Upgrade

RPS

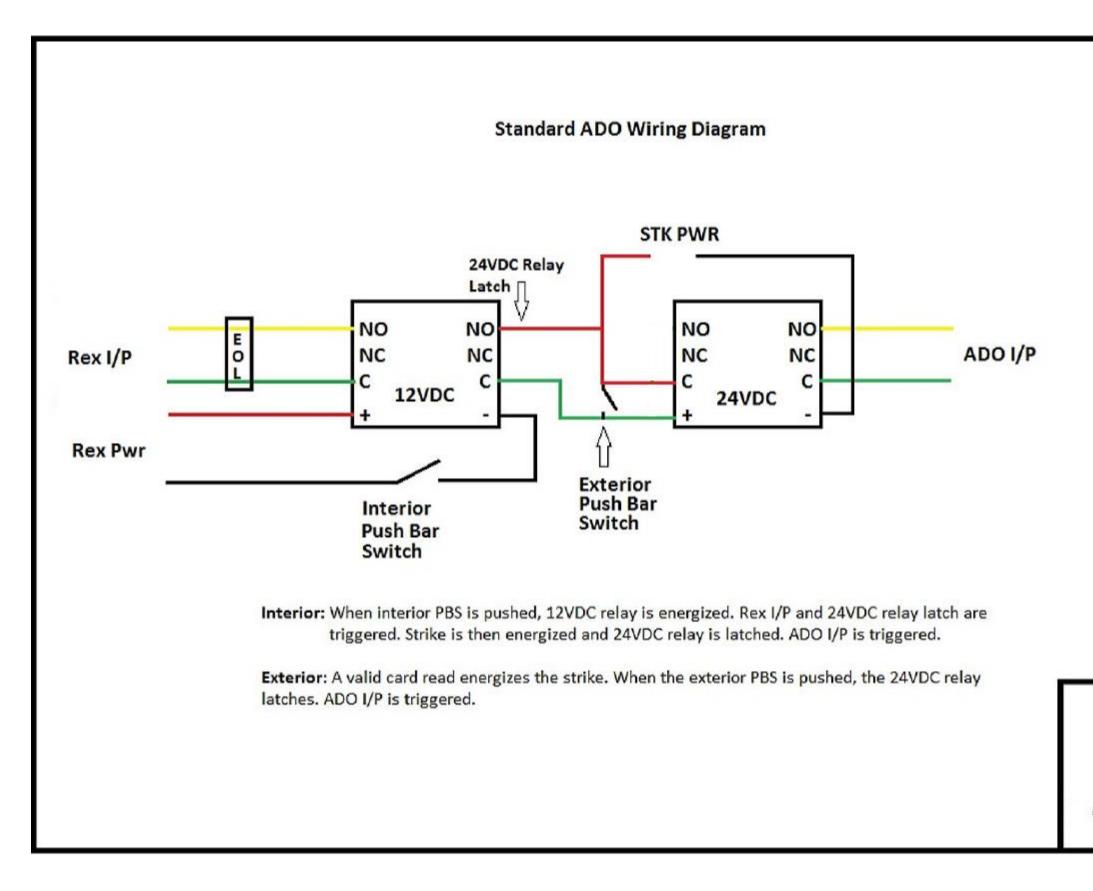
D5370-USB D5371-USB 9 H D5500CU-LITE

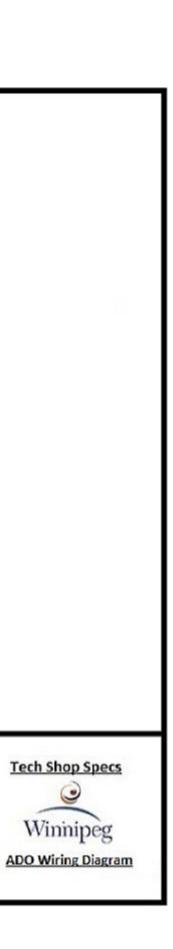
RPS Lite

B99 USB Cable

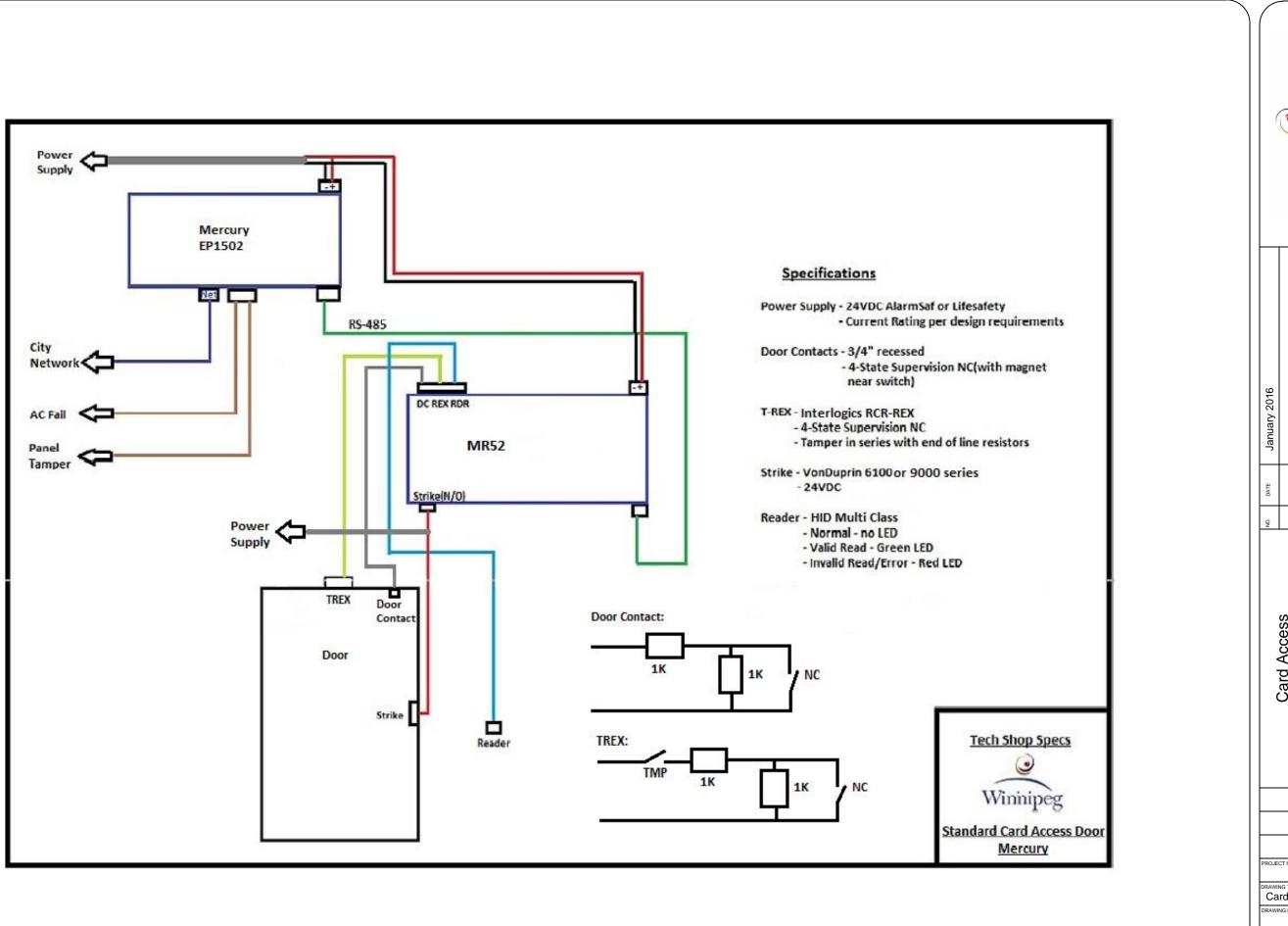
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B12 Bracket for D8103/

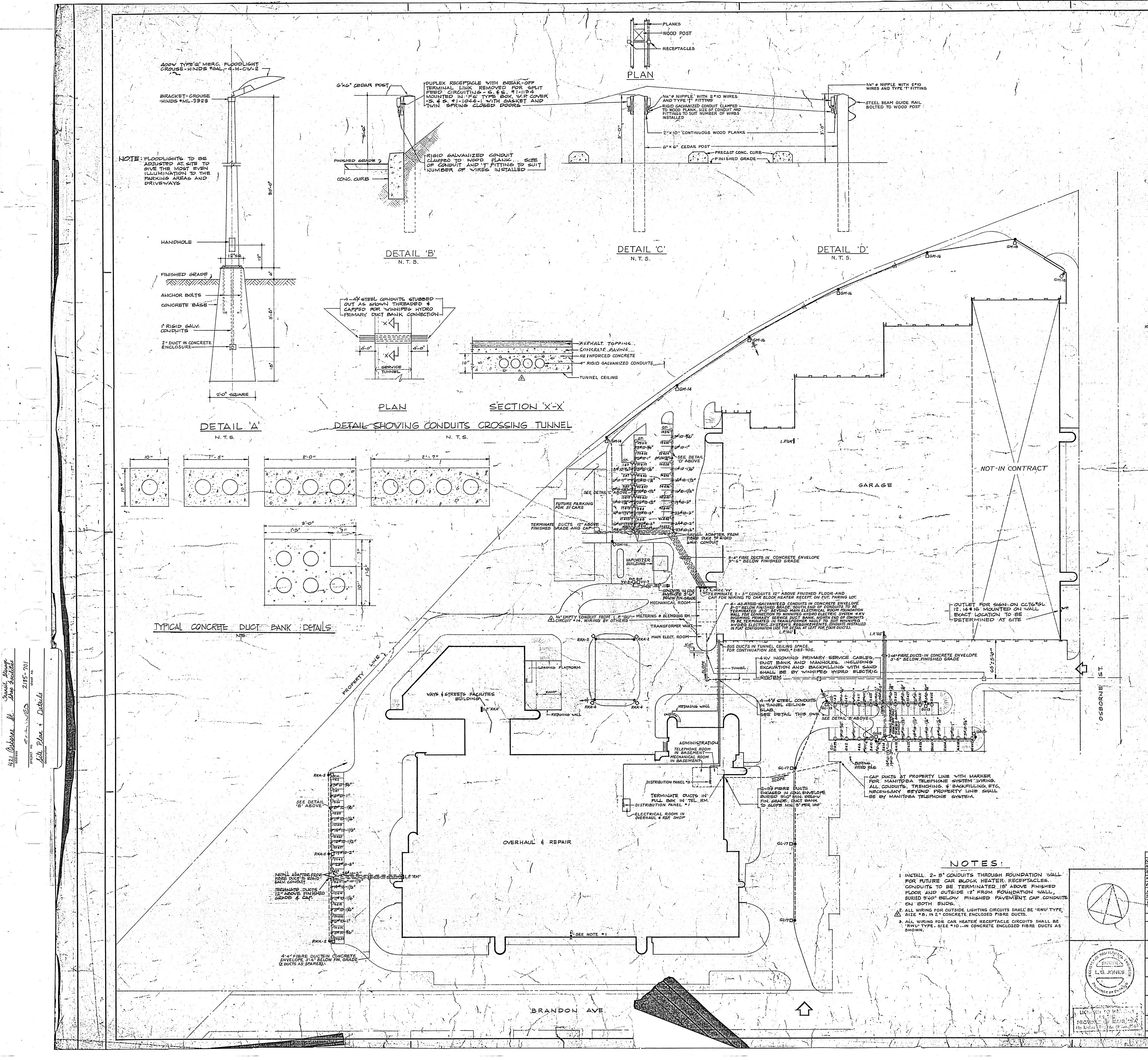




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LEGEND

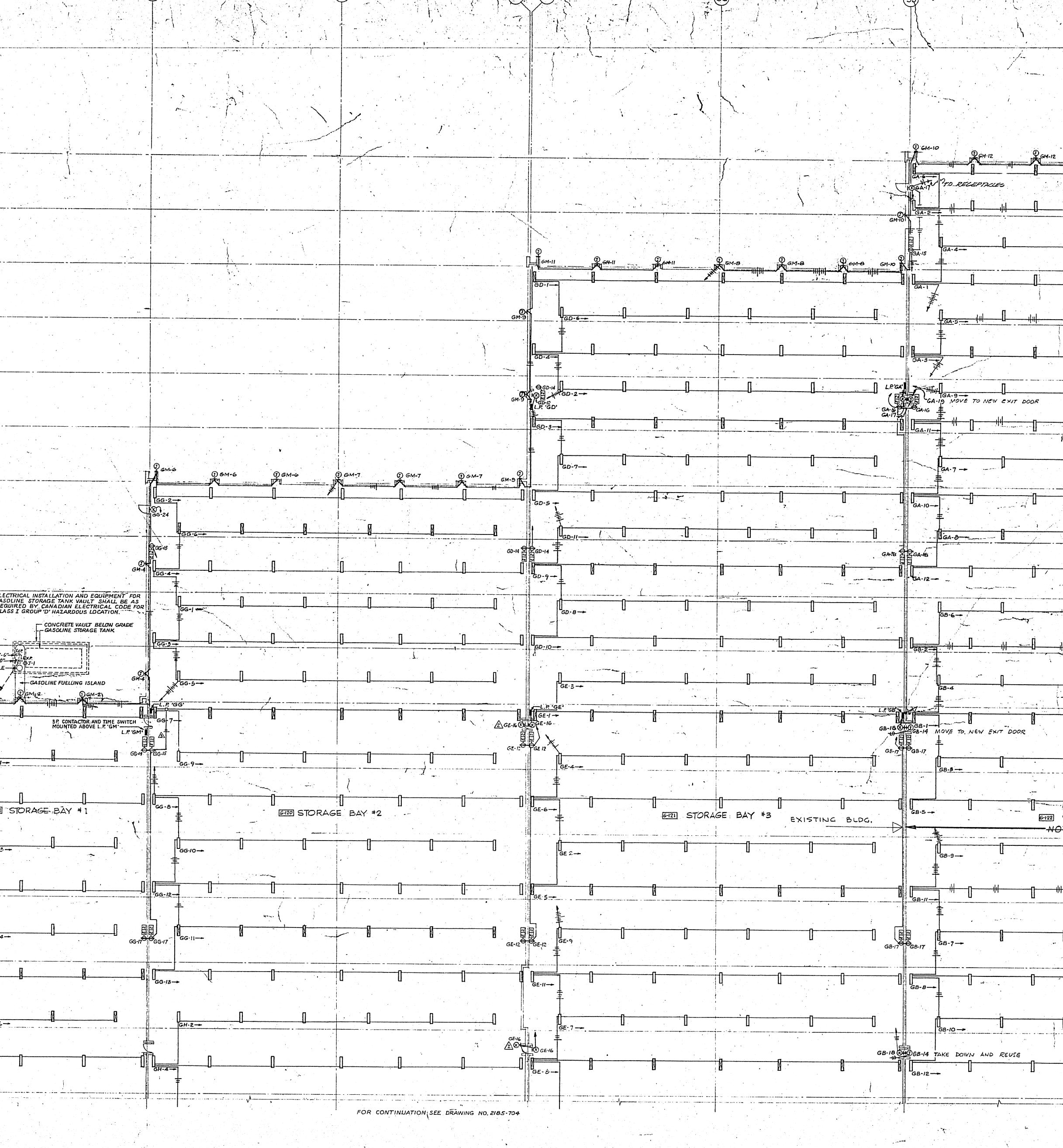
	FLUORESCENT LIGHTING FIXTURE, CELING MOUNTED, TYPE'A' CONNECTED TO LIGHTING PANEL RG, CIRCUIT #7 FLUORESCENT LIGHTING FIXTURE, USED AS NIGHT LIGHT		
0	FLUORESCENT LIGHTING FIXTURE, BRACKET TYPE OUTLET BOX	1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.	
€ €	INCANDESCENT OR MECURY VAPOUR LIGHTING FIXTURE		
KX XI	BRACKET TYPE EXIT LIGHT ILING		
\$3 \$2	BOWAY SWITCH SWITCH WITH PILOT LIGHT		
	SINGLE POLE SWITCH		
⊕= .⊕= .⊕=×₽	DUPLEX RECEPTACLE MOUNTED ABOVE COUNTERTOP		
⊖ ^{ex} r; €	DUPLEX RECEPTACLE, EXPL. PROOF, 20 A, 125 V, CROUSE HINDS + CPS 152-212. WELDING RECEPTACLE 1004, 3PH; 4W, 200V TO MATCH ERUIP. DUPLEX RECEPTACLE, 200 V, 15 A HUBBELL + 5662.		
Commaster)	CLOCK MOUNTED 12'O" ABOVE FINISHED FLOOR IN GARAGE, OVERHAUL: & REPAIR SHOP AND 7'G" IN OFFICE BUILDING UNLESS OTHERWISE NOTED		
Θ	FLOOR RECEPTACLE, HUBBELL # 5261 IN NEPCO BOD BOX		
	SHAVING OUTLET, MOUNTED 3'G" ABOVE FINISHED FLOOR TELEPHONE WALL MOUNTED OUTLET	1 ** •••• 1 2	• • • • • • • • • • • • • • • • • • •
	P.A. MICROPHONE		
	P.A. HORN SINGLE PROJECTION MOUNTED APPROX. 15-0" ABOVE FINISHED FLOOR P.A. SPEAKER CEILING MOUNTED	1 1 1 1	
RECESSED SURF	P.A. HORN DOUBLE PROJECTION MOUNTED APPROX. 15-0" ABOVE FINISHED FLOOR UNLESS OTHERWISE NOTED		
Ē	FIRE ALARM MANUAL STATION FIRE ALARM BELL 10"DIA. OR AS NOTED		
	FIRE ALARM HORN DOUBLE PROJECTION 1360F COMBINATION TYPE F.A. DETECTOR		
⊗ ⊡ ∙	190°F FIXED TYPE F.A. DETECTOR PISCONNECT SWITCH	A CALL	
	MANUAL STARTER MAGNETIC STARTER		
	COMBINATION MAGNETIC STARTER		
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.,	OTHERS ELECTRIC HEATER 200V SPH. SUPPLIED AND INSTALLED BY. OTHERS	2	
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e	30'-0" HIGH STANDARD WITH ONE 400 W TYPE 'Q' MERCURY		
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⊳	INTERCOM. SYSTEM MICROPHONE	1 Park	
Þ _0	INTERCOM. SYSTEM SPEAKER TALK-BACK STATION (MITS'G") & ASSOCIATED TRUMPET (M.H. 15'O") OUTLET BOX FOR GAS FIRED INFRA-RED HEATER MOUNTED ADJACENT TO HEATER, WIRING & CONNECTION		
	INTERCOM. SYSTEM SPEAKER TALK-BACK STATION (MITS'G') & ASSOCIATED TRUMPET (M.H. 15'O") OUTLET BOX FOR GAS FIRED INFRA-RED HEATER MOUNTED ADJACENT TO HEATER, WIRING & CONNECTION TO HEATERS BY OTHERS.		
	INTERCOM. SYSTEM SPEAKER TALK-BACK STATION (MITS'G') & ASSOCIATED TRUMPET (M.H. 15'O") OUTLET BOX FOR GAS FIRED INFRA RED HEATER MOUNTED ADJACENT TO HEATER, WIRING & CONNECTION TO HEATERS BY OTHERS. OUTLET BOX FOR 208V CONNECTION TO CARBON MONOXIDE ANALYZER MTD. G'O" ABOVE FINISHED FLOOR.		とくして
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•	INTERCOM. SYSTEM SPEAKER TALK-BACK STATION (MH.S.G.) & ASSOCIATED TRUMPET (M.H. 15'O") OUTLET BOX FOR GAS FIRED INFRA-RED HEATER MOUNTED ADJACENT TO HEATER, WIRING & CONNECTION TO HEATERS BY OTHERS. OUTLET BOX FOR 200V CONNECTION TO CARBON MONOXIDE ANALYZER MTD. G'O" ABOVE FINISHED FLOOR UTLET BOX FOR 120V CONNECTION TO CARBON MONOXIDE MONITOR MTD. G'O" ABOVE FINISHED FLOOR FAN COIL UNIT COMPLETE WITH TERMINAL JUNCTION BOX. SUPPLIED 4 INSTALLED BY OTHERS, ELECTRICAL CONTRACTOR SHALL TERMINATE & CONNECT WIRING IN JUNCTION BOX.		
•	INTERCOM. SYSTEM SPEAKER TALK-BACK STATION (MIHS'G') & ASSOCIATED TRUMPET (M.H. 15'O") OUTLET BOX FOR GAS FIRED INFRA RED HEATER MOUNTED ADJACENT TO HEATER, WIRING & CONNECTION TO HEATERS BY OTHERS. OUTLET BOX FOR 208V CONNECTION TO CARBON MONOXIDE ANALYZER MTD. G'O" ABOVE FINISHED FLOOR. OUTLET BOX FOR 100V CONNECTION TO CARBON MONOXIDE MONITOR MTD. G'O" ABOVE FINISHED FLOOR. FAN COIL UNIT COMPLETE WITH TERMINAL JUNCTION BOX SUPPLIED & INSTALLED BY OTHERS, ELECTRICAL CONTRACTOR SHALL TERMINATE & CONNECT WIRING IN JUNCTION BOX. DENOTES NUMBER OF WIRES IN CONDUIT. EXPOSED IN UNFINISHED AREAS, OR CONCEALED IN WALL OR CEILING SPACE ABOVE IN FINISHED AREAS. ARROW HEAD PENOTES HOME RUN TO RESP. PANEL. UNMARKED RUNS INDICATE ZWIRES IN CONDUIT.		
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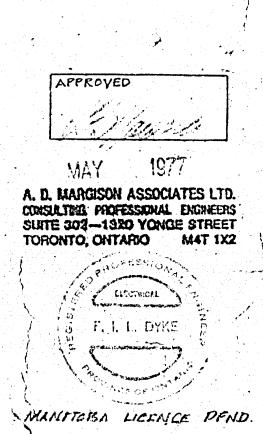
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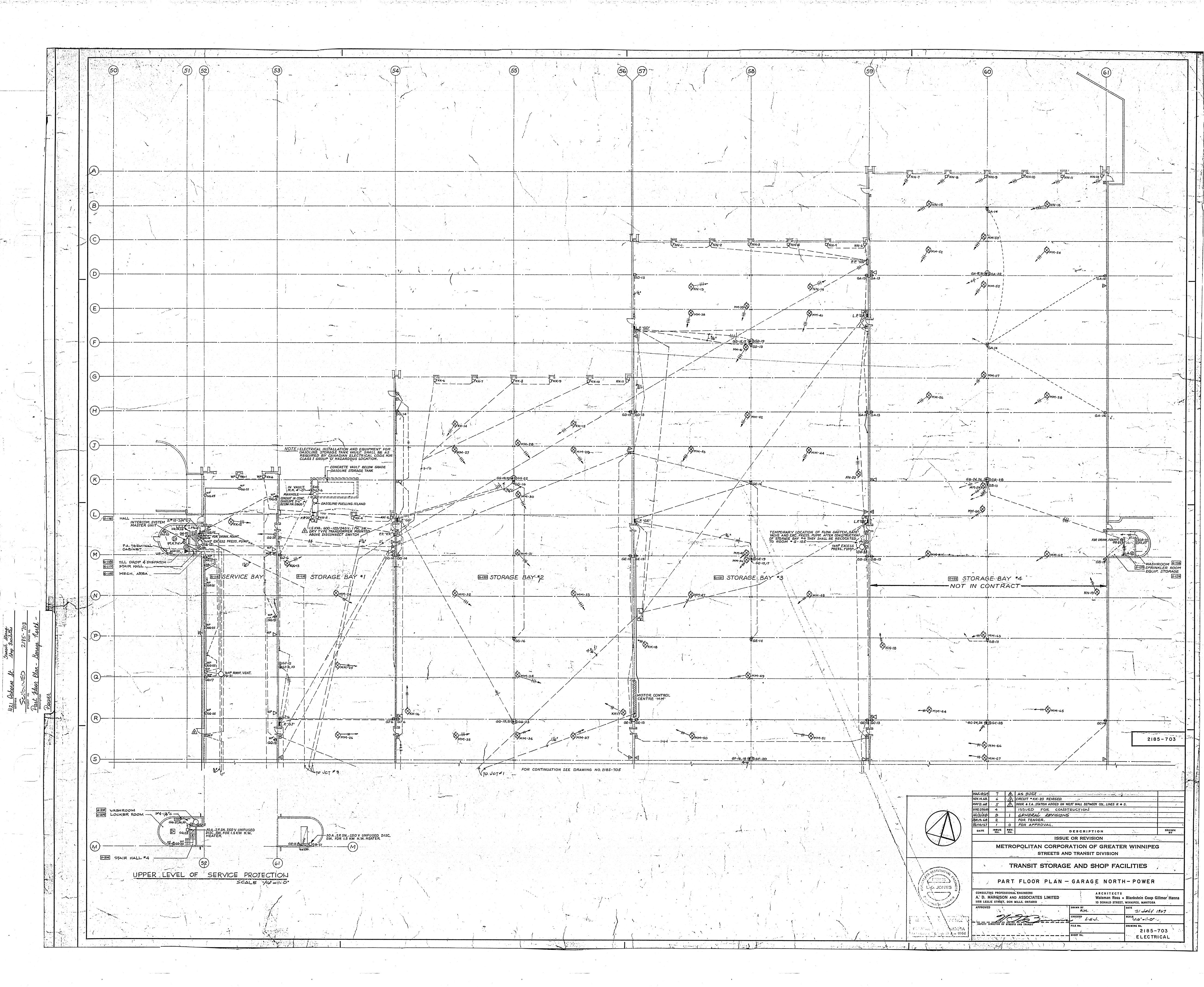
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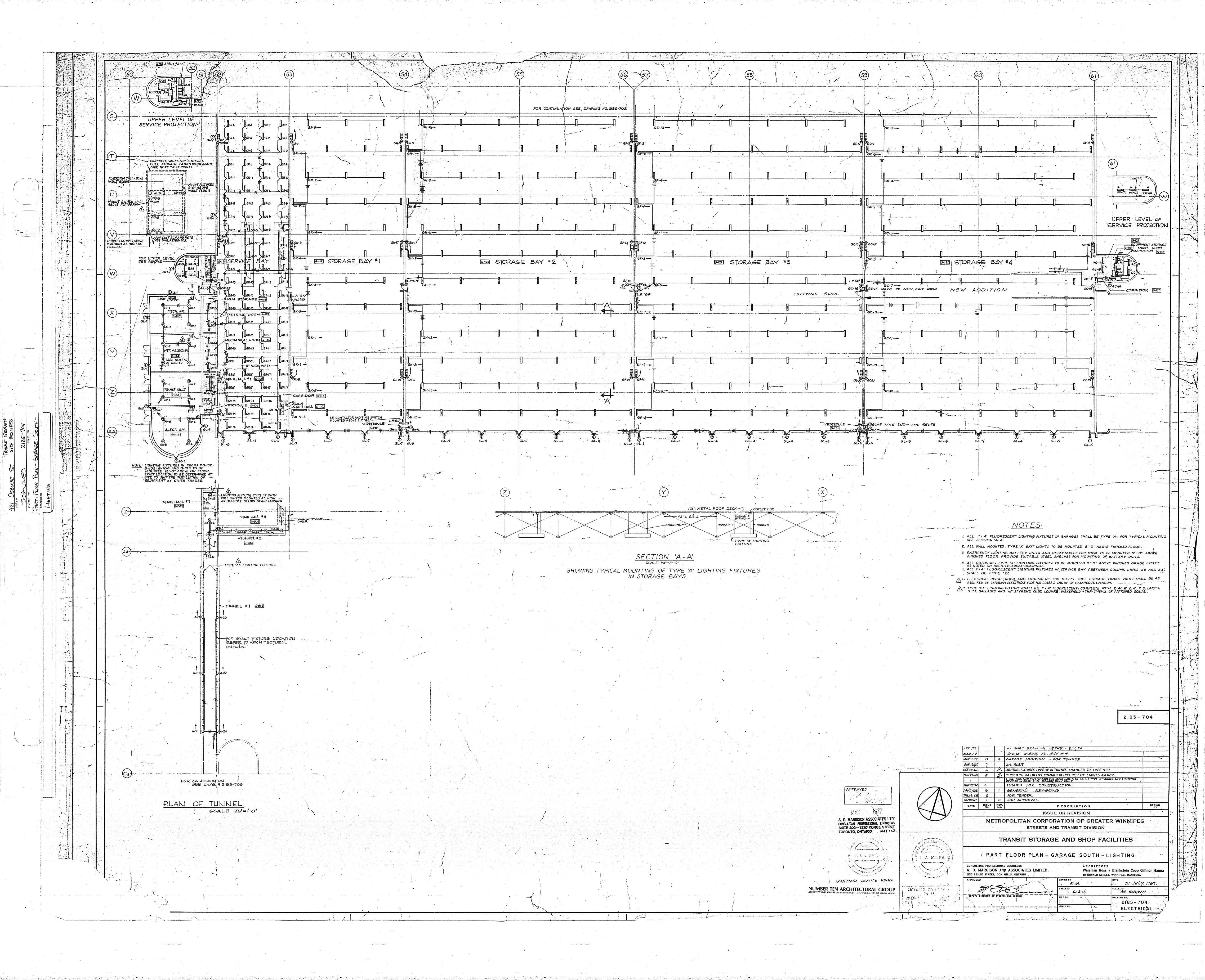
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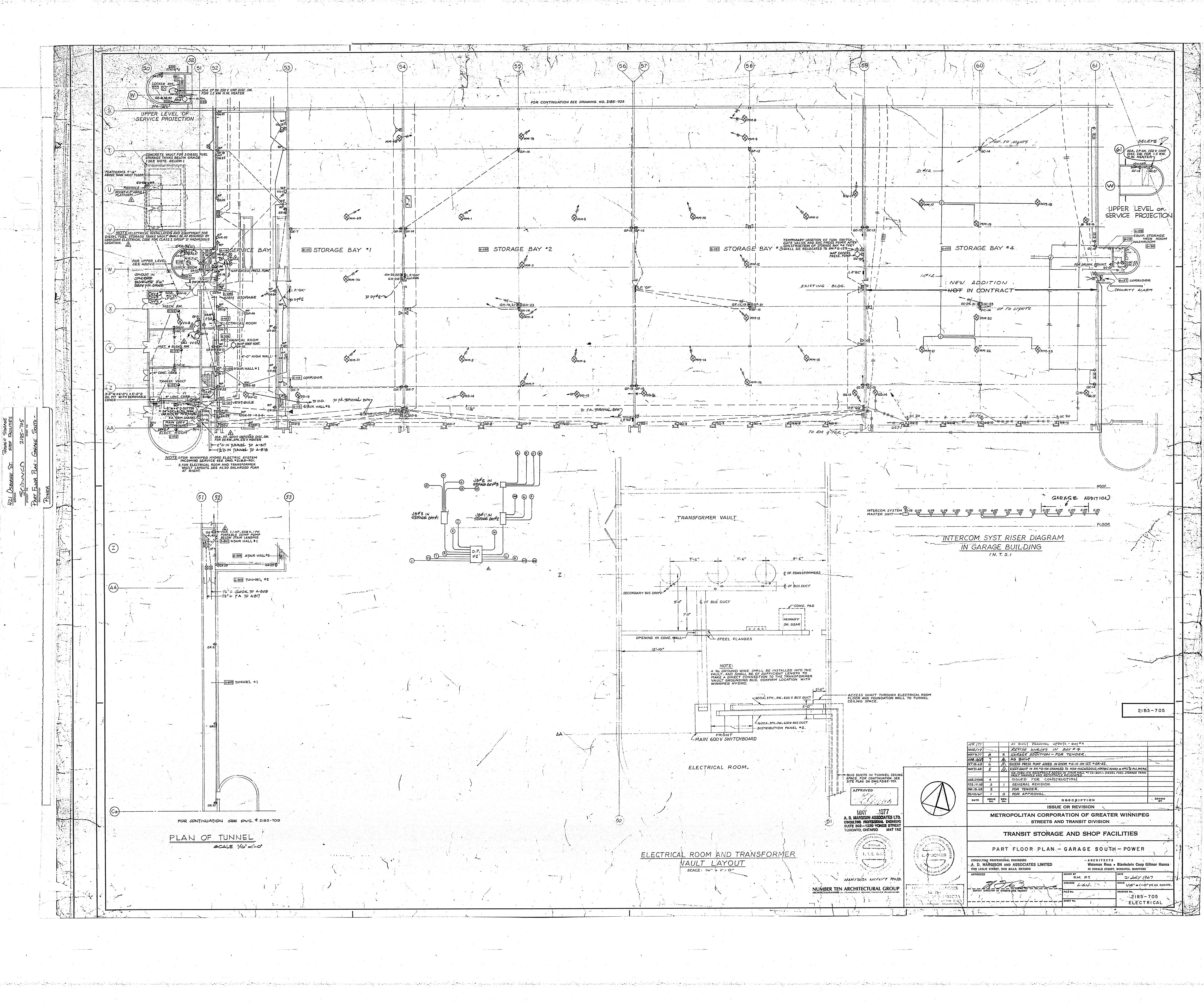
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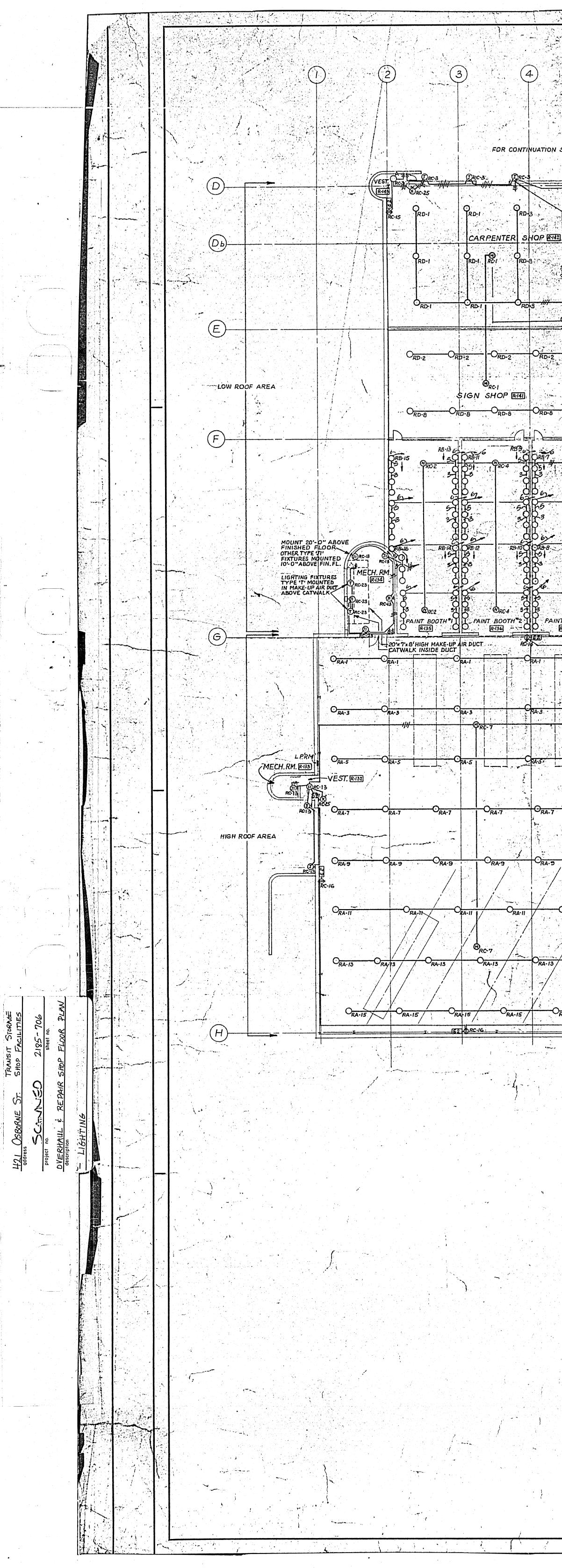
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•	NOTE: FOR NOTES, & TYPICAL MOUNTING DETAIL OF FLUORESCENT LIGHTING FIXTURES IN GARAGES SEE DRAWING NO. 2185-704.	
	APR. 17/77 AS BUILT DRAWING UPDATE - BAY #4 MAC, 79 REVISE WIRING IN BAY #4 MAY 9,77 7 4 GARAGE ADDITION - FOR TENDER MAR.1869 AS BUILT MAY 21.68. 5 2 DOOR & EXIT LIGHT ADDED ON WEST WALL BETWEEN COL. LINES R & S, EXIT LIGHTS ADDED.	
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L. G. JONES	TRANSIT STORAGE AND SHOP FACILITIES	
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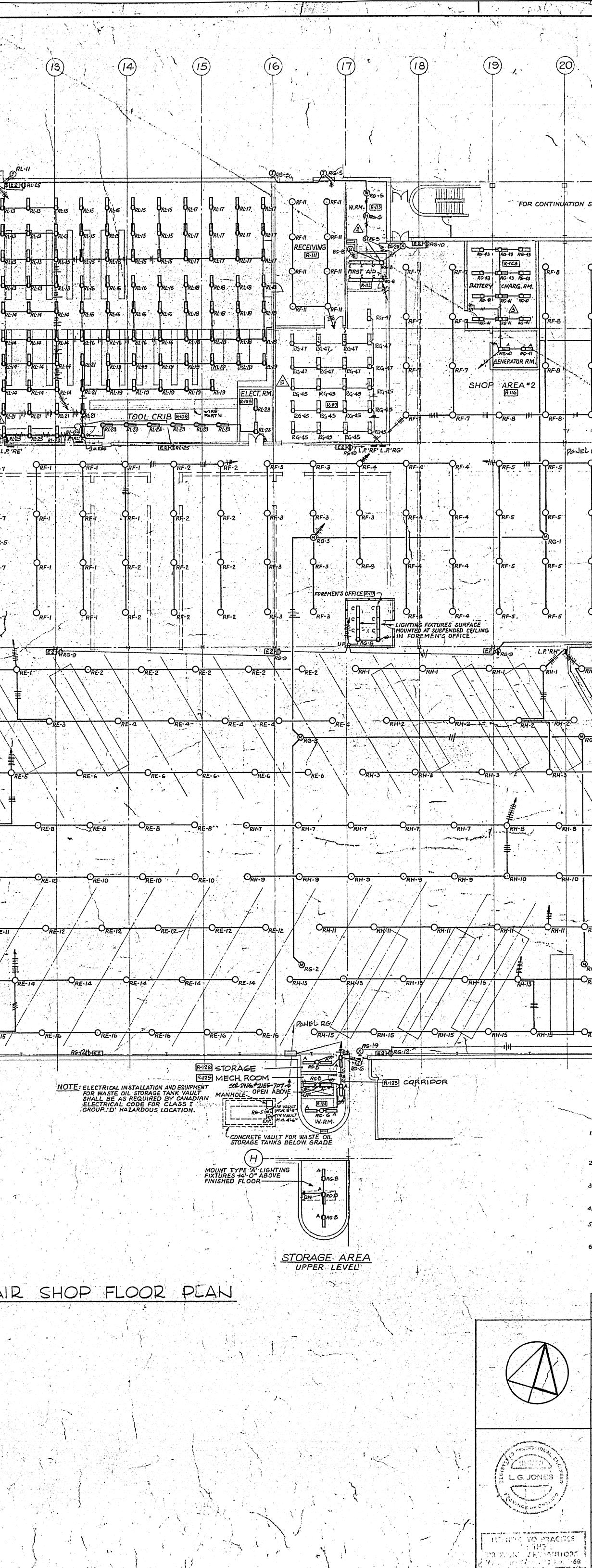
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SEE DRAWI	NG # 2185-708						(12) RI-11 D
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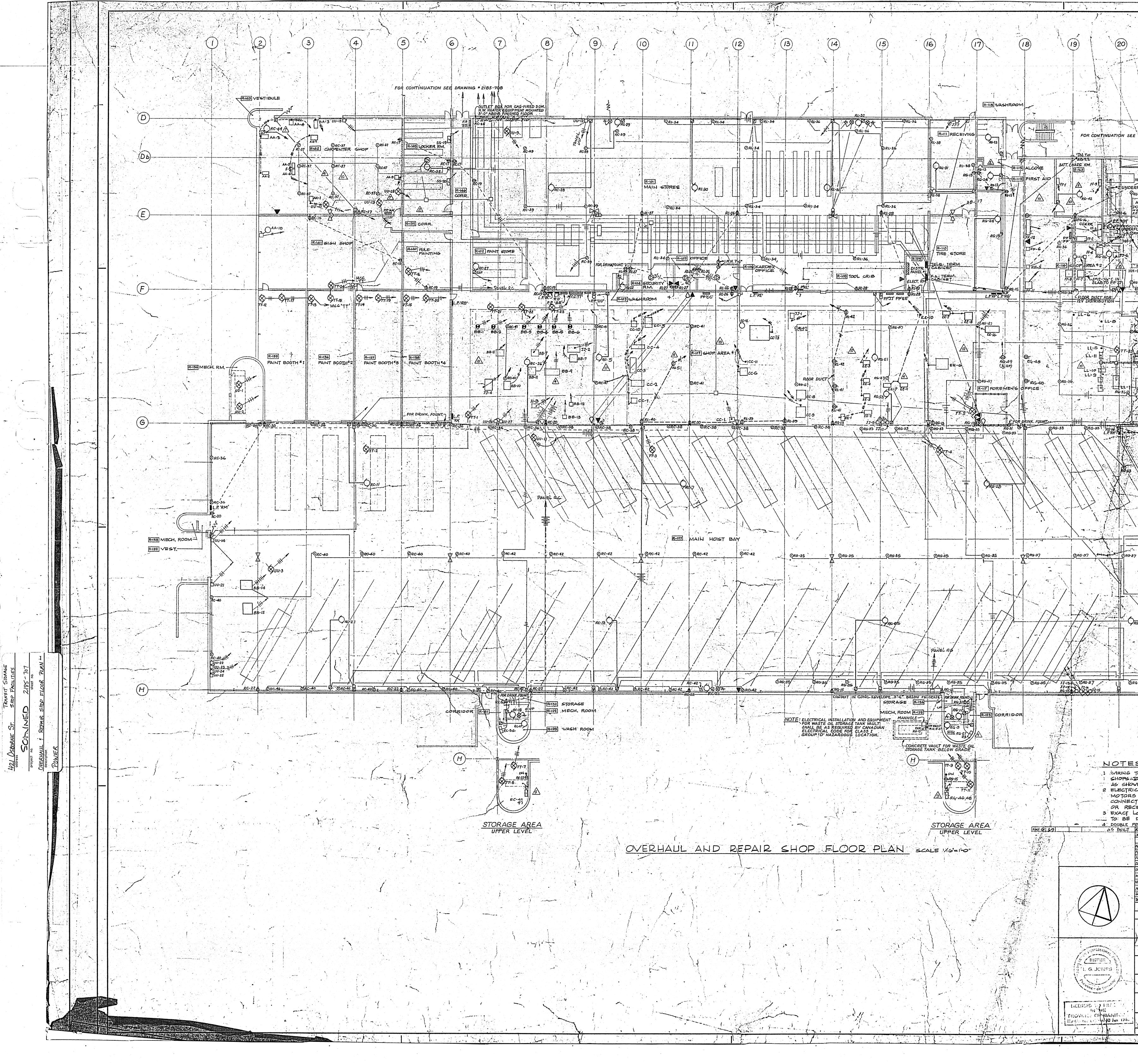
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LIGHTING FIXTURES TYPE 'A' CEILING MOUNTED IN OIL STORAGE-ROOM		
<u>NOTES:</u>		
I. ALL LIGHTING FIXTURES IN MAIN HOIST BAY (HIGH ROOF AREA) SHALL BE TYPE 'K' UNLESS OTHERWISE NOTED. MOUNT BOTTOM OF FIXTURE FLUSH WITH THE BOTTOM FLANGE OF BEAM.		
2. ALL LIGHTING FIXTURES IN SHOPS AND STORES (LOW ROOF AREA) SHALL BE TYPE 'L' UNLESS OTHERWISE NOTED, MOUNT BOTTOM OF FIXTURE		
FLUSH WITH THE BOTTOM FLANGE OF BEAM UNLESS OTHERWISE NOTED. 3. ALL LIGHTING FIXTURES IN PAINT BOOTHS SHALL BE TYPE 'P' UNLESS	tree a	
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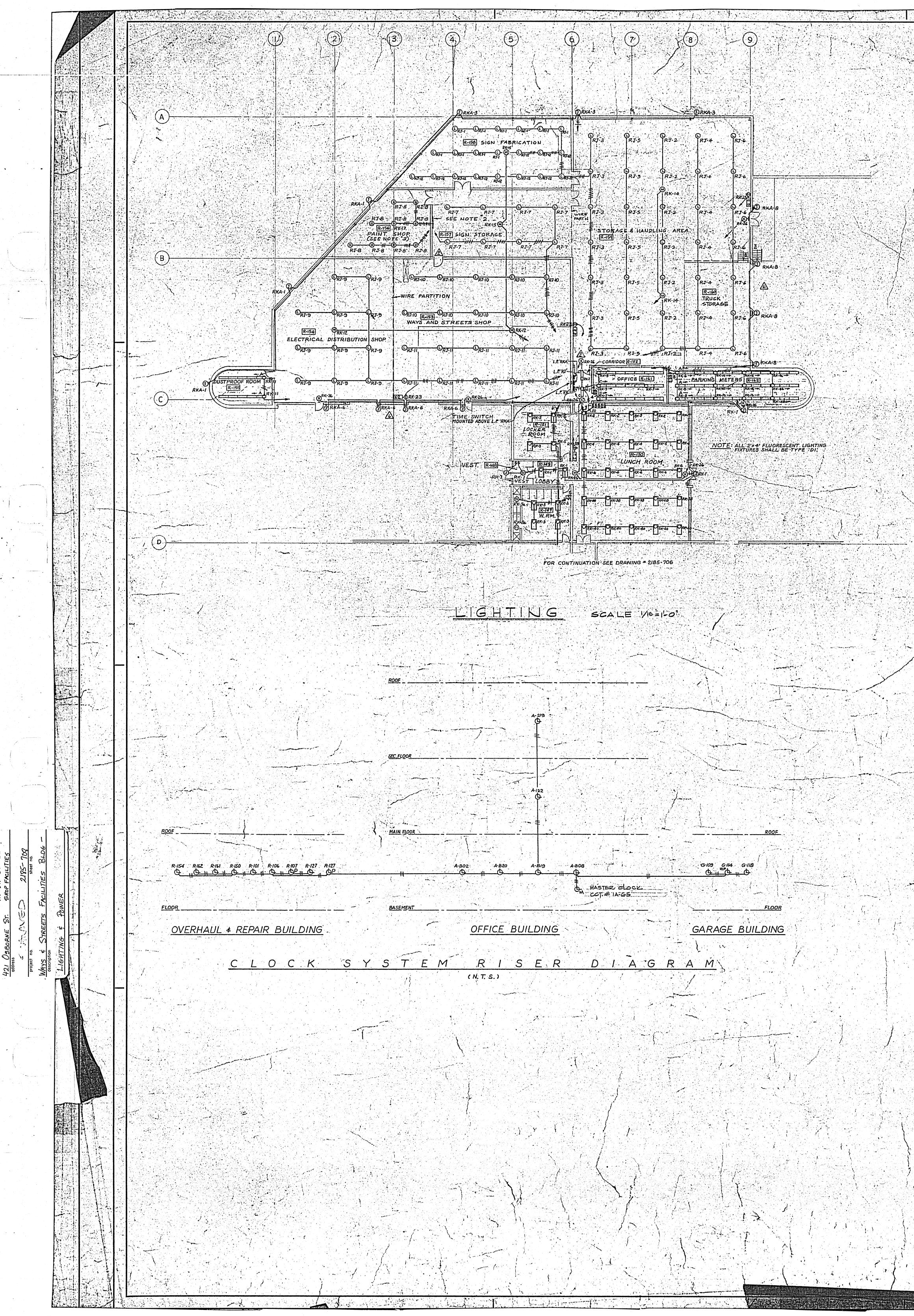


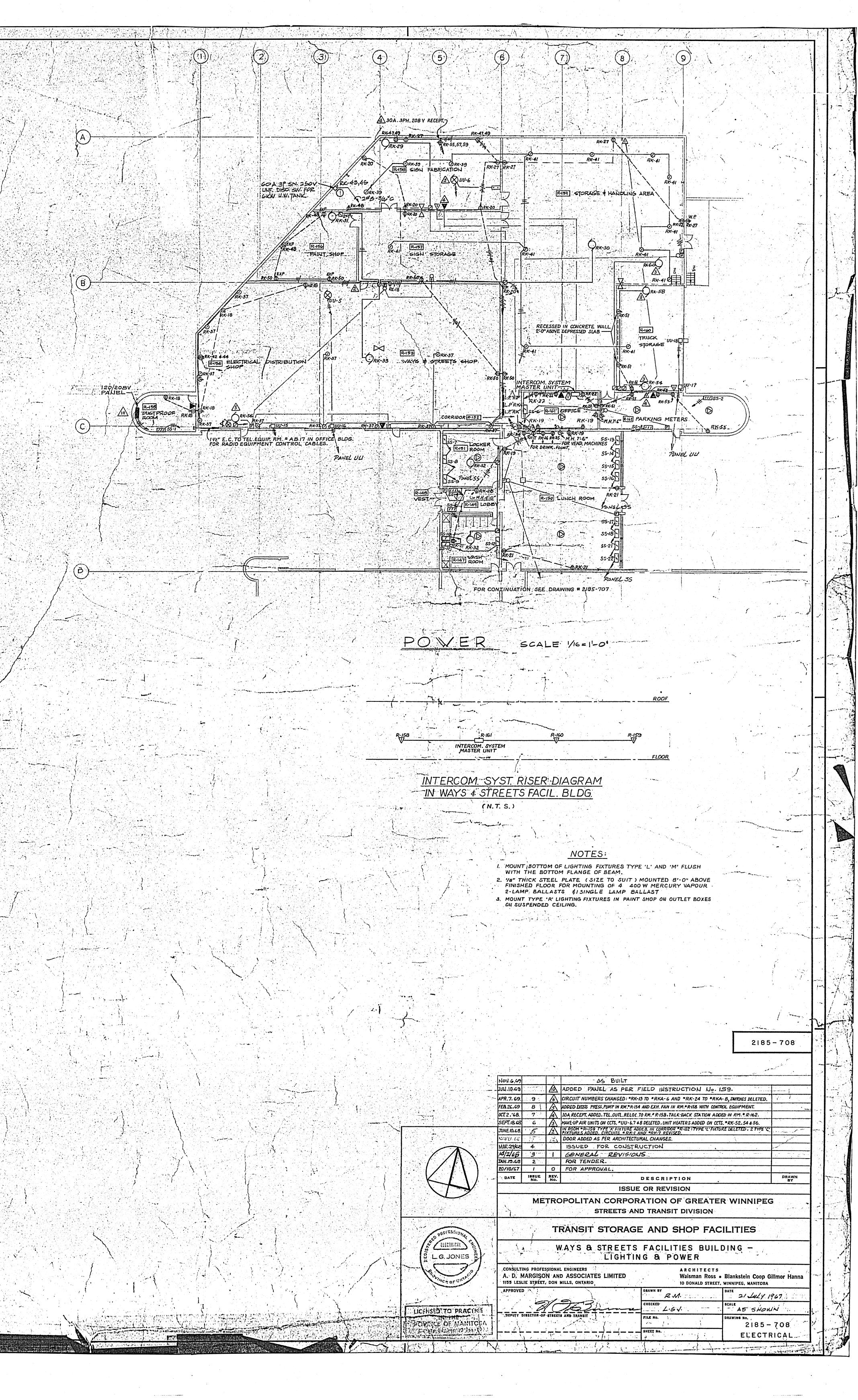
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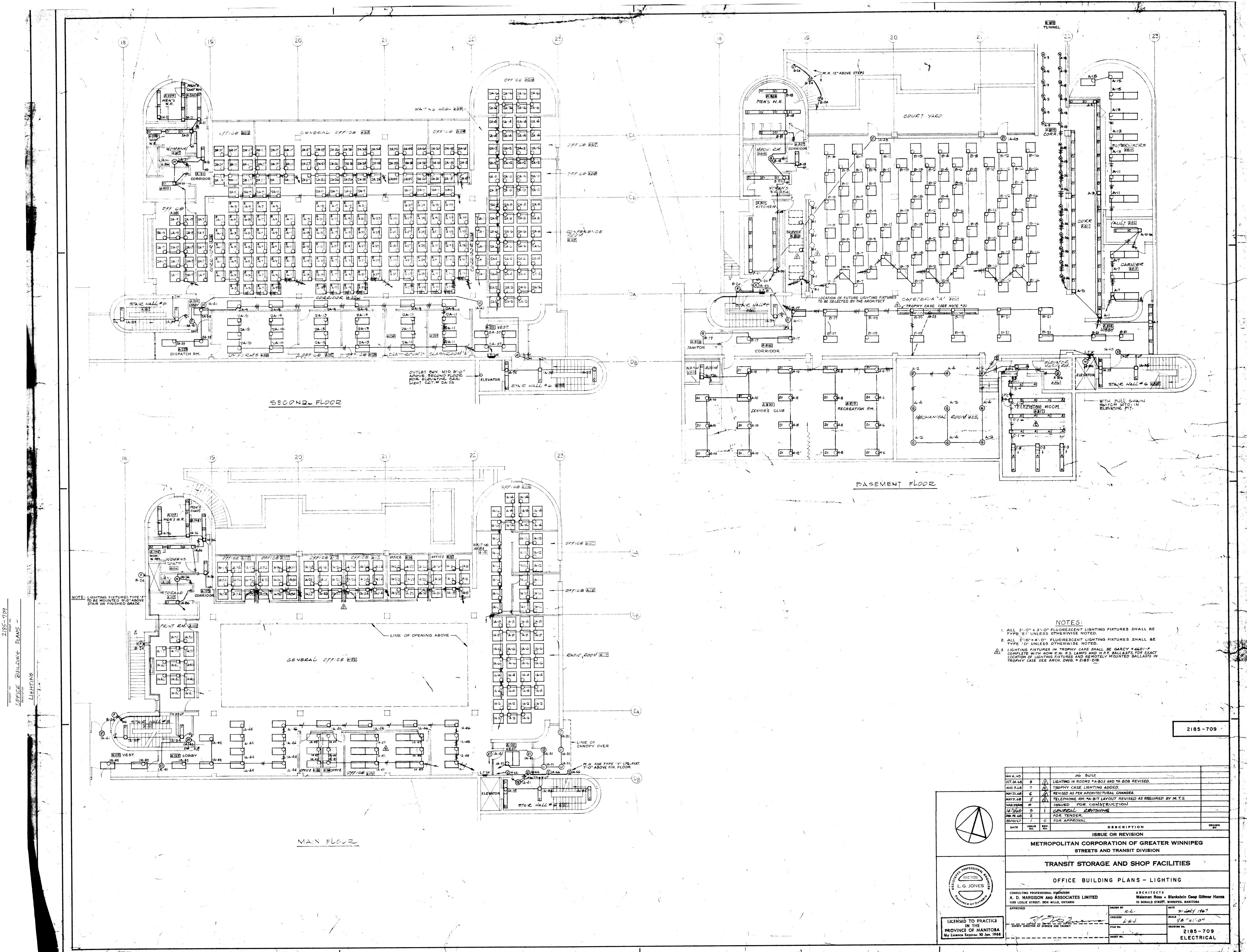
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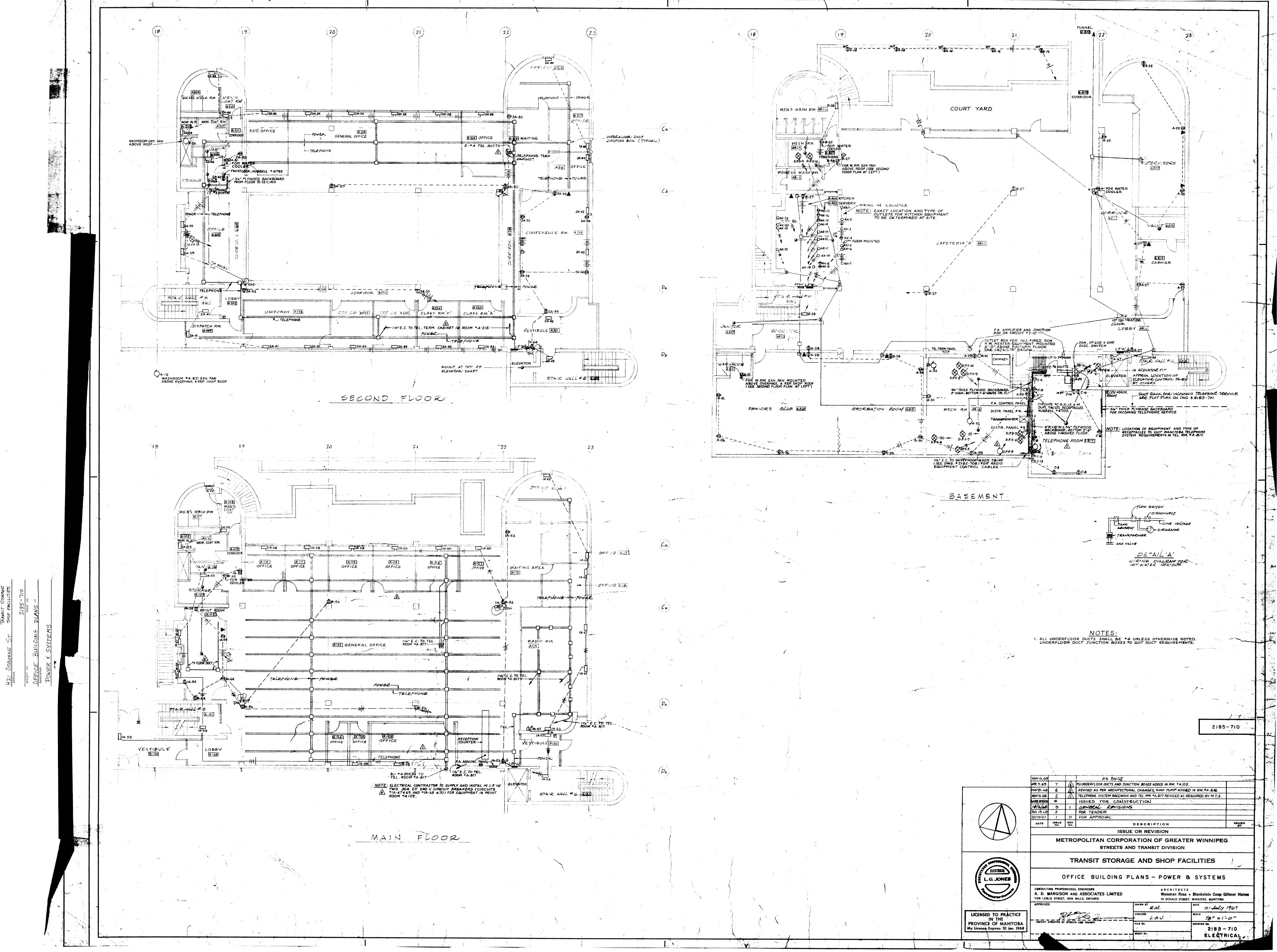


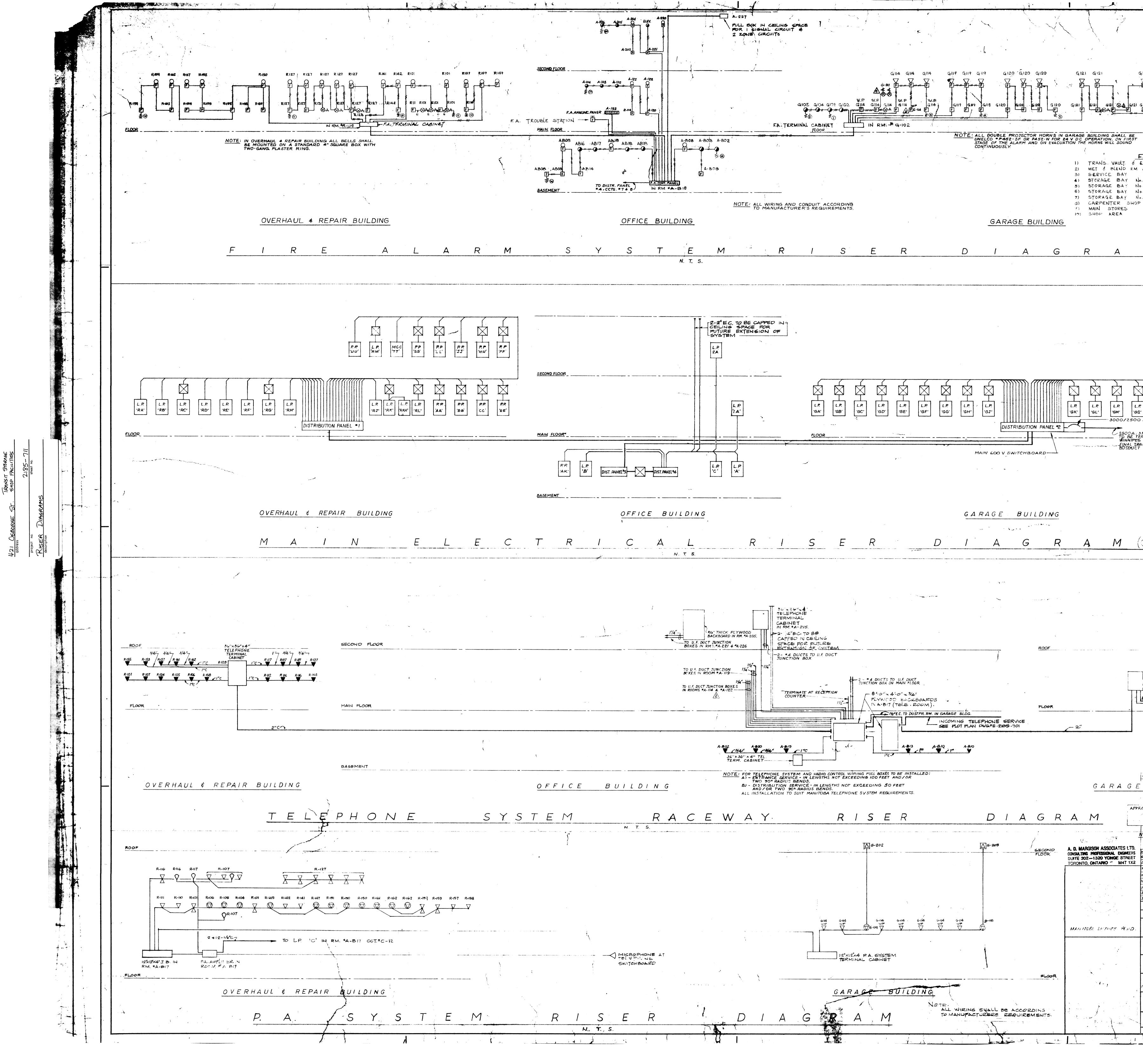
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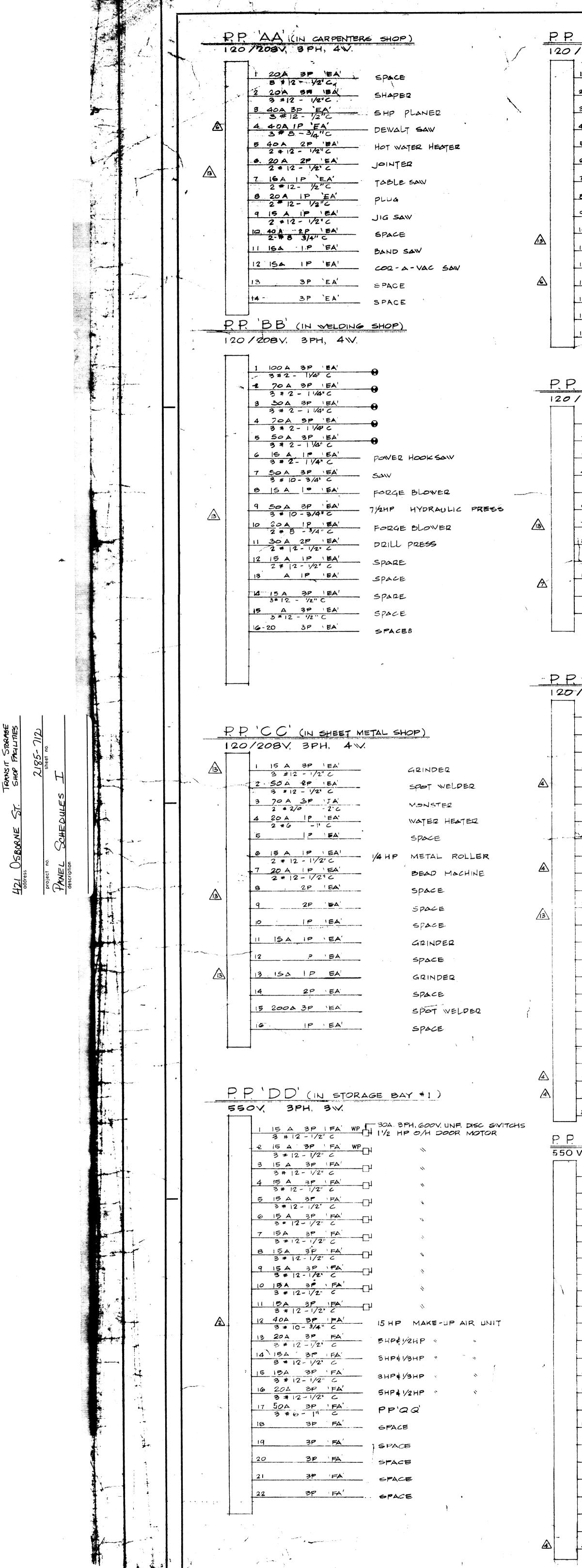


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EE' (IN AISLE OF	PADIATOR ROOMA)	P.P. 'KK' (IN STORAGE BAY \$1)	
12081. 3PH. 4W	POSITE RADIATOR ROOM)	550 V, SPH, SW.	
1 90A 3P (EA)	MICROSIPING MACHINE	1 154 3P 'FA' WP - 30A 3PH/600V. UNF. DISC. SVITCH 3 # 12-1/2" C - 11/2 HP O/H DOOR MOTOR	HS "
2 15A 1P 1 EA 2 # 12 - 1/2 C	PLUG	$\frac{2}{3 \# 12 - 1/2"} \frac{3P}{C} \frac{FA'}{C} \frac{WP}{D}$	÷
3 15 A 1P 1 EA 2# 12- 1/2" C	PLUG	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
4 20A IP ' BA' 2* 12 - 1/2" C 5 15A IP ' BA'	plua plua	3 + 12 - 1/2 C " 5 15A 3P 'FA' []	
2# 12-1/2" C G 20A P 'EA' 3# 8-3/4" C	SERING MACHINE	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	
7 15A 1P EA' 2 # 12 - 1/2" C	SEAVING MACHINE	7 15A 3P 1FA' 3# 12-1/2" C	
8 15A 1P 'EA' 2# 12- 1/2"C	BAND SAW	8 15A 3P 1FA' 3# 12-1/24 C	
9 20A 25 'EA' 26 12 - 1/2' C 10 15A 15 'EA'	SENING MACHINE	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	
2 + 12 - 1/2 C	Space	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
12 ISA IP EA	SEWING MACHINE	12 40A 3P PA' 15 HP MAKE-UP AIR UNIT	
13 2P EA'	SPACE	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
14 15A IP EA	JIG SAW	$3 \pm 12 - 1/2" C$ $3 \pm 12 - 1/2" C$ 15 20 A $3P$ (FA' 54Pd (B4P)	
16 304 2P EA	SAW FILE	$\frac{3 + 12 - 1/2" c}{16 20A 3P FA'} = 5HP \neq 1/2HP $	
	·	17 20A 3P 'FA' 5HPE/2HP	
	,	18 20A 3P 1FA' 5HP41/2HP \$ \$	
2084, 3PH, 4W	CAL SHOP)	B 20 15A 3P. 'FA' = 30A.3P. 600Y UNE DISC. SW.	
1 20A 3P EA	GRINDER	$ \begin{array}{c} \underline{5} \\ 3 = 12 - \frac{1}{2^{n}c} \\ 3 = 12 - \frac{1}{2^{n}c} \\ 1 = 3 \\ 21 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 5 \\ 5 \\ 5$	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	15 HP GENERATOR TEST	22 3P FA SPACE	
3 15 4 2P EA 3* 12 - 1/2" C	GLASS BEAD CLEANER	23 3P 'FA' SPACE	
4 40A 3P 'EA' 3# 8-3/4" C 5 15A 1P 'EA'	SPARE	24 3P FA SPACE	
2# 12- 1/2 C 6 15A 19 EA	plug plug		· • •
2* 12-1/2° C 7: 20A IP EA 2* 12-1/2° C	1/2HP SPEEDO TESTER		
18 15A 1P EA 2# 12-1/2" C	PLUG		
10 15 A 1 F 1 EA	SPACE	DD111' (ILLENGUE BEBUUT CLOB)	
11 1PEA'	PLUG SPACE	120/208 V. 3PH. 4W	
12. 15 A IP 'EA'	DRILL PRESS	1 20A 3P IEA CALIMESTER	
		2 20A 3P EA' PRESS	
1		A 20A I.P EA' SPARE	
CIN MACHIN	1E EHOP)	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
1208 (3PH. 4)		$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	
1 40A 3P 1 EA' 3# 12- 1/2" C	LATHE	7 154 10 EX - 1/4HP BORING MACHINE	
2 40A 3P 'EA' 3# 12-1/2" C	BATTERY CHARGER	8 15A IP 'EA' GRINDER 2# 12-1/2" C	
3 401 3P IEA' 3# 12- 1/24 C	3 HP LATHE	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3
4 30A 3P (EA' 3 # 12- 1/2" C 5 20A 3P (EA'	5 HP LATHE	II IBA IP EA'	~
34"E.C.3 6 30A 3P 1EA' 3# 12-1/2" C	GRINDER	2# 12-1/2" C VALVE BEINDER 12 15A 1 3P IEA' SURFACE MASTER	
7 15 A 3P EA' 3# 12-1/2" C	LATHE	13 15A IF EA SPACE	, , ,
2# 12-1/2" C	LATHE	14 IP EA SPACE	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5 HP LATHE FOR FUTURE USE	IC IP EA SPACE	
3/4" E.C	SPARE		
12 15A IP EA' 2# 12-1/2" C	1/3 HP DRILL PRESS		
13 15A IP EA' 2 # 12-1/2" C	FLOOR PLUG		
14 15 A 2P EA'	GRINDER		•••
2 # 12 - 1/2" C $10 201 IP EA'$ $2 # 12 - 1/2" C$	DRILL PRESS		
17 15A IP 'EA' 2# 12-1/2" C	1/4 HP DRILL PRESS	<u>P.P. 'NN (IN STORAGE BAY #3)</u> 550V. 3PH. 3W.	
18 304 IP EA 2#12-1/2" C	FLOOR PLUG	- 30A, 3PH, GOOV, UNF. DISC. SWIT	TCHES
19 15A IP EA 2# 12-1/2" C 20 15A IP EA	1/4 HP LATHE	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
$2 # 12 - 1/2" C^{7}$ $21 40A IP EA'$ $2 # 12 - 1/2" C$	HACK SAW HP LATHE (FUTURE)	$3 \pm 12 - 1/2"$ C. $3 \pm 12 - 1/2"$ C. $3 \pm 12 - 1/2"$ C. $3 \pm 12 - 1/2"$ C.	
2# 12-1/2" C 22 /5A IP EA 3/4" E.C.	DRILL PRESS	A ISA 3P FA -	ARAG
3/4" E.Q. V	• FOR FUTURE USE	3 15A 3P 'FA' 3 # 12-1/2" C	,
24 156 3P 'EA'	MILLING MACHINE	7 15A 3P 'FA' [] \\	. I. C.
JJ' (IN AISLE OPPOSI	TE RADIATOR ROOM)	$3 \pm 12 - 1/2$ C C	1. C.
V, 3 PH., 3W. 	eller O		1.C.
3 # 8 - 3/4" C 2 30A 3P 'FA'	SHEAR 10 HP 12×6 HAMMER	3 # 12-1/2" C	I. C.
3 # 12 - 1/2" C 3 30 A 3 P 'FA' 3 # 12 - 1/2 " C	IO HP GRINDER		I.C.
4 50 A 3P 'FA' 3* 10 - 3/4" C	LATHE	12 16A 3P FA 3 # 12-1/2" C V N 13 20A 3P FA' 5HP41/3HP MAKE-UP AIR UNIT	I.C
5 30A 3P 'FA' 3 = 12 - 1/2" C 6 15A 3P 'FA'	BUS HOIST	3 # 12 - 1/2" C = C = C = C = C = C = C = C = C = C	
3 # 12 - 1/2" C 7 30A 3P 'FA' 3 # 12 - 1/2" C	BUS HOIST	IS 25A 30 LEA!	1. C.
8 A 3P 'FA' 3*12 - 1/2 " C	BUS HOIST		I.C. •
$3 \neq 12 = 1/2 \cdot C$	THE BUS HOIST	$\frac{17 \ 20A \ 3P \ FA}{3 \ # \ 12 - 1/2' \ C} \ 5HP = \frac{1}{2HP} $ $18 \ 20A \ 3P \ FA'$	10
3712-11/2" C 11 30A 3P 'FA'	☐ 7½HP " " ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓	$3 \pm 12 - 1/2^{+}$ C 19 20A 3P $+ FA'$	1.C. 1.C.
3 7 12 - 1/2" C	☐ 7 1/2 HP ··· ··	$3 \pm 12 - 1/2$ C $20 \ 20A \ 3P \ FA' \ 5HP \pm 1/3HP \ 11$ $3 \pm 12 - 1/2$ C	
13 ICA 3P 1/FA' 3 # 12 - 1/2 !! C	Dee 2	21 3P 'FA' SPACE	
5 # 12 - 12 6	CRANE	22 <u>3P FA</u> SPACE	
3# 12 - 1/2" C 16 15A 3P 1FA	CRANE	23 3P FA SPACE 24 3P FA' SPACE	
3 + 12 - 1/2" C 17 304 3P FA' 3 = 12 - 1/2" C	BUS HOIST		
3 = 12 - 1/2 = C 18 15 A 37 FA' 3 = 12 - 1/2 = C	1 2, 1/2 # 1/3 HP CRANE		
19 15A 3P FA 3# 12 - 1/2 " C	GRINDER		
20 15 A 3P FA' 3 F 12 - 1/2 " C 21 - 1/5 3P FA'	TH DOOR		•,
=/4" E.C. → 22 /5A ¥P 'FA'	FOR FUTURE USE FOR FUTURE USE		ł
3/4" E.C. 23-28 3P. 'FA'	- SPACES	1	and the second se

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			······) () () () () () () () () () () () () ()		<i>;</i> /	,				`		X
F	<u>P</u>	'QQ' (IN STOR	AGE BA	Y # 3)			$\langle \cdot \cdot \rangle$		L	IGH	TIN	16	PAN
5	550	D√. 3 PH, 3√.					PANEL	LOCATION		ITING			15A, I
		1 15A 3P 'FA' FA' J	- 30A. 3M.	600V. UNF. Q	MOTOR'		'S A'	GARAGE	~				24
		3 # 12-1/2" C	- 1/2 111 -			ŝ	'G B'	A A	~				27
		2 15A 3R 'FA' 3 # 12-1/2" C	َ ل	A / T	5	5 []	'G C'	4	~		J	,	28
				2		/	'G D'		~		~	1×10^{-1}	18
		3 15A 3P 1FA 3# 12-1/2" C	J	•			'G E'	* 2			~	7	18
		• •					'6 F	• 7	~		1		22
		4 15A 3P 'FA' 3 1 12-1/2" C	1 <u>}</u>	1 GARAGE	ADDITION		'GG'	•	~		1		24
			1				'GH'	*	~		~		24
	1	5 15A 3P FA	-			1	'6 J'	*	~		~		12
		G 15A 3P FA'	1	1. 1	N. K		'GK'	•	~		1		10
		3 # 12-1/2" C				1	GL		~		~		20
		7 15A 3P FA'	L	*	N. I.C.	1	'G M'	* /	~	N.,	1		20
						1	GQ'	*		~	1		31
		8 15A 3P FA'	L	*	N.I.C.	Δ	'GR'	4	~		1		40
		0 154 30 154'	,				'6 S'	*	~		~		48
		3 # 12 - 1/2" C	-	*	N. I.C.	1	'RA'	OVERHAUL & REPAIR	~			~	
	1	10 15A 3P 1FA	1	*	N.I.C.		'R B'	•	~			V	-
		3# 12-1/2 V C -	,	x			'R C'	*	-		~		46
		11 15A 3P FA 34 12-1/2" C	1	*	N. I. C.		'R D'	× ×	~				
							'R E'	*	1			~	
		12 15A 3P 1FA' 3 # 12-1/2" C	L	*	N. T. C.		'R F'	*				~	
		13 20A 3P 'FA'					'RG'	1	~		~		42
•		3 # 12 -1/2" C	5HP=1/2H	IP MAKE-UP	AIR UNIT		'RH'	\	V			~	
		14 20A 3P 'FA'					'RJ'	WAYS & STREETS FACILITIES BLDG	~			~	-
		3 + 12-1/2" C		*	N. I. C.	$ \mathbf{A} $	'RK'	*	V .		1		51
		15 20A 3P FA'		*	N.I.C.		'R L'	OVERHAUL & REPAIR	×				42
	1	3 # 12-1/2 C		•			'R M'	N	×		<u> </u>		36
		16 20A 3P 'FA'		*	N. I.C.		<u>'A'</u>	ADMINISTRATION			1		42
		3# 12-1/2" C					'B'	*	ļ		~		32
		17 3P ' FA'	SPACE		1	2	'C'	+	L				14
		18 3P 'FA'	_				1A	•		~	~		72
			Space				24			<u> </u>			48
		19 3P FA'	SPACE	\mathcal{N}			'RKA'	WAYS & STREETS FASCILITIES BLDG	t	 			B
	1						'GT'	IN GARAGE, MECH. RM.	×	<u> </u>	Y		<u>60</u>
		20 3P 'FA'	GPACE				'GU'	IN GARAGE, ELECT. RN. G-102	×		· ·		16
				,						1	1		

P.P. 'SS' (IN CORRIDOR #R-146) 120/2081. 3PH. 4 .

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20		208	V.	3PH,	4 🔌	\sim		
	1	70A 3 * 4-	3P	EA	20	K₹	HEATE	R
	2	50A 3 # 6-			15	ĸw	K	
	3	50A 3 # 6	3P -1"	C EA'	15	K v	N	
	4	30A 3 # 10	3P - 3/4"	EA'	6	ĸ₩	N	
	5	30A. 3 # 10	3P - 3/41	<u>'EA'</u> C	6	ĸw	*	
	6	1		6	з	ĸ₩	*	
	7	30A 2 # 10	2P 1 -3/4	EA' C	4	K≪	*	
	B	30A 2 + 10	•		4	Kv	*	
	<u>q</u>	30A R # 10	2P - 3/4"	C EA'	4	K∾∕	*	
	10	30A 2 # 10	2P - 3/4"	EA' C	4	ĸ₩	*	
	11	30A 2 # 10	- 3/4"	C	4	K \¥		
	12	30A 2 # 10		/	4	ĸ₩	*	
-	13			C	3	K₩	*	
. /.	14	-		EA'	3	K₹	۲	
ŕ	15	204 12			3	K₩	*	
4	16	2 # 12	- 1/2"		. 3	κw	*	
-				EA'		K₹	*	
-		20A 2 # 12			3		•	
•				EA'		κw	4	
./	1					XV	*	
-	('EA' C		κw	п	
•				<u>'EA'</u> C FA	-	KW	••	
		100 A 4. # 2 - 28				ANEL	- · , ·	Δ
			<u> </u>		9	PAC	ES.	

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GARAGE ADDITION

N. I.C. N. I.C. N. I. C. N. I.C. N. I.C. N.I.C.

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E	15A, IP	and an an and the state of a	R BREAK	and the second	NO: IP SPACES	FOTAL	REMARKS	-
	1/7, 17	13A 2P	20A 1 P	20A 2P	(OTHERS NOTED)	IPOLES	NEMIAR NO	- 7
	24	. 1	-		4	3 0		
	27	1 -	1	1 (20A 3P)	4	36		
	28	2	1	1 (20A 3P)	6	42		
1	18	1	1		4	24	÷	
1	18	1			4	24		÷ . ,
	22	2			4	30		A.
	24	- 2			- 2	30	· · · · · · · · · · · · · · · · · · ·	
٦	24	2	<u> </u>		2	30		
	12	1	,		4	18		
	10		·		2	12		
	20		at .		4	24	OPERATED BY TIME SWITCH	
	20				4	24	11 13 10 pt	
	31	1(30A2P)		1(70A 3P)	6	36		
	40	1(15A.2P) 1(30A, 2P)	1	1(70A 3P)		48	DOUBLE STACKED	
	48					48	DOUBLE STACKED	·
		20			4(2P)	24		
		20			4 (2P)	24		
	46	7		2		48	DOUBLE STACKED	· · · ~
		14		•	4(2P)	18		
		20			4(2P)	24	·	
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	42			2	4	48	DOUBLE STACKED	2
		20	• *		4 (2P)	24]
·		14	х. 	1	4 (2P)	18	· · · · · · · · · · · · · · · · · · ·	. .
	5 t	2	1-30A,3P.	1(40A2P)		60	DOUBLE STACKED	
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	36					36		
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	72			L	12	84	DOUBLE STACKED	1
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	B				4	12	OPERATED BY TIME SWITCH	ł
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	16				2	18		1

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APE/77 AV BULT PRAVILLA STVATE - BAL#4

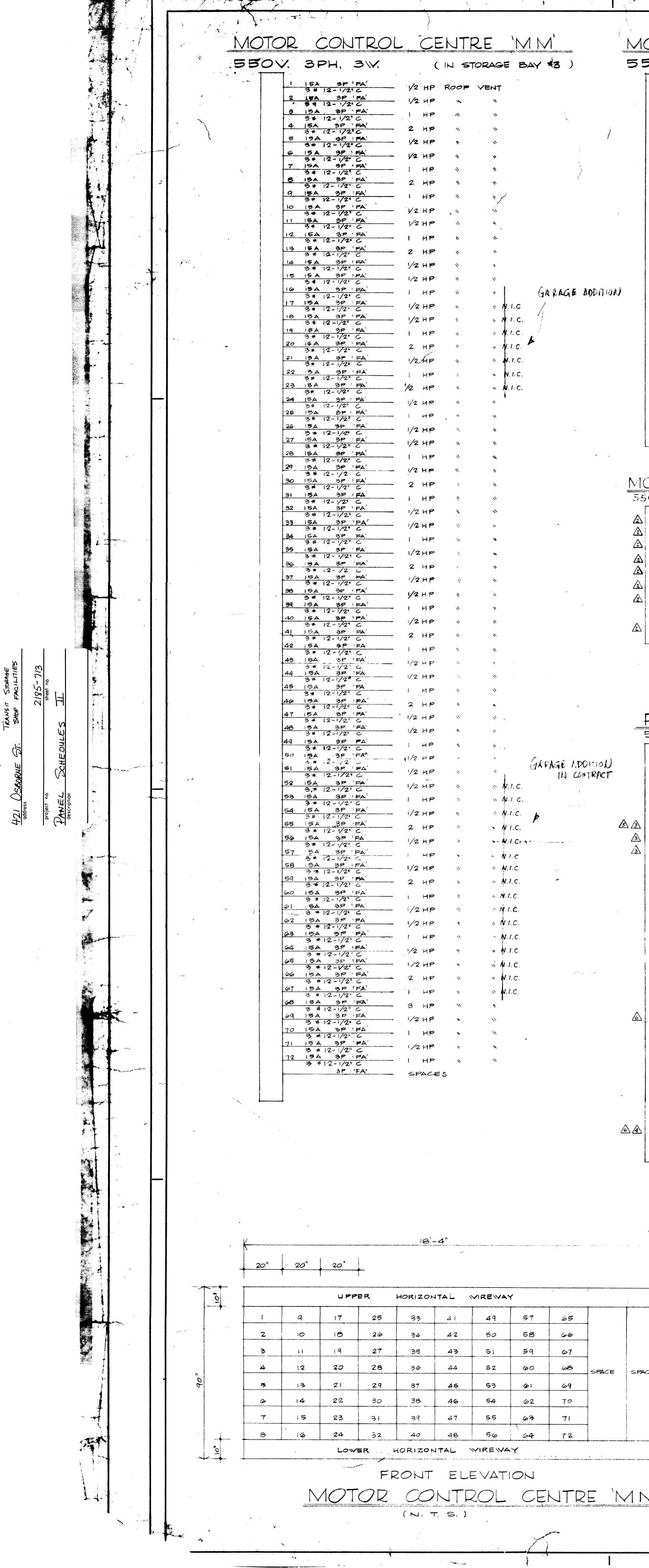
NUMBER TEN ARCHITECTURAL GROUP ARCHITECTS & PLANNERS 210-175 HARGRAVEST WINNIPEG: CANADARIC 3R9 (204) 942 (1941 2185 - 712 MAY 9,77 12 14 GARAGE ADDITION - FOR TENDER _____ Nov 6,69 11 AS BUILT A REVISED AS PER OWNERS EQUIPMENT RELOCATIONS & DELETION 30-69 مالال 17.69 مالال ADDED 20A 2P BRES TO PANEL RC & RG A. D. MARGISON ASSOCIATES LTD. CONSULTING PROFESSIONAL ENGINEERS SUITE 302-1320 YONGE STREET I GROWTO, ONTARIO MAT 122 CT.IB. 68. 7 A SPIEA RELAVED THE STREET OCT.IB. 68. 7 A BREAKERS AND EMPTY CONDUITS ADDED ON CCTS. "HH-5,10,22.23."J.J. 21 4 22. OCT.2.68. 6 /3 'RK' PANEL SCHEDULE REVISED. CIRCUIT # DD-12 AND L.P. 'GR' & 'C' REVISED. MAY 9,68. ISSUED FOR CONSTRUCTION MAR. 27/68 4
 MIND 27/60
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 DE
 BRAWN DESCRIPTION ISSUE OR REVISION METROPOLITAN CORPORATION OF GREATER WINNIPEG STREETS AND TRANSIT DIVISION TRANSIT STORAGE AND SHOP FACILITIES PANEL SCHEDULES I акснітест**s** Waisman Ross • Blankstein Coop Gillmor Hanna CONSULTING PROFESSIONAL ENGINEERS A. D. MARGISON AND ASSOCIATES LIMITED 10 DONALD STREET, WINNIPEG, MANITOBA 1155 LESLIE STREET, DON MILLS, ONTARIO APPROVED DRAWN BY' 21 JULY 1967 DEPUTY DIRECTOR OF STREETS AND TRANSIT L.G.J. N. T. S. DRAWING No. FILE NO. 2185-752 ELECTRICAL



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		A	
MOTOR CONTROL CENTRE / TT'	DISTRIBUTION PANEL #1	DISTRIBUTION PANEL *3	POWER PANEL 'AK'
5) 550V. 3PH. 3V. (IN OVERHAUL & REPAIR SHOP)	550V. 3PH. 3W. (IN ELECTRICAL ROOM * R-109)	550 V. 3PH., 3W. (IN MECH. RM. *A-BIB)	120/208 V, 3PH., 4W. (IN KITCHEN "A-BO2)
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	3 + 2 - 1'/4"C KOA 3P 'FA'	$\frac{1}{3} \frac{15}{12} - \frac{37}{12} \frac{15}{12} \frac{15}{$	I ISA IP 'EA' CASH REGISTER 2 ISA IP 'EA' V3 HP DRINK DISPENSER 2 IZ 'Y2" C 'Y3 HP DRINK DISPENSER 3 20A IP 'EA' 2 IP 'EA' 'Y3 HP DRINK DISPENSER 3 20A IP 'EA' 2 IZ 'Y2" C 'I.6 KW COFFEE WARMER
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3 15A 3P 'FA' 2-2 HP SUMP PUMP	2*12 - 1/2* C 4 20A IP 'EA' 2*12 - 1/2* C 5 20A IP 'EA' 2*12 - 1/2* C 5 20A IP 'EA' 2*12 - 1/2* C 5 20A IP 'EA' 2KW HOT FOOD UNIT
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	40A 3P 'FA' 3 # 8-3/4'C' L.P 'RD'	4 15A 3P 'FA' SPAKE	2 #12 - 1/2" C <u>6 20A IP 'EA'</u> 2KW H H H 2#12 - 1/2" C <u>7 15A IP 'EA'</u> 2KW H H H <u>2</u> #12 - 1/2" C <u>2</u> #12 - 1/2" C
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5 225A 3P 'JA' 150HP CHILLER 3 # 3/0 - 2"C	$\frac{2 \cdot 12 - \frac{1}{2} \cdot C}{\frac{15}{4} - \frac{17}{2} \cdot \frac{C}{2}} = \frac{12 \cdot \frac{1}{2} \cdot \frac{1}{2}}{\frac{15}{4} - \frac{18}{2} \cdot \frac{18}{2} \cdot \frac{18}{2} - \frac{18}{2} \cdot 1$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$3 + 4 - \frac{1}{4}$ C $70A 3P FA'$ $45 4 + \frac{1}{0} - 2$ C LP RF	6 30A 3P 'FA' 71/2 HP CIRC. PUMP 3# 12 - 1/2"C 71/2 HP CIRC. PUMP 7 30A 3P 'FA' 71/2 HP " "	2=12 - 1/2" C 10 15 A 3P 'EA' 3=12 - 1/2" C 11 70 A 3P 'EA' 3=4 - 1/4" C //2" //2" //2" //2" //2" //2" //2" /
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\frac{100A \ 3P \ FA'}{3 \ # \ 2 \ -1'/4'C} = LP \ 'RH'$	B 30A 3P 'FA' IO HP A/C UNIT	12 40A 3P 'EA' 12 KW FRYER 3*8 - 3/4*C 13 20A 3P 'EA' 5.2 KW HOT PLATE
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\frac{70A}{3 \mp 4 - \Gamma'_4 C} = L.P. RJ'$	9 15A 3P 'FA' 2HP RETURN AIR FAN 3#12 - '/2" C	14 20A 3P 'EA' G KW COFFEE MAKER 3#12 - '/z" C
AGE 4001101) 16 15A 3P FA 3# 12-1/2"C 17 30A 3P FA 3# 12-1/2"C 7% HP N N	$70A$ 3P FA' 45 $4 + \frac{1}{0}$ $-2"C$ LP RK' $3 + 4 - \frac{1}{4}$ 45 $4 + \frac{1}{0}$ $-2"C$ LP RK' $70A$ 3P FA' 45 $4 + \frac{1}{0}$ $-2"C$ LP $'RKA'$ $70A$ 3P FA' 45 $4 + \frac{1}{0}$ $-2"C$ LP $'RKA'$ $3 + 4 - \frac{1}{4}$ 45 $4 + \frac{1}{0}$ $-2"C$ LP $'RL'$	10 15 A 3P 'FA' 3/4 HP CIRC. PUMP	16 15 A 1P 'EA' 16 HP MILK DISPENSER 2#12 - 1/2" C 17 15 A 1P 'EA' 1/4 HP ICE CREAM 2#12 - 1/2 " C
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	<u>3#12 - 72"C</u> 3HP A/C UNIT <u>12 15A 3P 'FA'</u> <u>72 HP CIRC. PUMP</u> <u>3 #12 - 72"C</u>	<u>18</u> 70A <u>3P</u> 'EA' 21.5 KW RANGE <u>3 # 4 - 1/4" C</u> <u>19 15 A <u>3P</u> 'EA' I HP DISHWASHER <u>3 # 12 - 1/2" C</u></u>
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\frac{150ABP 'JA'}{3 * 1/0 - 2"C} = \frac{1121/2}{1121/2} \frac{2 \times (4 + 2/0 - 21/2"C)}{2 \times (4 + 2/0 - 21/2"C)} P.P. 'BB'$	13 15 A 3P 'FA' 2 HP KITCHEN EXH. FAN	20 20A 3P 'EA' 5 KW HEATER 3*12 - 12" C 21 30A 3P 'EA' 9 KW BOOSTER 3*10 - 14" C
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\frac{150A3P}{3 \pm 1/0} \frac{JA}{-2^{\circ}C} \frac{1121/2}{1121/2} \frac{2\times(4 \pm 2/0)}{2\times(4 \pm 2/0)} \frac{-21/2^{\circ}C}{PP} CC'$	14 30 A 3P 'FA' 10 HP ELEVATOR	22 15A 3P 'EA' IV2 HP WASTE DISPOSER 3#12 - 1/2" C 23-30 3P 'EA' SPACES
$ \begin{array}{ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	15 350 A 3P 'LA' 300 3×(4 = 300 MCM-3"C) D.P. = 4 2×(3 = 2/0-2"C) GOO V Δ-120/20B V Y, 3PH., 4W. TRANSFORMER 16-24 3P 'JA' SPACES	
SPACES	TOA 3P FA $3 \neq 4 - 1/4^{"}$ C 45 $4 \neq 1/0$ $-2"C$ P.P. 'FF' $70A = 3P$ FA' 45 $4 \neq 1/0$ $-2"C$ P.P. 'FF' $70A = 3P$ FA' 45 $4 \neq 1/0$ $-2"C$ P.P. 'HH' $3 \neq 4 - 1/4"$ 45 $4 \neq 1/0$ $-2"C$ P.P. 'HH'	SPACES	
MOTOR CONTROL CENTRE 'VV'	$\frac{225 \land 3P 13A'}{3 \ # \ 4/2 \ - 21/2"C} PP \ 'JJ'$		
550V 3PH. 3W (IN MECHANICAL RM. #G-105)	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	DISTRIBUTION PANEL #4	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\frac{200A 3P}{3 \# 3/0} - 2C \qquad 150 \qquad 2 \times (4 \# 4/0 - 5"C) \qquad P.P. 'SS'$ $\frac{125A 3P}{JA'} \qquad 150 \qquad 2 \times (4 \# 4/0 - 5"C) \qquad P.P. 'SS'$	120/208 V, 3PH, 4 W (IN MECH. RM. #A. BIB)	
$\begin{array}{c} 2 \\ \hline 3 \\ \hline 12 \\$	3 # 1 - 11/2" C MOIOR CONTROL CE 704 3P FA' 4# 1/0 2"C L.P. 'RM' 3 # 4-11/4" C	VIRE II' <u>1 150A 3P 'JA'</u> L.P. 'A' <u>4 * '/o - 2"C</u>	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	225A 3P 'JA' 3 #4/c -21/2"C P.P. 'UU'	2 125A 3P 'JA' L.R (B' 4 #1 - 2"C	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	B - 3P 'JA' SPACES	$\frac{3}{4} \frac{70 A}{4} \frac{3P}{4} \frac{'JA'}{LP} \frac{LP}{C'}$	
SPACES		$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
		$\frac{6}{4*4/0} = \frac{275}{3P} + \frac{3P}{3N} + \frac{3P}{2} + 3$	
		17 20A 1P 'EA' 2*12 - 1/2"C F.A. SYSTEM	
550V. 3PH. 3W. (IN OVERHAUL & REPAIR SHOP)		$\frac{B}{2^{\#}/2} - \frac{1P}{2^{\#}/2} - \frac{1EA'}{2}$	
IN CONTRACT	1	2#12 - 1/2"C 10-16 3P 'JA' SPACES	
$ \begin{array}{ccccccccccccccccccccccccccccccccccc$			
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	DISTRIBUTION PANEL #2 (IN MAIN 600 V SWITCHB 550V. 3PH. 3W. (IN ELECTRICAL ROOM # G-102)		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	AOA 3P FA' 3 * 8 - 3/4"C 3 PH. GOO-120/20BV TRANSFORMERS MOUNTED ABOVE RESP. LIGHTING PANELS. 10 4 # 2 - 2'C L.P. 'G.A'		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		AS BUILT ERAWING UTVATE BAY 44
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\frac{70A 3P}{3 # 4 - 1'/4"C} = \frac{7}{12} + \frac{4}{12} + \frac{1}{12} + 1$	30 26	26
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	3 * 8 - 3/4" c 40A 3P FA' 3 * 8 - 3/4" c 3 * 8 - 3/4" c LP GE LP GE LP GE		IBUTION PANEL #2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0-2500A 0-750 V	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	40A 3P FA 30 4 # 2 - 2'C L.P. 'GH' 1	SELECTOR SWITCHES	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	40A 3P 'FA' 30 4# 2 - 2"C L.P. 'GL'	2	
	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	O A CONTACTOR - DLEY TYPE 'ML', M-TORK #IB37ZSK XY CONTACT	
• • • • • • • • • • • • • • • • • • •	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.	2185-713
	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	FRONT ELEVATION MAIN 600 V SMIT	DN
6'-8" <u>3'-4"</u>	3 + 1 - 11/2"C PP DD' = 3 + 6 - 1"C PP QQ' $= 23A 3P 5A' PP 'KK' = 0A 3P FA' PP 'NN'$ $= 3 + 1/0 - 2"C PP 'KK' = 3 + 4 - 14"C PP 'NN'$	APPROVED	12 E CARAGE ADDITION - FOR TENDER 9 11 AS BUILT 9 10 A CIRCUIT #DP3-13 MOTOR HP REVISED.
	90A 3P FA 3 = 2-11/4 C MOTOR CONTROL	CENTRE 'MM'	
<i>i</i> 9 17 25 , 8	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	TURE BUD, ONTAGO MAT 1X2 SEPT. 18. 6 MAR: 29/6	8 6 3 MAKE-UP AIR UNITS ON CIRCUITS # UU-6,7 & B DELETED. 5 2 MOTOR CONTROL CENTRE 'VV' REVISED, CIRCUIT * DP4-9 ADDED. 8 4 ISSUED FOR CONSTRUCTION
66 2 10 18 9 67 3 11 19 2	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	14/2/68 JWN. 19.62 20/10/6	B I GENERAL REV/SIONS B 2 FOR TENDER. 7 1 0 FOR APPROVAL.
68 SPACE SPACE 3 69 5 13 21 3	3 # 10 - 3/4" C 300A 3P 'LA' 3 # 350 MCM -3"C MOTOR CONTROL C	ENTRE 'VV'	ISSUE OR REVISION
70 6 14 22 <u>5</u>	1600/1600 A, 3P, A.C.B. 1600 A. 3P, 600 V LOW IMP, BUS DUCT DISTRIBUTION PA		METROPOLITAN CORPORATION OF GREATER WINNIPEG STREETS AND TRANSIT DIVISION
71 7 15 23 6 ' 72 8 16 '24 7	500 A 3 F 'MA' 600A, 3P, 600 V LOW IMP. BUS DUCT DISTRIBUTION PA	NEL #3	TRANSIT STORAGE AND SHOP FACILITIES
EPOLIT ELEVATION ERONT ELEV			PANEL SCHEDULES II
ITRE 'MM' M.C.C. 'TT' M.C.C. 'VV'			MARGISON AND ASSOCIATES LIMITED Waisman Ross • Blankstein Coop Gillmor Hanna Isslie street. don mills. ontario 10 donald street, winnipeg, manitoba
(N. T. S.) (N. T. S.)		The	DIRECTOR OF STREETS AND TRANSIT

1	15 A	IP	È
2	15A 2 = 12 - 1/2 15A		'EA
	15A 2=12 - 1/2		
3	20A 2*12 - 1/2*	<u>, 1P</u> , C	'EA
4	20A 2*12 - 1/2*		'E
5			'EA
	20A 2=12 - 1/2"		,
6	20A 2=12 - 1/2"	1P ' Č	<u>'E</u> /
7	15A 2 • 12 - 1/2		'E4
8			'EA
	15 A 2=12 - 1/2"		
9	15 A 2 12 - 1/2"	<u> 183</u> C	<u>'E</u> /
10	15 A 3=12 - 1/2"		'E/
11			'E
	70A 3#4 -1%4*		
12	40A 3*8 - 3/4	<u>3P</u> "C	<u>'E</u> /
/3	20A 3=12 - '/z'	ЗР	'E/
14			'E/
	20A 3#12 - 1/2"		
15	15 A 2 = 12 - 1/2'	<u> 1</u> P " C	<u>'E</u> /
16	15 A 2#12 - 1/2"		<u>'E</u>
/7			'E.
	15A 2#12 - 1/2		
/8	70A 3 * 4 - 11/4	<u>зр</u> "С	'EA
19	15 A 3#12 - 1/2"	<u>3</u> P	'E.
20	3 = 12 - 1/2" 20 A	C 3P	'EA
	20A 3=12 - 1/2"		
21	30A 3#10 - ¥4	<u>38</u> "C	Έ.
22	15A 3#12 - 1/2"		'E/
23-3		5 F	'E

MANITOBA HYDRO INTEROFFICE MEMORANDUM

то

FROM David Dudar C.E.T. Technical Assistant - Protection Distribution Planning & Protection Distribution Engineering - Winnipeg Dept. 820 Taylor Ave. (1), Winnipeg, MB

Brian Adamyk Energy Services Advisor Major Accounts Department 360 Portage Ave. (6), Winnipeg, MB

DATE 2010 11 26

SUBJECT UTILITY INFORMATION REQUIRED FOR CITY OF WINNIPEG TRANSIT, 421 OSBORNE AVE

Customer Information

Name:	City of Winnipeg Transit
Address:	421 Osborne Ave

Source Information

Station:	Jessie
Feeder:	22U81

347/600V Supply Transformer Information

kVA:	1500
Secondary Voltage:	347/600V
Connection:	Delta - Grounded Wye
Minimum Impedance:	4.0%
Primary Protection ¹ :	Westinghouse RBA RDE 400, 125E

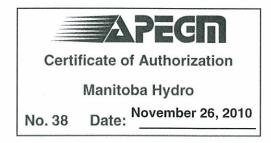
Fault Levels at Supply Transformer^{2, 3}

Switching Configuration	Voltage (kV)	LLL (Amps)	LG (Amps)	R1 (pu)	X1 (pu)	R0 (pu)	X0 (pu)
Normal System Operation ⁴	12	9055	8369	0.1087	0.4996	0.5667	0.4635
Fully Networked	12	9166	8430	0.1075	0.4935	0.5667	0.4635

Impedances are per unit on a 100MVA base

Notes

- 1. Manitoba Hydro sources replacement fuses from various manufacturers, therefore the fuse stated above is only representative of the fuse installed
- 2. These values are reflective of the normal and expected maximum available fault levels at the customer location, depending on the configuration of the supply, and can be used for arc flash hazard calculation.
- 3. These values are valid for the system configuration at the time of this study. These fault levels and impedances can change in the future as a result of changes to the Manitoba Hydro system, including feeder reconfiguration or re-conductoring, increasing the size of substation transformers and from new or re-conductored sub transmission lines. While these changes are infrequent in nature, they are not uncommon and Manitoba Hydro does not communicate changes in fault level or impedance information to customers unless a new request is initiated.
- 4. The Normal switching configuration is intended for overcurrent protection coordination studies, power quality studies, harmonic assessment and mitigation reports, or power factor correction studies only. The normal fault level information is not to be used for equipment rating purposes.



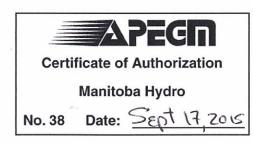
David Dudar C.E.T.

POWER QUALITY BENCHMARK

City of Winnipeg Transit Department 421 Osborne St. Winnipeg, Manitoba Premise # 6399318 City Centre CSC

Prepared By:	Marianela de los Rios Londono, IEEQ Student
8 8	Customer Engineering Services
	Industrial & Commercial Solutions

Reviewed By: G. A. Keena, C.E.T. Customer Engineering Services Industrial & Commercial Solutions



August 25, 2015





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TABLE OF CONTENTS

1 2		MARY	
3		ERVATIONS	
3.	.1	Voltage Variation	
3.	.2	Voltage Unbalance	9
3.	.3	Voltage Harmonics	.10
3.	.4	Current Harmonics	.12
3.		Voltage Flicker	
4	POW	/ER DĂTA	.17
4.	.1	Power and Power Factor	.17
4.	.2	Power Factor Correction	.18

APPENDIX A Power Quality Specification PQS2000-01

1 SUMMARY

All electrical measurements were found to be within acceptable limits during the monitoring period.

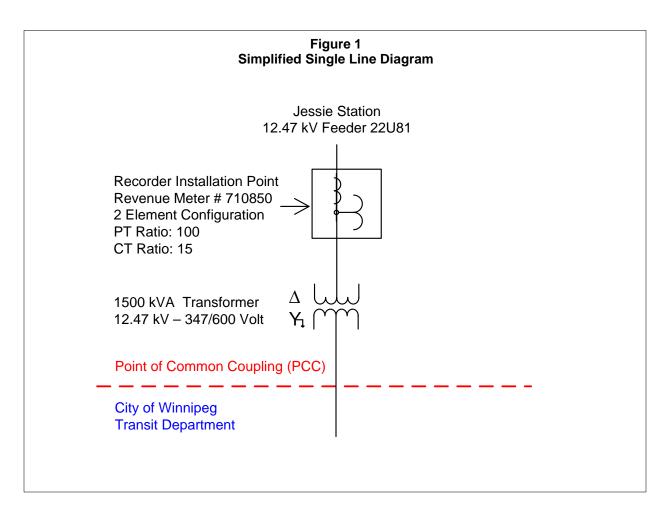
The energy profile indicates that there is potential for savings related to demand reduction.

2 INTRODUCTION

The purpose of a Power Quality Benchmark is to ensure that both Manitoba Hydro's electrical supply and the customer's facility are operating within acceptable power quality limits at the Point of Common Coupling (PCC). The PCC is defined as the point on Manitoba Hydro's system that is electrically nearest to the customer's installation. For the purposes of this benchmark, the PCC is located at City of Winnipeg Transit Department's Revenue Meter # 710850.

A Power Quality Benchmark can be used as a diagnostic review of a facility's power quality at the PCC. Monitoring and benchmarking power quality characteristics can enhance a facility's predictive maintenance program by identifying power quality issues that can result in lost production, adverse interaction or equipment damage within the facility. In addition, a benchmark is a comparative tool that can be used to assess electrical system characteristics before and after large facility modifications.

To collect information for this benchmark a Dranetz PX5 Power Quality Recorder was installed at the PCC as shown in Figure 1. The electrical supply was monitored from July 2, 2015 at 11:00 to July 8, 2015 at 09:25. The analysis given in this report is valid only for the stated monitoring period.



3 OBSERVATIONS

This section provides the relevant electrical operating limits as they apply to City of Winnipeg Transit Department. It also provides a graphical summary of the data collected at the PCC during the monitoring period from July 2, 2015 at 11:00 to July 8, 2015 at 09:25. In each subsection the measurement being evaluated, the applicable limit, and the measured values are stated. Note that the applicable limits are taken from Manitoba Hydro's Planning Criteria, CSA Standard CAN3-C235-83, and Power Quality Specification PQS2000-01.

The event on July 4th was utility in origin. The data has been excluded from Table 6 – Voltage Flicker Limits.

3.1 Voltage Variation

Average steady state voltage was found to be within acceptable limits 100% of the time during the monitoring period as required by Manitoba Hydro's Planning Criteria which has adopted CSA Standard CAN3-C235-83. The average steady state voltage range and upper and lower limits are provided in Table 1 below.

Table 1 - Voltage Variation Limits							
Indices	Lower Limit	Measured Value	Upper Limit	Comments			
Average Steady State Voltage Variation	11847 V	12392 V to 12675 V	13094 V	Within Manitoba Hydro's Planning Criteria			

Figure 2 below shows the average steady state voltages and the upper and lower average steady state voltage limits. Figure 2 also shows the average current values (in amps).

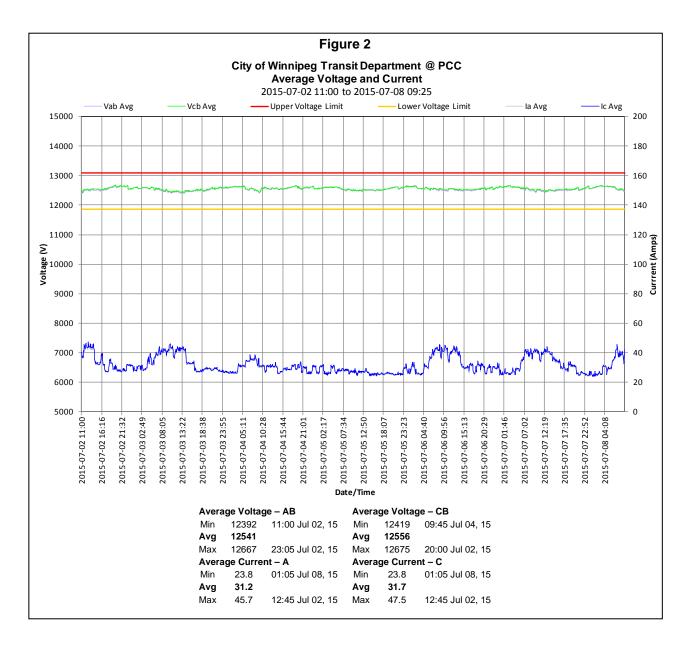
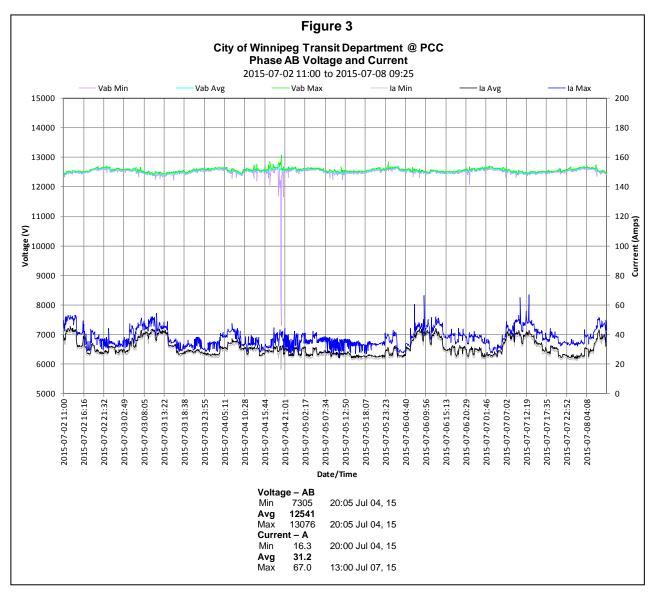
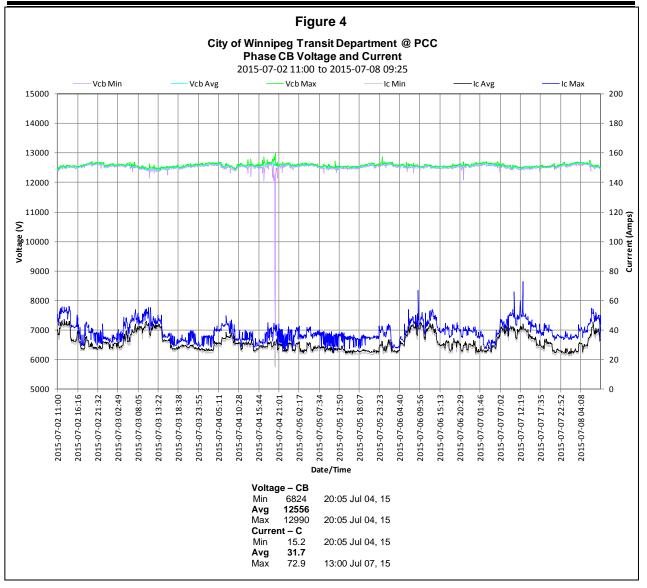


Figure 3 below shows the minimum, maximum and average values for phase AB voltage and phase A current. The graph for phases BC voltage and phase C current is available in Figure 4 on page 8.



The event on July 4th was utility in origin.



3.2 Voltage Unbalance

Voltage unbalance was not evaluated as the monitoring information collected was from a 2 element revenue metering system which only provides voltage and current information from two phases.

3.3 Voltage Harmonics

Voltage total harmonic distortion (THD) was within acceptable limits 100% of the time during the monitoring period as required by Manitoba Hydro's Power Quality Specification PQS2000-01. The average voltage THD and average voltage THD upper limit are provided in the Table 2 below.

Table 2 - Voltage Total Harmonic Distortion Limits							
Indices	Measured Value	Upper Limit	Comments				
Voltage Total Harmonic Distortion	2.1 %	5 %	Within PQS2000-01 Section 2.4.2 limit				

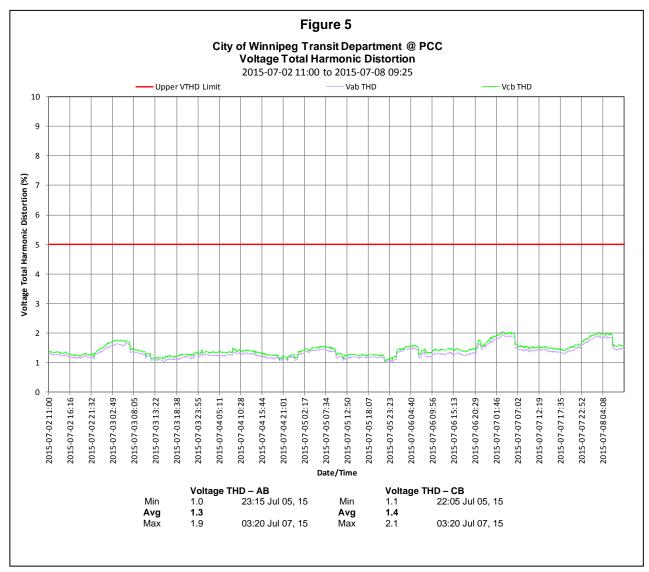
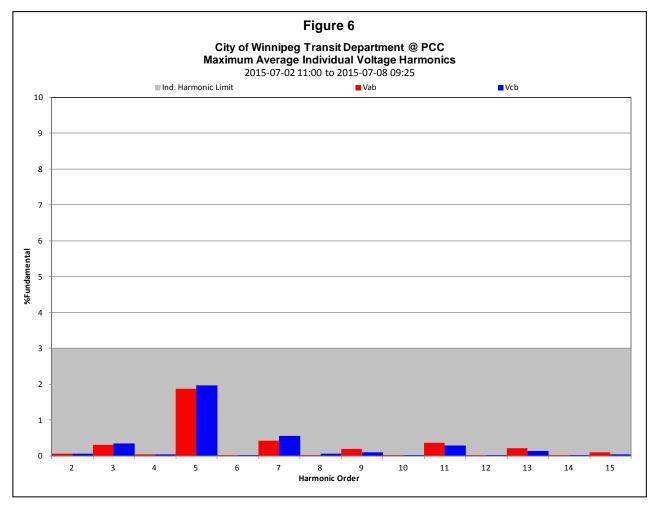


Figure 5 below shows the average voltage THD and the upper voltage THD limit.

Individual maximum average voltage harmonics were within acceptable limits 100% of the time during the monitoring period as required by Manitoba Hydro's Power Quality Specification PQS2000-01. The individual voltage harmonics and applicable limit are provided in Table 3 below.

	Table 3 - Maximum Average Individual Voltage Harmonic Limits								
Phase I argest Harmonic		Magnitude (% Fundamental)	Upper Limit	Comments					
AB	h≥2	5	1.9 %	3 %	Within PQS2000-01 Section 2.4.2 limit				
СВ	h≥2	5	2.0 %	3 %	Within PQS2000-01 Section 2.4.2 limit				

Figure 6 below shows the individual maximum average voltage harmonics and individual maximum average voltage harmonic limit.



3.4 Current Harmonics

Current total demand distortion (TDD) was within acceptable limits at least 95% of the time during the monitoring period as required by Manitoba Hydro's Power Quality Specification PQS2000-01.

The limit for current TDD is determined based on the ratio of symmetrical short circuit level to City of Winnipeg Transit Department's transformer rating.

The transformer rating and the symmetrical short circuit level are below for City of Winnipeg Transit Department at 12.47 kV:

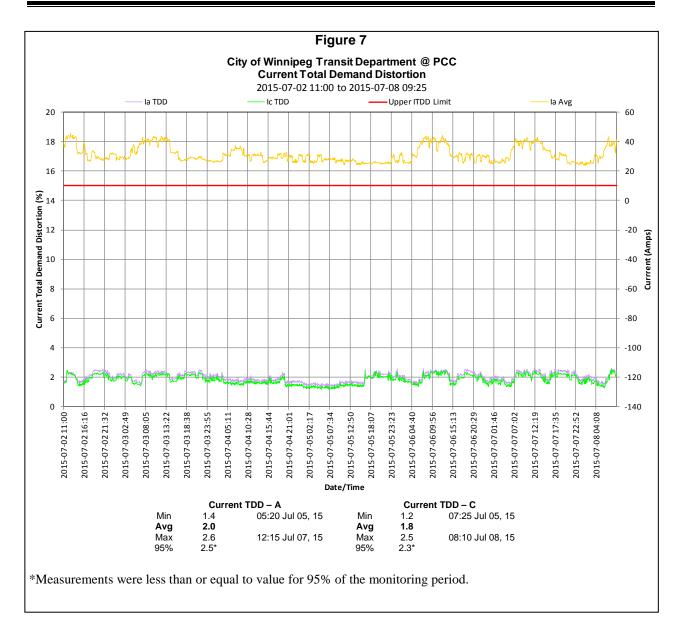
Short Circuit level at Transformer Primary *	9117	А	I _{SC}
Manitoba Hydro Transformer Rating - 1500 kVA	69	А	I_{L}
$I_{SC}/I_L =$	132		

* NOTE: The identified fault current (I_{SC}) is not to be used for equipment sizing, harmonic mitigation or arc flash calculations. It is only to be used to establish current total demand distortion limits.

The current TDD and applicable limit based on the ratio of I_{SC} to I_L are provided in Table 4 below. Note that City of Winnipeg Transit Department should operate their facility such that their TDD remains below the limit specified at least 95% of the time.

Table 4 - Current Total Demand Distortion Limits			
Indices	Measured Value	Upper Limit	Comments
Current Total Demand Distortion	2.5 %	15 %	Within PQS2000-01 Section 2.4.3 limit

Figure 7 on page 13 shows the average current TDD and upper current TDD limit.

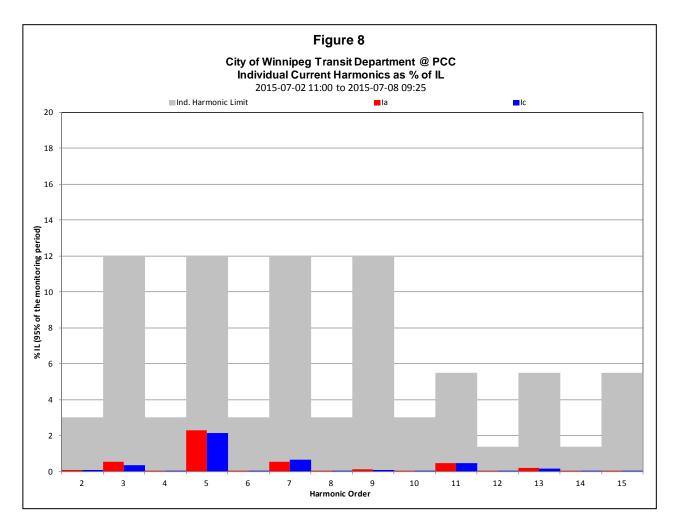


Individual current harmonics were within acceptable limits at least 95% of the time during the monitoring period as required by Manitoba Hydro's Power Quality Specification PQS2000-01. The individual current harmonics and limits for each range of harmonics are provided in Table 5 below.

	Table 5 - Individual Current Harmonic Limits						
Phase	Harmonic Range	Largest Harmonic	Magnitude (% I _L)	Upper Limit* Comments			
٨	h<11	5	2.3 %	12.0 %	Within PQS2000-01		
А	11≤h<17	11	0.5 %	5.5 %	Section 2.4.3 limit		
С	h<11	5	2.1 %	12.0 %	Within PQS2000-01		
C	11≤h<17	11	0.5 %	5.5 %	Section 2.4.3 limit		

*Note that the limit for even harmonics is 25% that of the limit for odd harmonics.

Figure 8 below shows the individual current harmonics and the upper individual current harmonic limits.



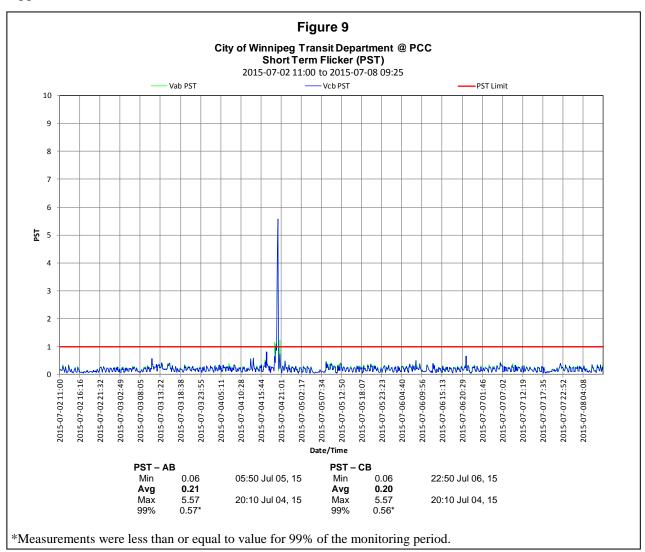
3.5 Voltage Flicker

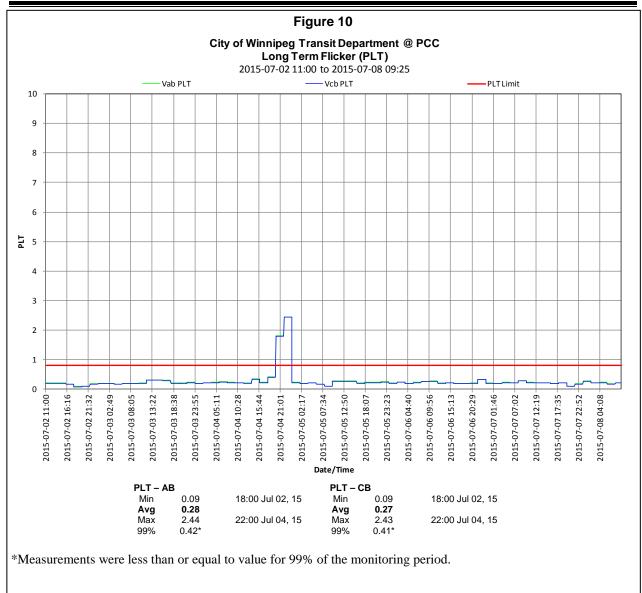
Short Term Flicker (PST) and Long Term Flicker (PLT) were found to be within acceptable limits at least 99% of the time during the monitoring period as required by Manitoba Hydro's Power Quality Specification PQS2000-01. The PST and PLT and their limits are provided in Table 6 below.

The event on July 4th was utility in origin. The 99% values exclude this event data.

Table 6 - Voltage Flicker Limits					
Indices	Measured Value	Upper Limit	Comments		
Short Term Flicker (PST) - 99 th Percentile	0.57	1.0	Within PQS2000-01 Section 3.3.1 limit		
Long Term Flicker (PLT) - 99 th Percentile	0.42	0.8	Within PQS2000-01 Section 3.3.1 limit		

Figure 9 below shows the PST and its upper limit. Figure 10 on page 16 shows the PLT and its upper limit.





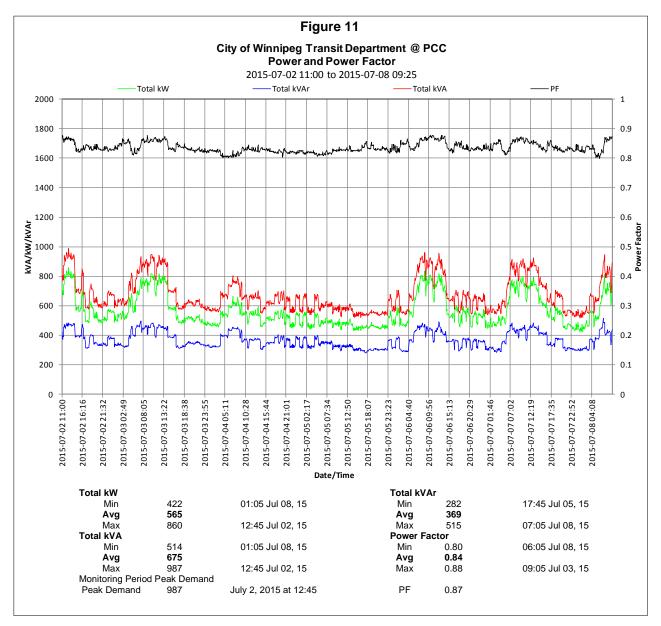
4 POWER DATA

This section provides the power data recorded at City of Winnipeg Transit Department.

4.1 Power and Power Factor

The peak demand recorded during the monitoring period was 987 kVA with a lagging power factor of 0.87. This peak occurred on July 2, 2015 at 12:45. The highest peak demand recorded in the last 12 month period was 1229 kVA recorded in March 2015.

Figure 11 below shows the power data recorded during the monitoring period. This data is not evaluated against any limit, but is provided for City of Winnipeg Transit Department's interest.



4.2 **Power Factor Correction**

This section provides background information on power factor correction and identifies typical demand savings. These are estimated savings, which could be realized by reducing the demand (kVA) requirements of the City of Winnipeg Transit Department facility.

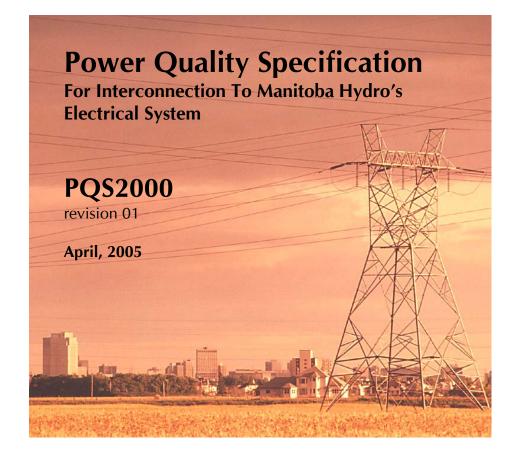
Opportunities exist to reduce the demand portion of the electrical bill and the details regarding the estimated savings associated with a variety of different capacitor sizes are outlined in the power factor optimization provided in Table 7 on page 19.

As an example, if a 300 kVAR capacitor was installed, the approximate annual savings for the past year would have been \$12,277 before taxes and the power factor would be approximately 0.977.

Note that this table is provided for informational purposes only. The savings contained in the table are not guaranteed and are only estimates based on the measurements taken in this benchmark.

			Table 7			
			er Factor Opt			
		it Department		-		
	ct	City Centre Distri		421 Osborne		
		9318	Premise: 639			
				kVA (Measured)	987	DEMAND
				Measured	0.87	P.F.
				Calculated	859	kW
				Calculated	487	kVAR
	65	Medium. Before tax	e General Service			Demand Rate
				ini i Demana onarg	7.15	Domand Hate
4(300	250	150	50	ze (kVAr)	Capacitor Si
0.99	0.977	0.964	0.931	0.891	er Factor	New Pow
98	987	987	987	987	emand kVA	A∨g D
12	108	96	65	24	VA reduced	K
80	879	891	922	963	NEW KVA	
\$14,050	\$12,277	\$10,920	\$7,335	\$2,684	SAVINGS	ANNUALS
	1 . X	Death and Death	0'		ф/I \/ А	0
		Payback Period	Ī		\$/kVAr	Capacitors
0.5	0.49	0.46	0.41	0.37	\$20.0	
0.8	0.73	0.69	0.61	0.56	\$30.0	CADITAL
<u> </u>	0.98	0.92	0.82	0.75	\$40.0	CAPITAL COST
1.4	1.22	1.14	1.02	0.93	\$50.0	0001
1.	1.47	1.37	1.23	1.12	\$60.0	
1.9	1.71	1.60	1.43	1.30	\$70.0	
2.2	1.95	1.83	1.64	1.49	\$80.0	
2.5	2.20	2.06	1.84	1.68	\$90.0	
	2.44	2.29	2.05	1.86	\$100.0	
3.2	2.69	2.52	2.25	2.05	\$110.0	
3.4	2.93	2.75	2.45	2.24	\$120.0	
3.1	3.18	2.98	2.66 ion is similar for 7	2.42	\$130.0	

APPENDIX A Power Quality Specification PQS2000-01





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Table of Contents

1.0	General Information	4
	1.1 Legislative Authority	4
	1.2 Authors	4
	1.3 Revisions	5
	1.4 Mitigation Of Power Quality Problems	
	1.5 Definitions	
2 0		•
2.0	Waveform Distortion	9
2.1	Introduction	
	2.1.1 Purpose	
2.2	General Requirements	9
	2.2.1 Customers Affected By This Document	9
	2.2.2 Information Supplied By The Customer	9
	2.2.3 Basis For a Power Quality Benchmark	. 10
	2.2.4 Power Quality Assessment and Mitigation Report	
2.3	Harmonic Measurement	. 10
	2.3.1 Measurement Period	. 10
	2.3.2 Analysis Period	
	2.3.3 Equipment	. 11
2.4	Limits For Design Purposes	. 11
	2.4.1 Voltage Unbalance	
	2.4.2 System Voltage Distortion	. 11
	2.4.3 Customer Current Distortion	
	2.4.4 Customer Voltage Distortion	. 13
	2.4.5 System Frequency	. 13
2.5	Limits of Interference With Communication Circuits	. 13
	2.5.1 Power Line Interference on Telephone Lines	. 13
	2.5.2 Design Limits	. 14
	2.5.3 Communication Interference	. 14
3.0	Flicker	.15
3.1	Introduction	. 15
	3.1.1 Manitoba Hydro's Flicker Philosophy	. 15
	3.1.2 Purpose	. 15
	3.1.3 Scope	
3.2	General Information	
	3.2.1 Customer's Affected By This Section	. 16
	3.2.2 Information Supplied By The Customer	. 16
	3.2.3 Information Supplied To The Customer	. 16
	3.2.4 Power Quality Assessment and Mitigation Report	

3.3	Limits For Controlling Flicker Levels	17
	3.3.1 Limits For Flicker Levels	17
	3.3.2 Limits For Voltage Fluctuations	
	3.3.2.1 Automatic Acceptance	17
	3.3.2.2 Limits For Dynamic Fluctuations	
	3.3.2.3 Limits For Periodic Fluctuations	
3.4	Application	20
	3.4.1 Customers With Multiple Flicker Producing Loads	
	3.4.2 Predicting P _{ST} Levels	
	3.4.3 Measuring Voltage Fluctuations and Flicker Levels	
Apr	pendix 1 – Bibliography	.22
	pendix 2 – CAN/CSA E1000-2-2-97 Flicker Curve	
	pendix 3 – Cumulative Frequency Analysis	



1.0 General Information

1.1 Legislative Authority

Section 15(5) of The Manitoba Hydro Act authorizes Manitoba Hydro to set, coordinate and enforce standards for the security, reliability and quality control of the transmission and distribution lines, of any person whose lines are interconnected with the transmission and distribution lines of Manitoba Hydro. Pursuant to section 10 of Regulation 186/90 – Electric Power Terms and Conditions of Supply, Manitoba Hydro is authorized to determine the voltage, frequency, phasing and other characteristics of power, the determination of which is final and binding on the user. Pursuant to this legislative authority, Manitoba Hydro has established the following Power Quality Specification.

1.2 Authors

The primary authors of this document are:

Glenn Paskaruk, P.Eng. Service Quality Section Distribution Planning & Design Division, T&D

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Kelvin Kent, P.Eng. System Planning Dept. Transmission Planning & Design Division, T&D

It was written in collaboration with, and is maintained by, the Manitoba Hydro Power Quality Committee which includes representation from the following departments:

Service Quality Business Engineering Services Department System Planning Department System Performance Department Electrical Distribution Planning & Design Department



1.3 Revisions

Revision Date 01 – January 2005	 Major Changes added Flicker criteria revised harmonic burst criteria revised the section related to mitigation responsibilities created a General Information section
00 – November 2000	Document created, addressed harmonics only

note:

Manitoba Hydro will review this document periodically and make revisions necessary to reflect changing system conditions and industry practices. When revisions are made, Manitoba Hydro will distribute the revised document to all regular recipients as soon as practically possible and make copies available upon request, however, it is the customer's responsibility to ensure it has the latest version of this document.

1.4 Mitigation Of Power Quality Problems

When Limits Are Exceeded:

It is Manitoba Hydro intent to plan and design its system so power quality levels are within the limits specified in this document.

In emergency situations, it may be necessary for Manitoba Hydro to make temporary changes to its system which may adversely affect power quality levels. Under these circumstances, distortion and/or flicker levels at the PCC may be temporarily exceeded.

The Manitoba Hydro service contract deals with concerns when limits are exceeded and covers responsibilities for mitigation of power quality interference issues.

Manitoba Hydro may perform a post installation Power Quality analysis for comparison with the original benchmark. If power quality limits are exceeded, Manitoba Hydro will assist the customer in determining the cause of the problem only.

1.5 Definitions

The following definitions are specific to Manitoba Hydro and may differ from those used by IEEE and other Industry Standards:

Flicker: flicker is the impact a voltage fluctuation has on the luminous intensity of lamps and fluorescent tubes such that they are perceived to 'flicker' when viewed by the human eye. The level at which it becomes irritating is a function of both the magnitude of the voltage change and how often it occurs.

PQS2000 Revision 01/ April 2005 /DR7 © 2005 MANITOBA HYDRO-ELECTRIC BOARD. All rights reserved. Flicker is quantified using the following:

Pst: the short-term flicker index, a unit of flicker level as defined in IEC Standard 61000-4-15 based on a 10 minute period. P_{st} is obtained by direct measurement using the IEC "flicker meter", calculated analytically, or obtained through computer simulation. In North America, a P_{st} of 1.0 (one) corresponds to the 'threshold of flicker irritation' for rectangular (step) voltage changes applied to a 120V incandescent lamp.

Plt: the long-term flicker index. P_{lt} is calculated using 12 consecutive (120 minutes) P_{st} samples and is given by:

$$P_{lt} = \sqrt[3]{\frac{1}{12} \cdot \sum_{j=1}^{12} P_{st_j}^{3}}$$

Emission Level: the maximum allowable P_{st} contribution available to a customer connecting a load assuming there is zero background flicker.

Planning Level: this is the maximum P_{st} and P_{lt} level used by the utility for planning purposes and is used to control the cumulative impact of all fluctuating loads connected to the system.

Flicker Curve: a graph that plots voltage fluctuations vs. frequency of occurrence. The points on the curve are based on laboratory experiments that applied a periodic voltage fluctuation to a light bulb and determined the levels at which the flicker becomes irritating to the human eye. Most published flicker curves are based on rectangular modulation of the 60 Hz AC voltage waveform.

Flicker meter: an instrument used to measure the severity of flicker and determine the level in terms of P_{st} and P_{lt} . The specifications for a flicker meter are outlined in IEC Standard 61000-4-15.

Point Of Common Coupling (PCC): the location on the Manitoba Hydro system electrically nearest to the customer installation. It is where access for Power Quality measurement is obtained and other customers are, or can be, connected. It can be located on either the primary or secondary side of a supply transformer depending on whether multiple customers are supplied from the transformer.

Power Quality Assessment and Mitigation Report: a technical report supplied to Manitoba Hydro by the customer which includes the following:

- detailed description of equipment being installed including all nameplate data, single-line diagrams, etc.
- projected impact new equipment will have on harmonic and flicker levels
- projected levels of interference with communication circuits
- description of measures that will be taken to mitigate harmonic levels exceeding the limits specified in this document
- description of measures that will be taken to mitigate flicker levels exceeding the limits specified in this document
- calculations and/or computer simulation that verifies corrective measures will work

Power Quality Benchmark: measurements taken at the PCC which include voltage and current levels, voltage and current total harmonic distortion trending, power usage and power factor. Usually performed before new non-linear loads are installed in order to establish baseline characteristics of the system and allow for future comparisons.

Total Harmonic Distortion (THD): total harmonic distortion is defined as:

$$THD = \frac{\sqrt{\sum_{h=2}^{50} V_h^2}}{V_1} \times 100\%$$

where:

- V_h = magnitude of individual harmonic components at frequency 'h'
- h = harmonic frequency (of 60Hz) which can be integer or non-integer (interharmonic)
- V_1 = the magnitude of the nominal fundamental frequency voltage

Total Demand Distortion (TDD): total demand distortion is defined as:

$$TDD = \frac{\sqrt{\sum_{h=2}^{50} I_h^2}}{I_L} \times 100\%$$

where:

Ih = magnitude of individual harmonic components

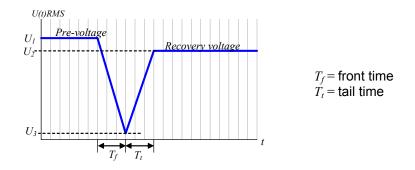
- h = harmonic frequency of (60Hz) which can be integer or non-integer (interharmonic)
- I_L = maximum annual demand load current (fundamental frequency component) at PCC

Voltage Variation: a change in the magnitude of the RMS voltage level. Voltage variations are generally of three types:

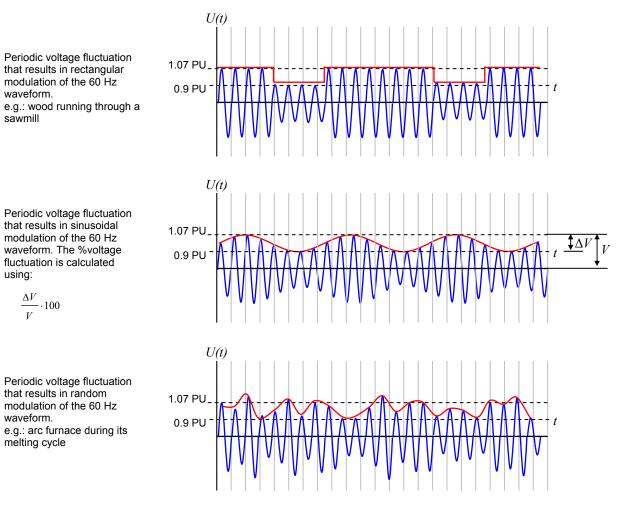
- i) **Voltage Sag:** a voltage variation in which the magnitude of the RMS voltage drops to a level below nominal, then returns to nominal. The voltage magnitude is typically between 0.1 and 0.9 *per-unit* (PU), and lasts anywhere from 0.5 cycles to 1 minute. A variation that is under 0.5 cycles is called a *'transient'*, and anything over 1 minute is considered an *'under voltage'*.
- ii) **Voltage Swell**: a voltage variation in which the magnitude of the RMS voltage increases to a level above nominal, then returns to nominal. The voltage magnitude is typically between 1.1 and 1.8 PU, and lasts anywhere from 0.5 cycles to 1 minute.
- iii) **Voltage Fluctuation**: a series of voltage changes or a continuous variation on the RMS voltage magnitude. Fluctuations are typically small voltage variations, (but not necessarily), ranging anywhere between 0.9 and 1.1 PU in magnitude.

PQS2000 Revision 01/ April 2005 /DR7 © 2005 MANITOBA HYDRO-ELECTRIC BOARD. All rights reserved. Voltage fluctuations can be one of two types:

Dynamic (aperiodic) Fluctuations are caused by the starting and stopping of large inductive loads. Starting a motor or energizing a transformer are good examples. The RMS voltage drops, then recovers to a steady-state level that is less than the pre-voltage. One dynamic fluctuation produces 2 voltage changes.



Cyclic (periodic) Fluctuations are part of the normal, continuous operation of the load. The RMS voltage magnitude varies between two values resulting in amplitude modulation of the AC sine wave envelope.



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2.0 Waveform Distortion

2.1 Introduction

If a load draws a sinusoidal current when it is connected to a sinusoidal voltage supply, it is called a 'linear' load. When the load draws a non-sinusoidal (distorted) current, the load is called 'non-linear'. When non-linear currents are allowed to flow through the linear elements in a utility electrical system, the resulting voltage drops are non-sinusoidal. If allowed to accumulate, they can degrade the quality of the utility supply voltage. One way to control utility voltage quality is to limit the amount of waveform distortion produced by individual non-linear loads.

2.1.1 Purpose

The purpose of this section is to establish responsibilities and to specify limits for harmonic and interharmonic distortion created by non-linear loads connecting to the Manitoba Hydro electrical system.

2.2 General Requirements

It is Manitoba Hydro's responsibility to provide and maintain a voltage supply within harmonic limits as specified in this document. Based on engineering information provided by Manitoba Hydro, it is the customer's responsibility to ensure its load does not increase harmonic levels on the Manitoba Hydro system beyond limits specified herein and does not impact other customers' electrical services. This section describes, in detail, the flow of information between Manitoba Hydro and the customer.

2.2.1 Customers Affected By This Document

All new or existing customers whose load may exceed acceptable harmonic levels or who may be affecting nearby customers are impacted by this document. This is typical of:

- customers adding large non-linear loads to the Manitoba Hydro system
- customers who have or who are considering installing power factor correction capacitors

2.2.2 Information Supplied By The Customer

Whenever customers propose connecting equipment (as defined in 2.2.1) to the Manitoba Hydro system, or whenever existing customers may be exceeding harmonic limits, Manitoba Hydro requires all relevant information pertaining to the connected loads, including:

- i) single-line diagram of the installation
- ii) all non-harmonic producing loads
- iii) all harmonic producing loads and their harmonic spectrums
- iv) transformer ratings and impedance
- v) cable impedance that should be included for harmonic analysis
- vi) power factor correction capacitor and filter information, if applicable

note: For 66kV and greater interconnections, refer to Manitoba Hydro's "Transmission System Interconnection Requirements" document for more details regarding other information that may be required.

2.2.3 Basis For a Power Quality Benchmark

Upon reviewing the information supplied in 2.2.2, Manitoba Hydro, at its discretion, will perform a Power Quality Benchmark measurement at the PCC. The basis for doing so will be determined using existing data and by the extent to which the Manitoba Hydro system will be impacted.

Whenever a Power Quality Benchmark measurement is performed, the following information will be supplied to the customer¹:

system data:

- i) normal short circuit MVA level at the PCC
- ii) supply transformer nameplate information (when applicable)
- iii) impedance spectrum at the PCC (when applicable)

measured data:

- iv) voltage and current levels
- v) total harmonic distortion, (voltage and current), at the PCC
- vi) power usage and power factor

¹ Where a technical representative is acting on behalf of the customer, this information will be provided to the customer only, unless the customer has provided written consent for Manitoba Hydro to provide the information to such representative.

2.2.4 Power Quality Assessment and Mitigation Report

Upon receiving the Power Quality Benchmark information, the customer must provide Manitoba Hydro with a Power Quality Assessment and Mitigation Report. This report must include information outlined in Section 2.2.2 and demonstrate that the harmonic limits specified in section 2.4 are met. Service connection will not be granted until the report is received and reviewed by Manitoba Hydro.

2.3 Harmonic Measurement

Harmonics and interharmonics up to the 50th shall be included in all calculations.

2.3.1 Measurement Period

When performing a Power Quality Benchmark, Manitoba Hydro shall normally perform measurements at the customer PCC for one week (168 hour period) during typical production load levels. The effect of a shorter production cycle and seasonal variation of loads will be considered in determining when a benchmark is performed. Manitoba Hydro reserves the right to choose the date/time and duration of the benchmark measurements.

2.3.2 Analysis Period

The maximum allowable level of total demand distortion (TDD) is determined with reference to the customer's I_{SC}/I_L ratio and Table 2.4.3 of this document. Actual TDD is based on data obtained during the measurement period. All customer facilities are expected to be at or below the maximum allowable TDD 95% of the time during all normal operating cycles. For shorter periods, during start ups or other transient conditions, the limits may be exceeded by up to 50% (1.5x the design limit). The TDD must be less than 1.5x the design limit 99% of the time during all normal operating cycles, with no occurances exceeding 2.0x the design limit.

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2.3.3 Equipment

Power harmonic analyzers must be capable of performing power quality measurements and harmonic calculations from n=1 to 50. They shall have a minimum sampling rate of 128 samples/cycle, (8kHz), with a resolution of at least once every 15 minutes.

2.4 Limits For Design Purposes

The criteria in this section shall be applied to design studies and equipment specifications.

2.4.1 Voltage Unbalance

The customer's design shall account for unbalance in the voltage supply using Table 2.4.1, where unbalance is defined as the ratio of negative sequence voltage to positive sequence voltage, or alternatively,

[%]unbalance = $\frac{Highest \ deviation \ from \ the \ average \ voltage \ of \ the \ 3 \ phases}{Average \ voltage \ of \ the \ 3 \ phases}$

Table 2.4.1 - Voltage Unbalance Limits			
Voltage Level	Rural	Urban	
25kV and less	5.0%	4.0%	
greater than 25kV 2.0%)%	

2.4.2 System Voltage Distortion

Manitoba Hydro shall normally limit the voltage distortion levels at the PCC to a maximum of the following values:

Table 2.4.2	Table 2.4.2 - Maximum System Voltage Distortion @PCC				
Bus Voltage at PCC (V _{bus})Individual harmonic or interharmonic voltage distortion (%)Total Voltage Distortio 					
69kV and less	3.0	5.0			
$138kV \geq V_{bus} > 69kV$	1.5	2.5			
V _{bus} > 138kV	1.0	1.5			

These values represent distortion levels based on the cumulative effect of all customers connected to the same point on the supply.

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2.4.3 Customer Current Distortion

As part of the Harmonic Assessment and Mitigation Report, the customer shall demonstrate that current distortion limits at the PCC will not exceed the limits as specified in this document. The values are summarized in Table 2.4.3.

Table 2.4.3 – Current Distortion Limits Maximum Harmonic Current Distortion In Percent of I _{Load} Individual Harmonic Order (Odd Harmonics)						
			$V_{bus} \leq 69kV$	/		
I _{sc} /I _L	<11	11≤ <i>h<</i> 17	17≤h<23	23≤h<35	35≤h	TDD
<20*	4.0	2.0	1.5	0.6	0.3	5.0
20 - 49	7.0	3.5	2.5	1.0	0.5	8.0
50 - 99	10.0	4.5	4.0	1.5	0.7	12.0
100 - 1000	12.0	5.5	5.0	2.0	1.0	15.0
>1000	15.0	7.0	6.0	2.5	1.4	20.0
		69	$KV < V_{bus} \le 1$	38kV		
I _{sc} /I _L	<11	11≤ <i>h<</i> 17	17≤ <i>h<</i> 23	23≤h<35	35≤h	TDD
<20*	2.0	1.0	0.75	0.3	0.15	2.5
20 - 49	3.5	1.75	1.25	0.5	0.25	4.0
50 - 99	5.0	2.25	2.0	0.75	0.35	6.0
100 -1000	6.0	2.75	2.5	1.0	0.5	7.5
>1000	7.5	3.5	3.0	1.25	0.7	10.0
	V _{bus} > 138kV					
I _{sc} /I _L	<11	11≤ <i>h<</i> 17	17≤ <i>h<</i> 23	23≤h<35	35≤h	TDD
<50*	2.0	1.0	0.75	0.3	0.15	2.5
≥50	3.0	1.5	1.15	0.45	0.22	3.75

- Harmonics and interharmonics up to h = 50 shall be included in all design calculations

- Even harmonics are limited to 25% of the odd harmonics listed above

- Current distortions that result in a DC offset, e.g., half-wave converters, are not allowed

- Duration of harmonic levels is outlined in section 2.3.2

*All power generation equipment is limited to these values of current distortion, regardless of actual I_{SC}/I_L or voltage level

where:

- *I*_{SC} = short-circuit current for normal system conditions that result in minimum short circuit capacity at the PCC, considering all supply alternatives
- I_L = maximum annual demand load current (fundamental frequency component) at PCC

2.4.4 Customer Voltage Distortion

The customer shall design its installation and specify equipment such that the steady state voltage distortion (VTHD) contribution due to the installation complies with Table 2.4.4 below.

Table 2.4.4 - Maximum Customer Voltage Distortion Design Limits				
Bus Voltage at PCC (V _{bus})Individual harmonic or interharmonic voltage distortion (%)Total Voltage Distor THD (%)				
69kV and less	2.0	3.5		
$138kV \geq V_{bus} \ge 69kV$	1.0	1.5		
V _{bus} > 138kV	1.0	1.0		

Table 2.4.4 ensures that total bus voltage distortion levels do not exceed levels specified in Table 2.4.2 particularly in the case of parallel resonance.

2.4.5 System Frequency

Calculations and design shall consider a fundamental frequency range of:

Table 2.4.5 – Frequency		
Continuous	$60\pm0.2~\text{Hz}$	
\leq 30 seconds	58 Hz to 63.5 Hz	

2.5 Limits of Interference With Communication Circuits

2.5.1 **Power Line Interference on Telephone Lines**

Communication circuits most susceptible to power line interference are low frequency, analog telephone circuits. The interference is a function of separation between the power circuit and the telephone line, the parallel distance, and the plant susceptibility and interference potential of the power line.

The interference potential of the power line can be estimated using the I·T product described by;

 $I \cdot T = I_{RMS} \times TIF$

however, the complexity of the problem makes it extremely difficult to accurately calculate the interference level with all 3 factors included. As a result, this guideline relies on measurements to check compliance.

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2.5.2 Design Limits

The maximum balanced and residual Inductive Influence (I·T) levels shall be as follows:

Table 2.5.1 – Maximum I*T Limits @PCC		
Balanced I·T	Residual I .T	
6000	100	

Power line influenced noise can be measured at the telephone plant. Using special instruments, "noise to ground" can be measured in dBrnc, (decibel C-message weighted). Measurements of noise to ground (Ng) \leq 80 dBnrc will generally not cause telephone interference.

2.5.3 Communication Interference

Manitoba Hydro strives to keep the balanced I·T product harmonic interference level below 6000 on any one line that may cause induction into communication circuits. For any particular application, Manitoba Hydro is prepared, if necessary, to discuss the allowable I·T as specified in section 2.5 with the understanding that any required interference mitigation directly resulting is the responsibility of the customer.

After it has demonstrated that its plant meets minimum standards for integrity and susceptibility, the communication company, with Manitoba Hydro's cooperation, is responsible for demonstrating the violation of telephone interference limits and identifying (when applicable) the customer suspected of causing interference problems.

3.0 Flicker

3.1 Introduction

Electrical equipment that is switched or switches as part of its normal operation, may cause voltage fluctuations. From a utility's perspective, there are 2 issues that raise concern:

- the risk of the voltage magnitude being outside accepted tolerances
- 'flicker' effect from light sources as a result of the fluctuation

Section 3.0 explains the flicker requirements of loads connecting to the Manitoba Hydro system.

3.1.1 Manitoba Hydro's Flicker Philosophy

Manitoba Hydro plans and designs its system primarily;

- to meet steady-state load demand (KVA) requirements
- to ensure steady-state voltage levels are within CSA Standards
- to maintain reliability levels that are as good or better than industry averages

For economic reasons, Manitoba Hydro does not plan or design its network to carry the starting current requirements of individual loads. As a result, voltage fluctuations introduced by these loads may cause visible flicker depending on the size of the load, the impedance of the system at that point, and the frequency of the fluctuations.

Manitoba Hydro's responsibility is to ensure that overall flicker levels are kept within acceptable levels by placing limits on voltage fluctuations introduced at the customer's point of common coupling. Based on engineering information provided by Manitoba Hydro, it is the customer's responsibility to ensure its load does not introduce voltage fluctuations beyond limits specified in this document.

3.1.2 Purpose

Section 3.0 establishes a uniform practice pertaining to voltage fluctuations and their impact on the Manitoba Hydro electrical system and other customers. This creates equity among customers in different parts of the Province, clarifies responsibilities of both the customer and Manitoba Hydro, and protects the overall integrity of the Manitoba Hydro system.

3.1.3 Scope

Section 3.0 establishes responsibilities for and specifies limits of voltage fluctuations introduced at the point of common coupling between the Manitoba Hydro electrical system and its customers. It covers the following voltage ranges:

 HV System
 > 25 kV

 MV System
 1000 V - 25 kV

 LV System
 <1000 V</td>

This is a technical document and does not address other policy or contractual requirements associated with interconnection to the Manitoba Hydro system.



3.2 General Information

3.2.1 Customers Affected By This Section

All new or existing customers whose load introduces voltage fluctuations, or who may be affecting nearby customers are impacted by this document. This is typical of:

- customers adding large non-linear loads to the Manitoba Hydro system
- customers who have or who are considering installing large motors (typically 15hp or greater for 3 phase, and 5hp or greater for 1 phase)

3.2.2 Information Supplied By The Customer

Whenever customers propose connecting equipment (as defined in section 3.2.1) to the Manitoba Hydro system, or whenever existing customers are introducing voltage fluctuations that cause other customers to complain, Manitoba Hydro requires all relevant information pertaining to the connected load(s).

General information is documented in the Electric Service Application form. Additional information specific to flicker producing loads includes;

- the load starting request form
- maximum %voltage fluctuation and expected rate of fluctuation during steady state operation

3.2.3 Information Supplied To The Customer

For motors and other large loads, Manitoba Hydro will provide load starting calculations and starting restriction(s).

In the case of load that produce periodic fluctuations during steady state operation, Manitoba Hydro shall provide;

- a background flicker measurement
- the short circuit MVA at the PCC

3.2.4 Power Quality Assessment and Mitigation Report

After the exchange of information, the customer shall provide Manitoba Hydro with a Power Quality Assessment and Mitigation Report that includes the expected flicker emission levels of the new load.

Manitoba Hydro, at its discretion, may perform a post installation flicker measurement to ensure that planning levels have not been exceeded by the addition of the new load(s). The results of the measurement shall be provided to the customer. They can also be provided to a consultant working on behalf of the customer, if the customer provides written consent for Manitoba Hydro to provide the results to such consultant.

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3.3 Limits For Controlling Flicker Levels

Manitoba Hydro strives to maintain a cumulative background flicker (planning) level of $P_{ST} < 1.0$ and $P_{LT} < 0.8$, 99% of the time, throughout its system. To achieve this, flicker emission limits have been established for individual loads connecting at various PCC voltages.

3.3.1 Limits For Flicker Levels

The customer shall design its equipment such that its flicker emission levels do not exceed the limits in table 3.3.1. The calculations shall assume there is no background flicker.

Table 3.3.1 – Customer Emission Limits ¹			
PCC Voltage	P _{ST}	P _{LT}	
LV (<1000 V)	1.0	0.8	
MV (1000 V – 25 kV)	0.9	0.7	
HV (>25 kV)	0.8	0.6	

¹ at or below these limits, 99% of the time, based on a 7 day benchmark measurement or other representative load cycle 1 day or greater

3.3.2 Limits For Voltage Fluctuations

This section contains limits for voltage fluctuations introduced by individual loads. By establishing limits on individual voltage fluctuations, Manitoba Hydro can ensure customers meet the emission limits in table 3.3.1.

3.3.2.1 Automatic Acceptance

Generally speaking, if the rate of voltage fluctuation is known, the first step in evaluating the disturbance level of a new load is to relate the maximum apparent power (S_{max}) of the load to the short-circuit power (S_{sc}) available at the PCC:

$$\Delta V\% = \frac{S_{\text{max}}}{S_{sc}} \cdot 100$$

- S_{max} should include the maximum power seen during starting
- for induction motors, S_{max} is typically 6X to 8X rated horsepower
- for induction furnaces, S_{max} is typically 2X to 4X rated KVA

Table 3.3.2 – Limits For Relative Power Variations ¹		
Changes per minute	ΔV	
< 10	0.4%	
10 to 200	0.2%	
> 200	0.1%	

¹ Taken from IEC 1000-3-7 Table 4

Loads having $\% \Delta V$ values at or below the levels specified in Table 3.3.2 are considered acceptable and **further flicker analysis is not required**. For values above the limits, sections 3.3.2.2 and 3.3.2.3 apply.

3.3.2.2 Limits For Dynamic Fluctuations

Dynamic voltage fluctuations are usually caused by the starting and stopping of motors. However, energization of other loads including transformers and capacitors may also cause brief voltage fluctuations. The primary reason for limiting dynamic fluctuations is to ensure proper operation of the load itself. The second reason is flicker. Although a single motor alone may not generate flicker complaints, the cumulative effect of several motors starting randomly on a distribution feeder can.

Using the information supplied by the customer in section 3.2.2, Manitoba Hydro first determines the ability of the system to supply the energy necessary to start and operate the proposed load(s). Using computer simulation of the supply circuit, the cumulative %voltage drop is calculated from the station to the customer PCC.

Based on the results of the simulation, Manitoba Hydro limits starting and operation of the load(s) to the values shown in table 3.3.3.

Table 3.3.3 - Load Starting Restrictions					
Voltage Change @PCC	Restriction				
<2.0%	no restriction				
2.0 - 2.4%	twice per hour				
2.5 – 2.9%	once per hour				
3.0 - 3.4%	once every 2 hours				
3.5 – 3.9%	once every 4 hours				
4.0 - 4.9%	once per day				
5.0 - 7.0%	not allowed ⁵				
>7%	not allowed ⁵				

Notes:

- 1. In some applications, a motor may cause voltage fluctuations during its steady state operation (jogging, jamming) and starting restrictions alone may not be sufficient. For these situations, section 3.3.2.3 applies.
- 2. For induction motors, Manitoba Hydro assumes a 6X locked rotor current.
- 3. Computer simulation is used to determine the maximum voltage fluctuation.
- 4. The table assumes one start produces 2 voltage changes.
- 5. Will be reviewed on a 'case by case' basis, and may be allowed in certain situations, (eg. a once-per-year transformer energization)

3.3.2.3 Limits For Periodic Fluctuations

When voltage fluctuations are produced by the normal, steady-state operation of a load (or loads), they are called 'periodic fluctuations'. Periodic fluctuations usually (but not necessarily) occur at frequencies greater than 1.0 changes/minute. Loads displaying this characteristic are typical of, but not limited to:

- arc furnaces
- welders
- motor jogging
- saw mills

Manitoba Hydro requires that individual loads do not introduce periodic fluctuations, at their PCC, above the curves shown in figure 3.3.1 below.

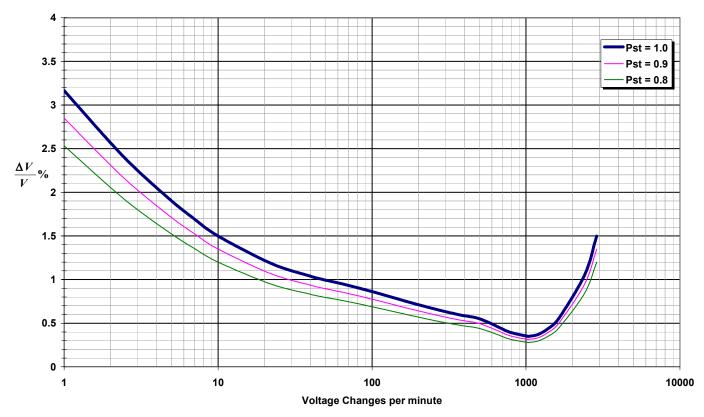


Figure 3.3.1 – CAN/CSA E1000-2-2-97 Flicker Curve For Periodic Voltage Fluctuations.

Notes:

- 1. The values were obtained experimentally through rectangular modulation of the 60 Hz AC waveform.
- 2. The human eye is most sensitive to fluctuations occuring at 8Hz, or 16 voltage changes per second. To convert the horizontal scale to fluctuations/sec. (Hz), divide by 120.
- To meet the limits table 3.3.1, the %∆V/V must fall on or below the corresponding P_{ST} curve, at the projected fluctuation rate. For loads with varying fluctuation rates (eg. arc furnace) %∆V/V should be checked against a representative range of fluctuation rates.
- 4. See Appendix 2 for an enlarged version of the upper frequency range.



3.4 Application

3.4.1 Customers With Multiple Flicker Producing Loads

In some cases, customers may have more than one flicker producing load. The cumulative impact at the PCC is determined as follows:

For dynamic fluctuations:

- Starting restrictions in Table 3.3.3 have been conservatively selected to account for multiple voltage fluctuations
- For customers connecting multiple motors at PCC voltages 25kV and less, the %voltage fluctuation is calculated based on the largest motor. Motors cannot be started simultaneously.
- For multiple motors connected at PCC voltages greater than 24kV, cumulative flicker is calculated using the methods described in IEC standard 1000-3-7.

For periodic fluctuations:

 The cumulative effect of operating 2 or more arc furnaces, for example, will be evaluated using the methods described in IEC standard 1000-3-7 regardless of the system voltage.

3.4.2 Predicting P_{ST} Levels

For loads that produce periodic flicker, the P_{ST} emission level of an individual load can be predicted using a 2 step process.

Step 1: determine the %change in voltage fluctuation and fluctuation frequency

This requires the short circuit level and in-depth knowledge of the load and its operating characteristics. In some cases, applying the appropriate shape factor (see IEC 1000-3-7) may also be necessary. For arc furnaces, the fluctuation frequency is not constant and multiple frequencies will have to be examined.

Step 2: determine the P_{ST} level

Due to the linear relationship between the P_{ST} level and the flicker curve, the P_{ST} can be determined directly from the flicker curve in figure 3.3.1. For example, if the $\%\Delta V/V = 0.7\%$ with a frequency of 40 changes/minute, the expected P_{ST} level is 0.66.

Note: Manitoba Hydro will supply the short circuit level at the PCC. The customer is expected to provide the projected voltage fluctuation and fluctuation frequency (rate)

Several flicker levels can be added together using the following formula:

$$Total P_{ST} = \sqrt[3]{\sum_{i} P_{ST_i}^3}$$



3.4.3 Measuring Voltage Fluctuations and Flicker Levels

Background flicker levels and voltage fluctuations shall be measured by:

- capturing the inrush current and voltage sag event at the customer's PCC using a
 power quality device capable of capturing high speed events.
- measuring the overall flicker level (P_{ST} and P_{LT}) over a representative measurement period.

The flicker level shall be measured using a power quality device that meets the requirements of the IEC flickermeter standard 61000-4-15. A graph of the cumulative frequency vs. P_{LT} shall be at or below the limits in Table 3.3.1, 99% of the time.

Using the RMS waveform from the voltage sag event, the maximum voltage change for dynamic fluctuations shall be calculated by subtracting the minimum RMS voltage from the steady-state pre-voltage:

%voltage change =
$$\frac{U_1 - U_2}{U_1} \times 100\%$$

where U_1 and U_2 are shown in figure 3.4.1.

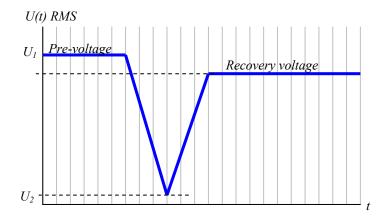


Figure 3.4.1 – RMS voltage profile of a dynamic voltage fluctuation.

The data from a flicker measurement shall be evaluated using a cumulative frequency method. This is explained in Appendix 3.



Appendix 1 – Bibliography

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IEEE P519A/D6: "Guide For Applying Harmonic Limits on Power Systems", January, 1999. (This guide is still in draft)

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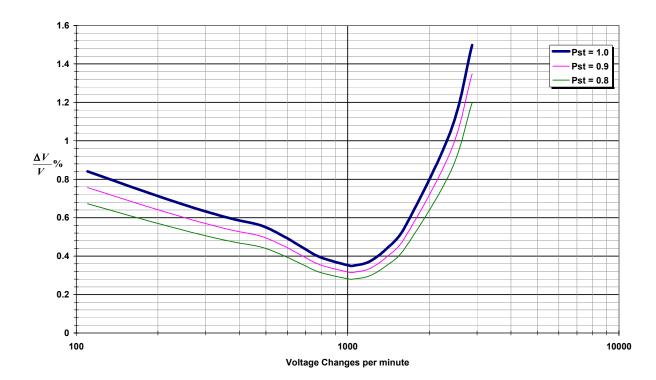
Note:

CSA = Canadian Standards Association CEA = Canadian Electrical Association IEEE = Institute of Electrical and Electronics Engineers IEC = International Electrotechnical Commission

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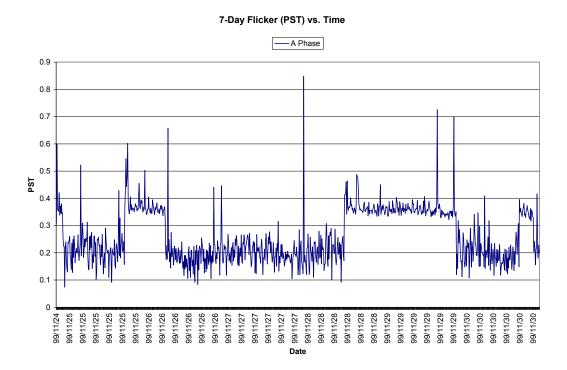
Appendix 2 – CAN/CSA E1000-2-2-97 Flicker Curve For Periodic Voltage Fluctuations (100 – 3000 changes/min.)





Appendix 3 – Cumulative Frequency Analysis

The flicker data collected during a 7-day benchmark measurement is sometimes difficult to analyze (see top graph below). As a result, it is best analyzed by plotting the PST values in a cumulative frequency graph. From this graph, the number of PST values above or below a particular threshold can be determined. (see bottom graph below)



Cumulative Flicker Frequency

- A Phase 100.0% 95.0% 90.0% 85.0% 80.0% 75.0% 70.0% 65.0% 60.0% 55.0% 50.0% 45.0% 40.0% 35.0% 30.0% 25.0% 20.0% 15.0% 10.0% 5.0% .0% 0.2 0.6 0 0.1 0.3 0.4 0.5 0.7 0.8 0.9 1 Pst

PQS2000 Revision 01/ April 2005 /DR7 © 2005 MANITOBA HYDRO-ELECTRIC BOARD. All rights reserved. April 20, 2015

City of Winnipeg Transit Department 421 Osborne Street Winnipeg, MB. R3L 2A2

Attention: Mr. Adolfo Laufer, P. Eng.

Facilities Maintenance Project Engineer

Reference: Electrical Load Study – 421 Osborne Street Winnipeg Transit Bus Garage Facility

Dear Sir:

Dillon Consulting Limited (Dillon) is pleased to submit our final report to Winnipeg Transit (Transit) for the electrical load study at the Winnipeg Transit Bus Garage located at 421 Osborne Street, Winnipeg.

Background

Winnipeg Transit has embarked on a number of projects within this facility over the years and is planning a number of new projects involving the need to add additional load to the electrical distribution system. Transit is concerned on the overall capacity and availability of the electrical distribution system with these new projects coming on line. In addition, Transit is concerned with the reliability of the main distribution equipment due its age and lack of available spare parts.

Dillon was retained by Transit to perform an electrical load study at this facility to determine the present electrical loading of the main distribution and associated sub-distributions. This should enable Transit to determine the capability to add additional electrical load to the present system.

Investigation and Data Gathering

Our report is based on electrical load data information recorded on site by Schneider Electric Service Department. Their monitoring equipment was installed on site during the period of March 12, 2015 to March 24, 2015. Data from the load monitoring for this period is included in Appendix A. In addition, Transit provided utility billing data for the past 12 months. These bills along with the recorded data show that the peak load values appear to occur during the winter months. Therefore, the peak value shown as 1048 amps appears to accurately represent the true peak.

Load monitoring equipment was connected on the electrical distribution equipment to record the load data information at the following distribution points:

- Main distribution circuit breaker
- Distribution 1 main circuit breaker (Overhaul and Repair Building)
- Distribution 3 main circuit breaker (Garage Building)
- Motor Control Centre VV (MCC-VV) main circuit breaker



Via: e-mail

1558 Willson Place Winnipeg Manitoba Canada R3T 0Y4 Telephone (204) 453-2301 Fax (204) 452-4412 *City of Winnipeg Transit Department Page 2 April 20, 2015*

The monitoring equipment recorded a wide range of data which may be of interest to Transit. However, for the purpose of this report, the focus will be on the electrical loading information and the availability to add additional load where required. Therefore, we will highlight the following data points:



- Current average (Amps)
- Voltage per phase (Volts)

These data points should provide the necessary information Transit requires to determine if the additional proposed loads can be connected to the existing electrical distribution system.

Results

The average and peak values for the monitoring data points noted above are summarized in the table below at each of the distribution points. In addition, this table also shows the actual current rating, in Amps, of the distributions as follows:

	Main Distribution	Distribution 1	Distribution 3	MCC-VV
Current (Amps) Peak	1048	664	126	126
Voltage L-L Average (Volts)	600	600	600	600
Current Full Load Rating (Amps) Actual Nameplate	2500	1600	600	300
Available Capacity based on full load allowable rating based on 80% rule (Amps)	952	616	354	114

Summary

Based on the above tabulated and calculated information along with the data recorded and included as Appendix A, the available capacity on each of the Distribution points is as follows:

952 A
616 A
354 A
114 A

*Note: Distributions 1, 3 and MCC-VV are sub-fed from the Main Distribution, so any load increases on Distributions 1, 3 and MCC-VV will impact the total on the Main Distribution.

City of Winnipeg Transit Department Page 3 April 20, 2015



In addition to the load study, Transit also requested an evaluation of the existing main distribution switchboard. Schneider Electric provided their review of this equipment and their response is included in Appendix B.

In summary, Schneider Electric advises that this equipment appears to not have been serviced in some time and will likely not be supported by the manufacturer for replacement parts. Spare parts will also become hard to source in case any modifications would be required.

As discussed with Transit, there have already been some issues with the existing equipment whereby circuit breakers were not functioning properly causing problems with the operation of the facility.

We would recommend a staged replacement of this switchboard with new equipment of adequate capacity for future growth over the next 25 years. We would be pleased to discuss this further with Transit to come up with a suitable plan for this changeover to minimize disruption to Transit's operation and within their budgets established. A separate engineering proposal would be required to carry out this work.

We thank you for the opportunity to provide these services to Transit, and look forward to a successful implementation of the proposed work plans.

Please contact the undersigned at (204)453-2301 or <u>bfeuer@dillon.ca</u> should there be any questions or comments regarding this report.

Sincerely,

DILLON CONSULTING LIMITED

Brian Feuer, P. Eng. Partner

BF/km

Encla Appendix A – Monitoring data (on CD) Appendix B – Condition report

Our file: 15-1692

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APPENDIX A

Monitoring Data (Refer to CD)

APPENDIX B

Condition Report



FIELD SITE VISIT

CUSTOMER: Dillon Consulting Limited

<u>SITE</u>: Osborne Bus Garage

ATTENTION: Brian Feuer

DATE: March 12, 2015

REASON FOR VISIT: Equipment Review and collection of Power Monitoring Data

<u>OBSERVATION</u>: Data for the following loads were collected from Noon March 12 to Noon March 23:

Main Distribution (Westinghouse 3000A) Distribution #1 (1600A) Distribution #3 (600A) MCC VV (200A)

<u>CONCLUSION</u>: The main switch gear is 1960 vintage. All the breakers are obsolete. The main Air circuit breaker has no signs of being serviced in recent years. Once it has been serviced a better idea of it's condition can be made. If a number of new breakers are to be added. The customer may want to upgrading the complete board by retrofilling. The existing switchgear structure and wires stay and all the obsolete breakers are replaced with new breakers and mounting system. This allows for more new breakers to be added in the future.

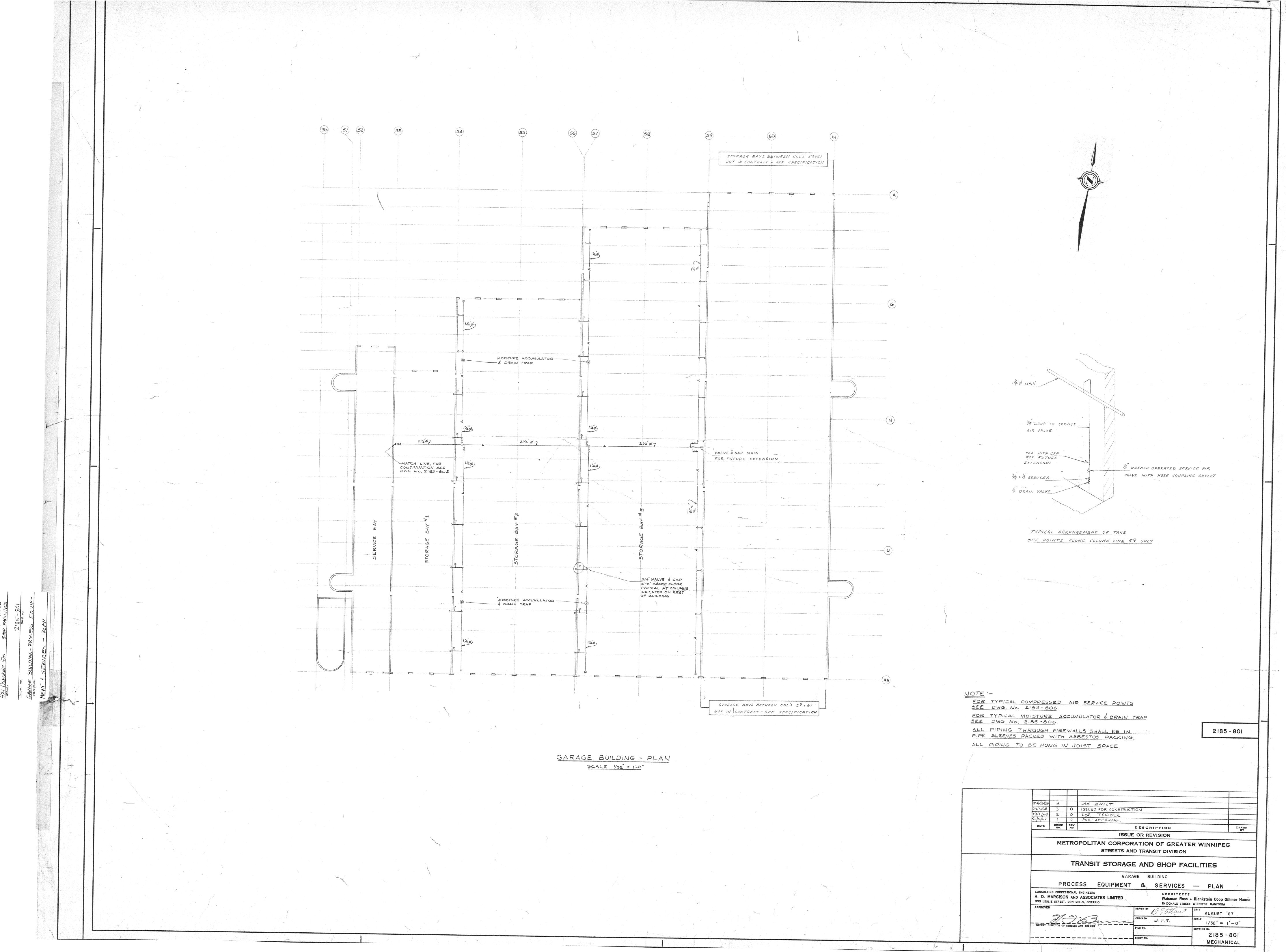
With a quick look at the Power Monitoring data. The Main service is lightly loaded (20 to 30%) with the peak load happening between 6:30 and 7:00 AM at around 35%. The power factor is running between 85 and 90%. (penalty \$ when below 90) But the cost may make the pay back to long. Harmonics are OK.

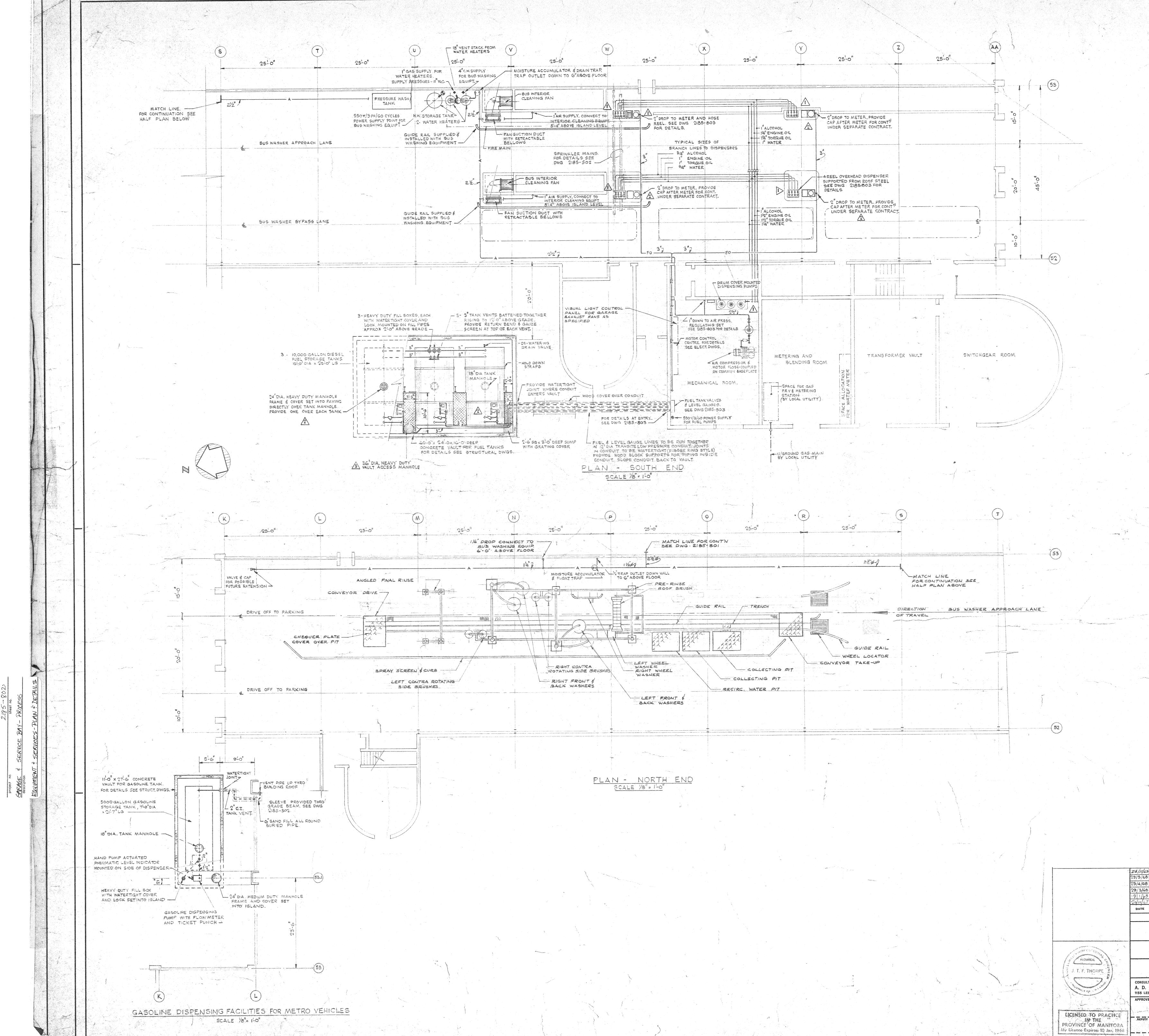
Dean Wiersema

Solutions Sales Representative: (204) 631-0685 dean.wiersema@schneider-electric.com

Schneider Canada Services, 21 Omands Creek Blvd, Winnipeg, Manitoba. R2R 2V2,

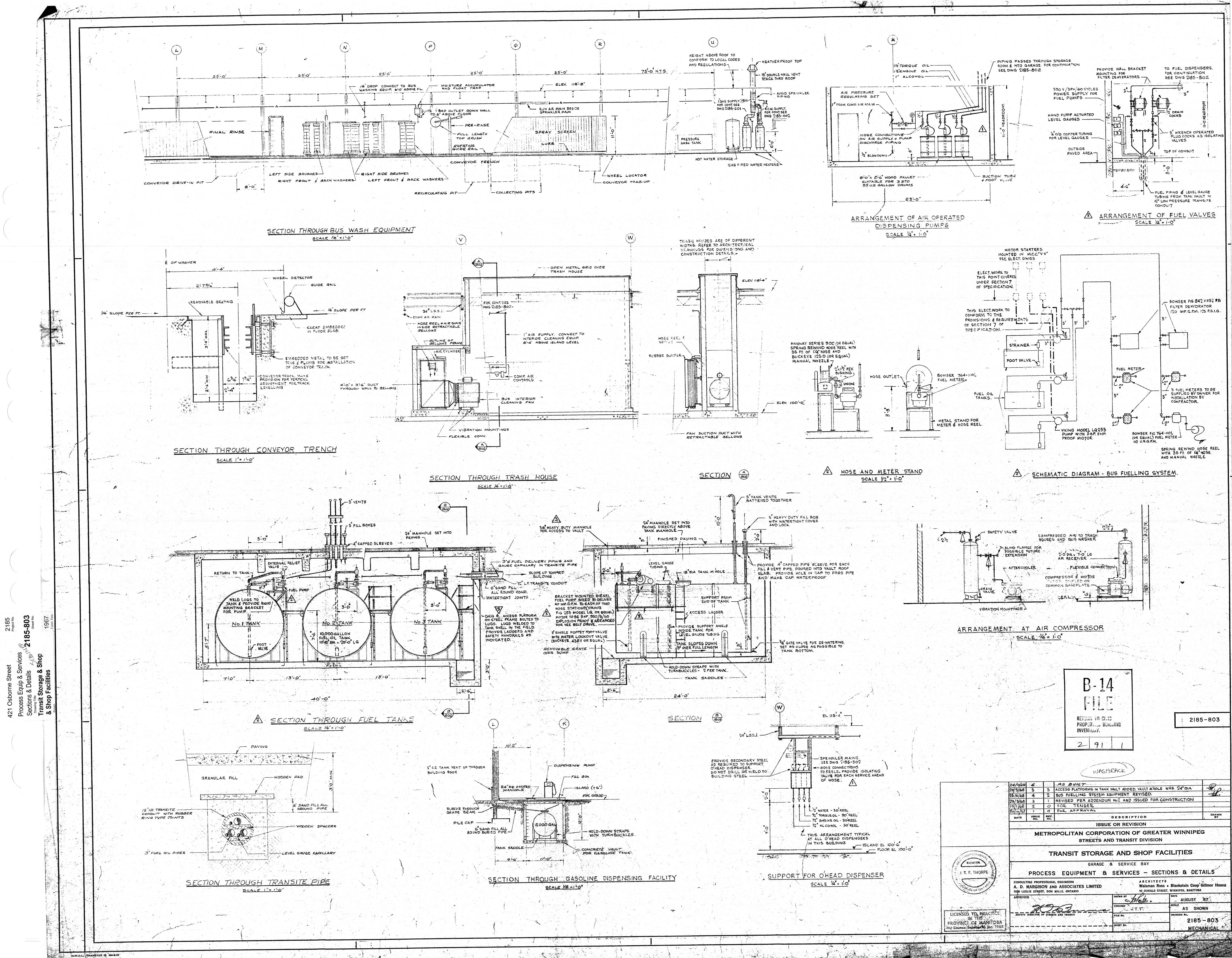
Winnipeg Transit Garage 421 Osborne - Premise # 6399318 Historical Electric and Gas Info											
Serv Month	Svc Cnt	Elec Days	Elec kW.h	Elec Bill Dem	% Load Factor	Elec Revenue	Svc Cnt	Gas Days	Gas m3	Gas Bill Dem	Gas Revenue
2014, MAR	2	59	506,037	1,129	61.5	\$27,734.55	2	61	104,972	12,238	\$200,628.31
2014, FEB	2	62	524,022	1,130	61.5	\$28,376.18	2	59	143,914	12,238	\$197,882.01
2014, JAN	2	60	510,772	1,126	62.2	\$27,883.40	2	61	262,101	13,031	\$85,471.67
2013, DEC	2 2	62	526,486	1,146	57.3	\$28,585.24	2 2	64 60	270,058	13,796	\$63,034.36
2013, NOV 2013, OCT	2	64 84	413,349 381,812	1,044 1,053	54.4 55.4	\$23,755.95 \$22,749.38	2	60 59	193,349 24,305	13,796 13,796	\$33,366.89 \$17,620.13
2013, SEP	2	30	449,955	1,106	55.9	\$25,532.98	2	59	13,005	13,796	\$6,896.99
2013, AUG	2	68	490,055	1,084	54.8	\$26,741.50	2	65	8,320	13,796	\$6,227.62
2013, JUL	2	58	442,621	1,126	55.9	\$25,473.22	2	60	5,680	13,796	\$4,654.20
2013, JUN	2	126	490,531	1,099	54.1	\$26,945.52	2	64	24,149	13,796	\$9,126.53
2013, MAY	2	29	429,165	1,111	55.0	\$24,244.25	2	60	88,108	13,796	\$23,642.93
2013, APR	2	29	469,260	1,164	57.3	\$25,808.33	2	59	104,306	13,796	\$42,921.39
2013, MAR	2	58	445,046	1,219	55.6	\$25,528.64	2	58	300,723	13,796	\$45,461.74
2013, FEB	2	62	588,222	1,243	59.0	\$30,538.21	2	61	372,406	13,796	\$57,053.09
2013, JAN 2012, DEC	2 2	60 65	510,877 572,412	1,215 1,282	57.7 55.8	\$27,708.70 \$30,302.35	2 2	61 64	365,766 363,735	13,796 15,410	\$60,988.63 \$54,035.11
2012, DEC 2012, NOV	2	65 59	572,412 435,535	1,282	55.3	\$30,302.35 \$24,323.86	2	64 59	244,308	15,410	\$37,422.98
2012, NOV 2012, OCT	2	57	395,110	1,068	54.5	\$22,528.93	2	59	92,261	15,410	\$22,908.50
2012, SEP	2	65	467,843	1,047	55.9	\$24,397.88	2	63	42,920	15,410	\$9,167.75
2012, AUG	2	59	447,091	1,120	56.8	\$24,111.80	2	60	4,430	15,410	\$4,575.26
2012, JUL	2	58	470,762	1,130	59.3	\$24,966.76	2	60	4,586	15,410	\$4,614.06
2012, JUN	2	97	499,109	1,102	54.9	\$25,679.18	2	64	41,075	15,410	\$10,273.61
2012, MAY	2	30	445,500	1,111	55.1	\$23,963.01	2	61	108,184	15,410	\$20,898.23
2012, APR	2	93	484,959	1,143	54.6	\$25,222.24	2	62	140,676	15,410	\$28,557.67
2012, MAR	2	29	481,140	1,228	55.7	\$25,571.57	2	60	264,129	15,410	\$43,494.91
2012, FEB	2	59	544,691	1,270	58.9	\$27,983.46	2	59	336,620	15,410	\$55,089.14
2012, JAN 2011, DEC	2 2	65 89	549,266 518,674	1,243 1,247	56.8 55.3	\$27,909.21 \$26,966.99	2 2	63 62	401,292 346,478	15,410 11,869	\$70,714.86 \$61,648.88
2011, DEC 2011, NOV	2	89 26	372,735	1,247	52.2	\$20,966.99 \$21,364.18	2	56	226,311	11,869	\$40,804.67
2011, ICT	2	60	442,637	1,102	53.4	\$23,328.35	2	62	121,866	11,869	\$23,707.01
2011, SEP	2	65	452,939	1,136	51.4	\$23,934.16	2	62	25,807	11,869	\$7,307.18
2011, AUG	2	60	444,071	1,133	53.9	\$23,631.65	2	61	1,076	11,869	\$3,951.48
2011, JUL	2	66	484,173	1,158	52.2	\$25,105.67	2	64	2,408	11,869	\$4,270.55
2011, JUN	2	90	445,646	1,155	51.3	\$23,888.71	2	61	36,203	11,869	\$10,970.10
2011, MAY	2	28	400,950	1,178	50.2	\$22,624.51	2	59	86,995	11,869	\$21,477.67
2011, APR	2	65	502,379	1,189	52.7	\$25,614.26	2	63	125,719	11,869	\$41,772.08
2011, MAR	2 2	59	487,658	1,252	55.2	\$25,576.78	2 2	60	298,689	11,869	\$66,249.70
2011, FEB 2011, JAN	2	55 67	484,069 562,079	1,267 1,279	56.0 54.7	\$25,623.98 \$28,076.03	2	56 64	324,694 382,652	11,869 12,181	\$70,999.49 \$80,981.87
2011, JAN 2010, DEC	2	60	480,556	1,185	55.7	\$28,078.03 \$24,758.81	2	64	322,824	12,181	\$68,175.84
2010, DEC 2010, NOV	2	56	390,846	1,112	51.7	\$21,392.67	2	58	210,193	12,521	\$45,275.72
2010, OCT	2	58	435,193	1,164	53.2	\$23,171.03	2	60	125,209	12,521	\$30,313.73
2010, SEP	2	66	518,340	1,203	53.9	\$26,028.53	2	63	49,885	12,521	\$13,765.45
2010, AUG	2	93	476,826	1,215	54.0	\$24,881.58	2	60	11,076	12,521	\$5,923.73
2010, JUL	2	33	491,535	1,086	56.6	\$24,212.08	2	64	3,909	12,521	\$4,490.28
2010, JUN	2	91	459,009	1,132	55.8	\$23,644.72	2	61	21,189	12,521	\$8,290.26
2010, MAY	2	31	461,835	1,126	54.6	\$23,640.62	2	62	95,833	12,521	\$24,715.85
2010, APR	2	90	470,588	1,154	54.1	\$23,562.00 \$22,709.43	2	61 50	150,732	12,521	\$43,271.47 \$72,141.06
2010, MAR 2010, FEB	2 2	28 55	433,620 433,214	1,219 1,244	52.4 52.9	\$22,709.43 \$23,022.80	2 2	59 55	260,474 301,946	12,521 12,776	\$72,141.06 \$82,996.04
2010, FEB 2010, JAN	2	55 69	433,214 557,629	1,244	52.9	\$25,022.80 \$26,816.41	2	55 66	356,053	12,776	\$82,998.04 \$99,139.09
2009, DEC	2	59	457,675	1,214	51.7	\$23,400.85	2	61	324,609	12,804	\$89,584.00
2009, NOV	2	53	377,456	1,135	52.7	\$20,424.31	2	56	200,873	13,456	\$57,736.23
2009, OCT	2	67	463,408	1,105	52.4	\$22,628.08	2	64	158,409	13,456	\$49,370.61
2009, SEP	2	59	423,290	1,114	52.3	\$21,554.15	2	60	14,447	13,456	\$8,433.15
2009, AUG	2	63	464,858	1,105	52.6	\$22,668.22	2	64	5,184	13,456	\$5,853.07
2009, JUL	2	61	411,413	1,157	50.6	\$21,573.74	2	60	5,779	13,456	\$5,204.13
2009, JUN	2	65	476,698	1,115	51.9	\$23,092.02	2	64 60	43,483	13,456	\$16,660.40
2009, MAY	2	61 50	401,078	1,112	51.3	\$20,908.88 \$23,032,20	2	60 50	106,314	13,456	\$35,033.10 \$62,271,52
2009, APR 2009, MAR	2 2	59 59	447,257 476,992	1,258 1,276	50.5 51.2	\$23,032.29 \$23,862.26	2 2	59 61	191,949 294,638	13,456 13,456	\$63,371.53 \$95,049.85
2009, MAR 2009, FEB	2	59 55	476,992 450,222	1,276	51.2	\$23,862.26 \$23,433.33	2	55	294,638 313,844	13,456	\$95,049.85 \$101,719.69
2009, JAN	2	71	596,350	1,277	53.3	\$27,154.04	2	67	390,471	15,155	\$138,801.59

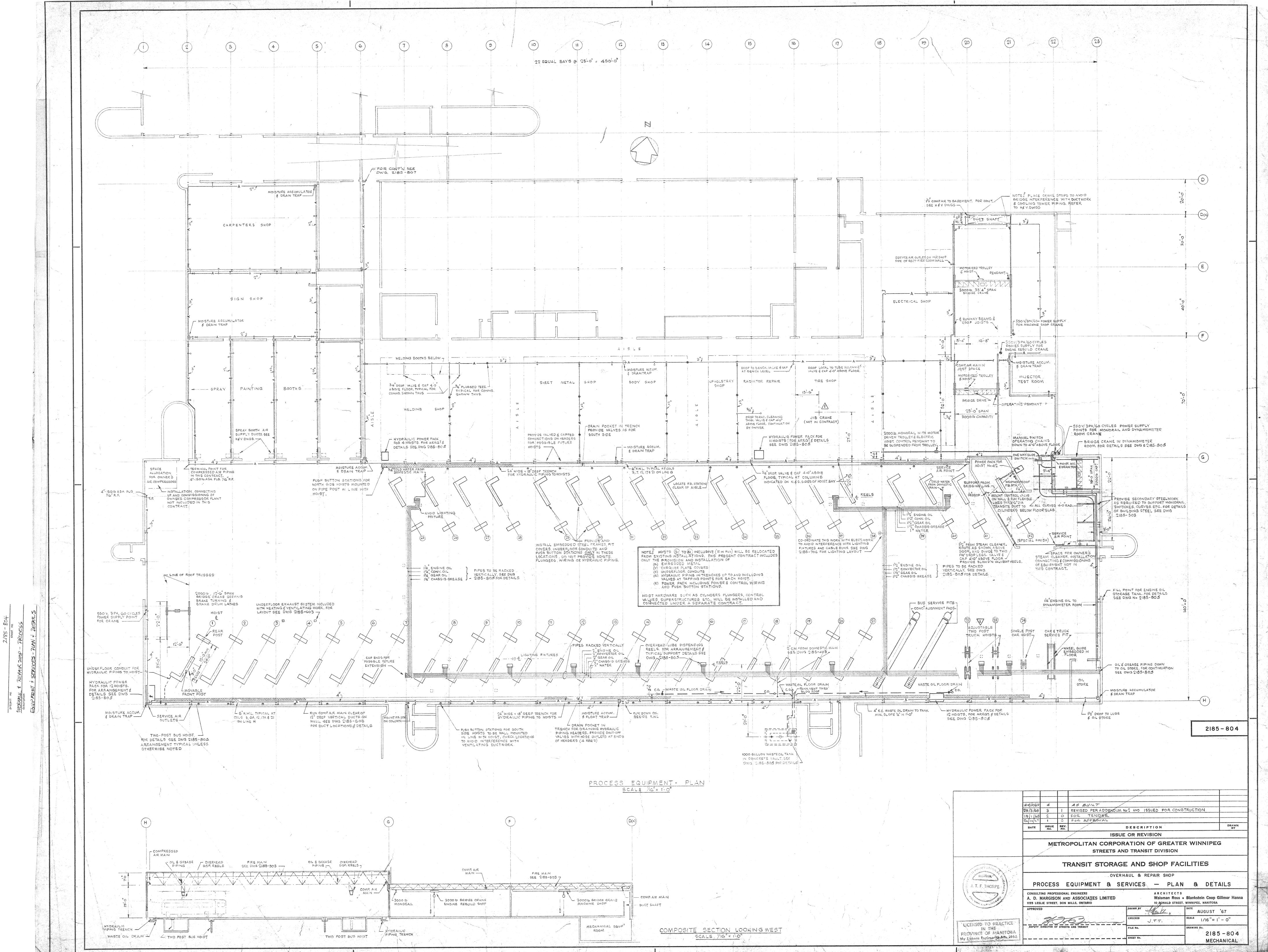




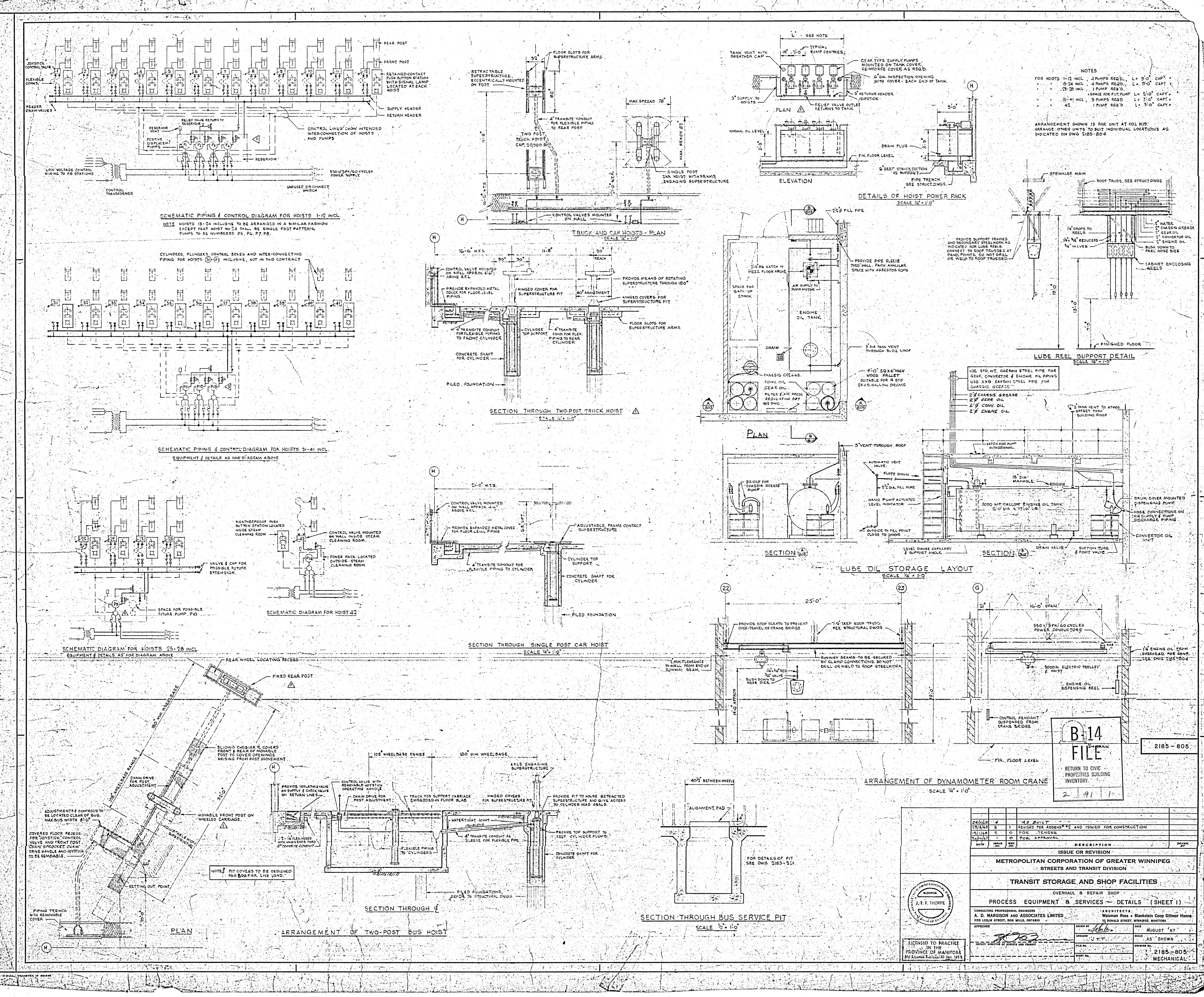
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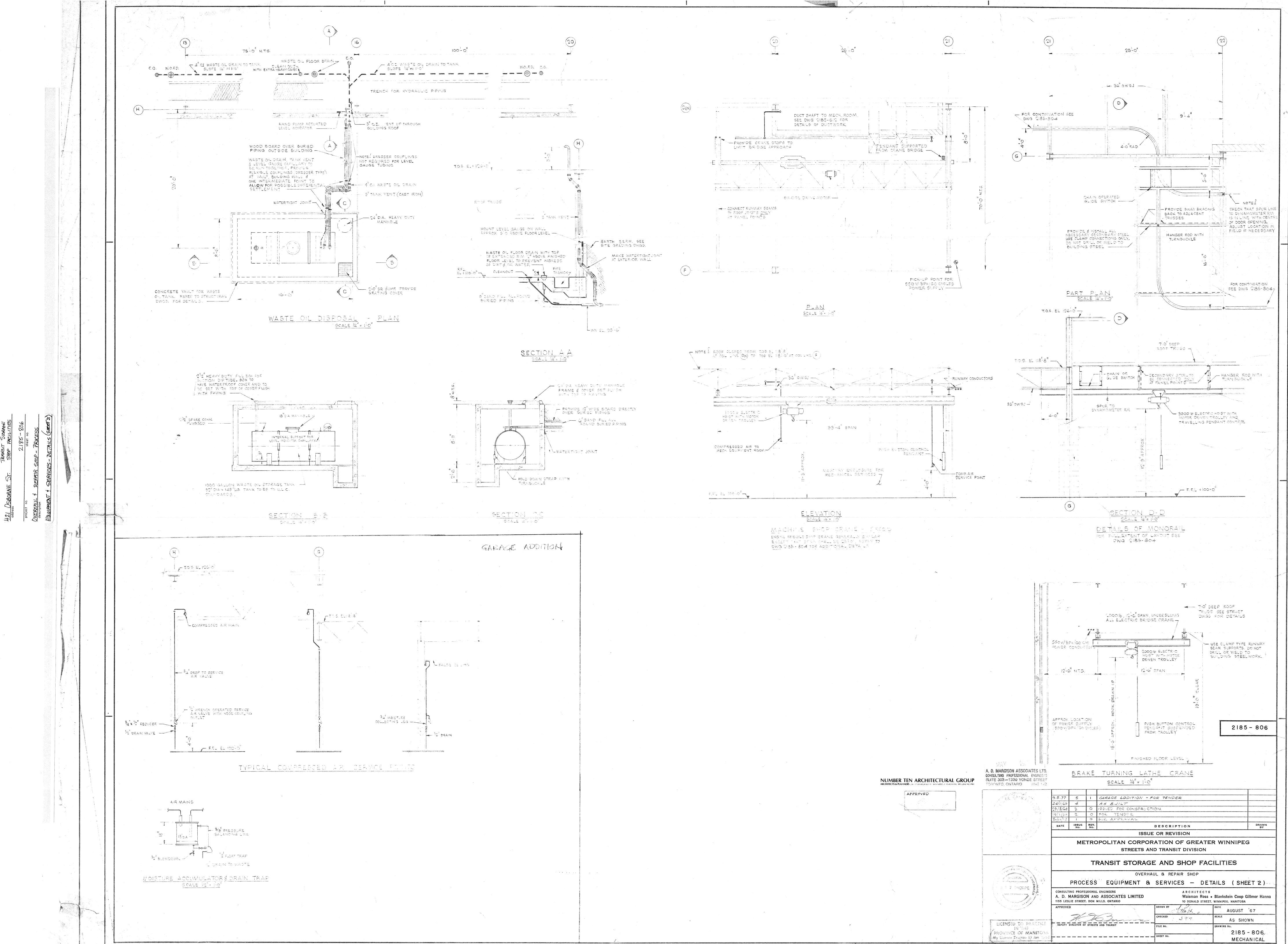


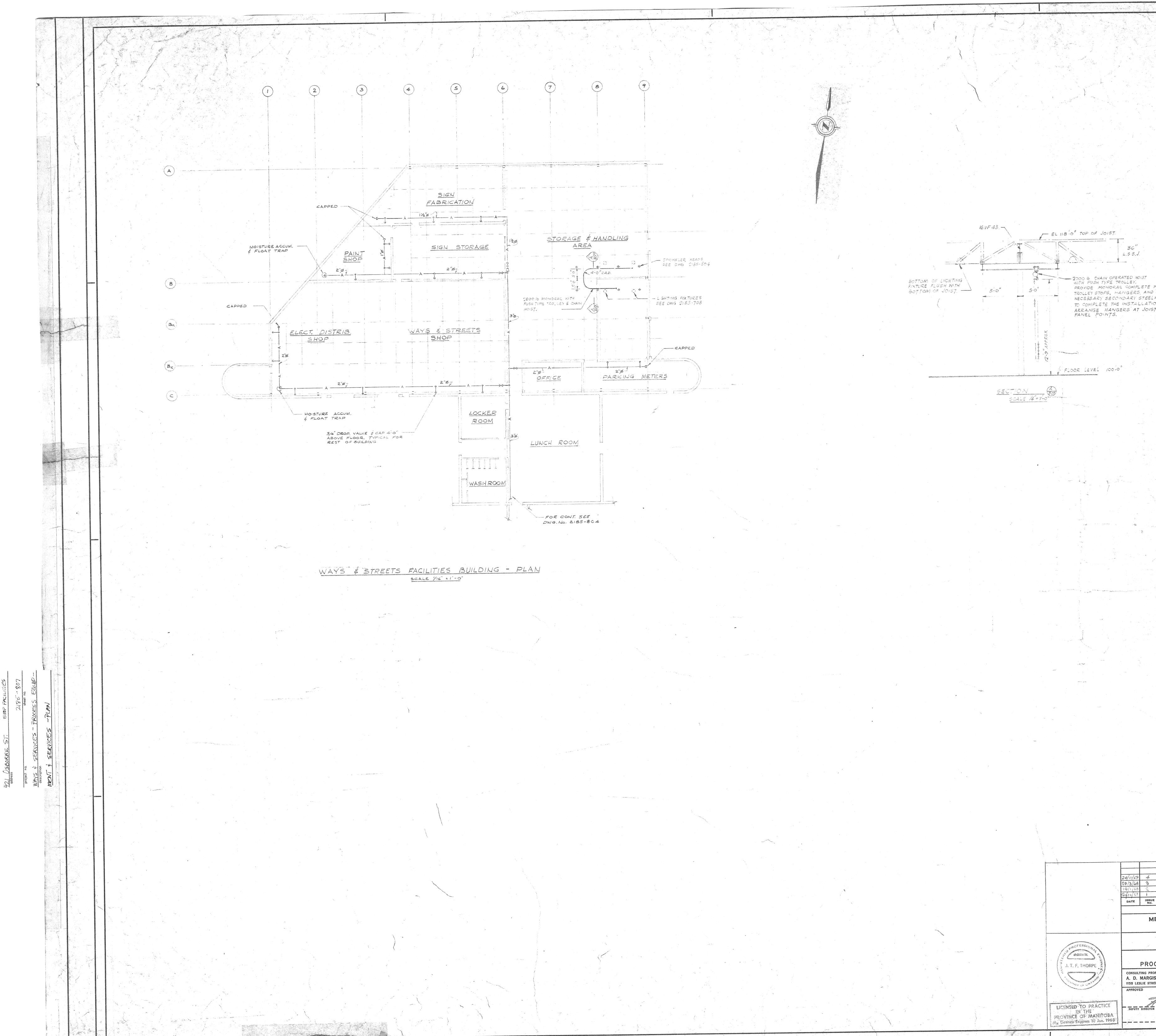


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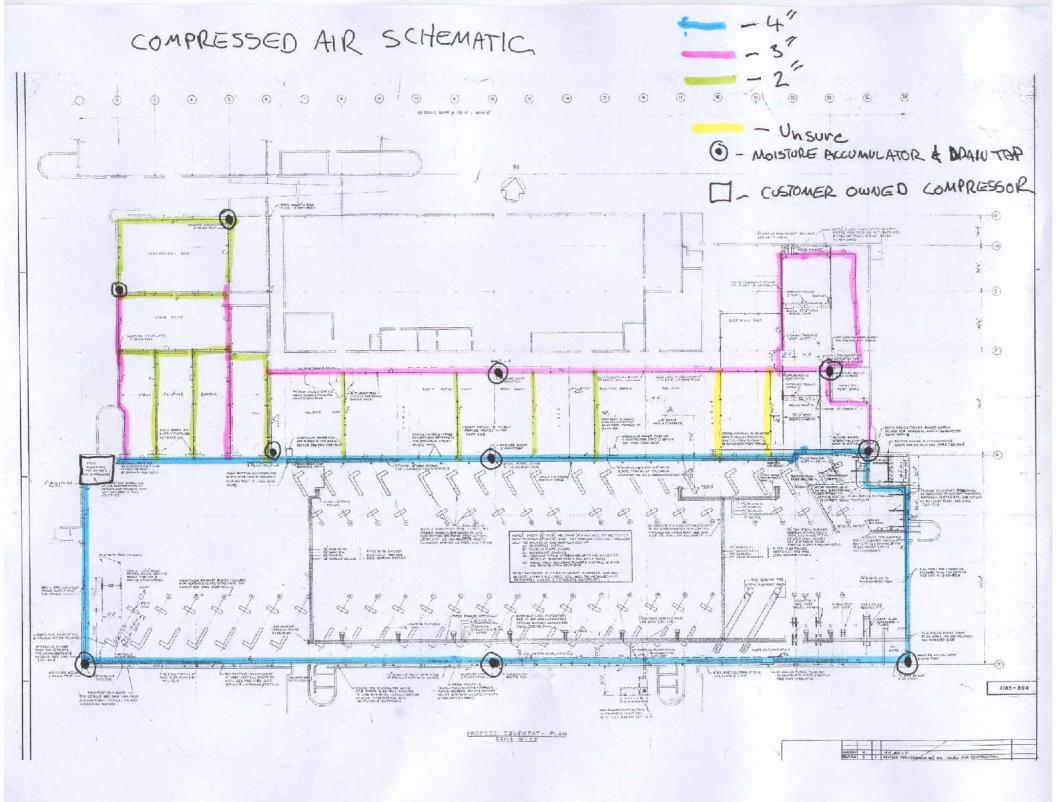
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ASBESTOS INVENTORY CONTROL



Planning, Property and Development Department Municipal Accommodations Division 4th Floor - 185 King Street • Winnipeg, MB • R3B 1J1

Building Name:	Building A, Maintenance Shop	Inspection Date:	July 8, 2015
Building Code:	TR01	Inspected By:	Elias Occupational Hygiene Consulting
Building Address:	421 Osborne Street	Construction Date:	

Material Location	Material Description	Drawing Label	Material Condition	Testing Status	Date M/Y	Test %	Est. %
	Stucco Column Cladding Throughout Building Should Be Tested Before Any Work Is Performed						
	Various Areas Have Been Tested See Inventory for Details						
Basement							
Cafeteria Storage	12x12 Ceiling Tile	C12	Good	Tested	May'09	0	
Cofetoria	Mastic - Pipe - Above Ceiling	MA	Good	Tested	May'10	25-50	
Cafeteria	Pipe Fitting Insulation - Above Ceiling	PF	Good	Tested	May'10	0.1-1	
Furnace Room	Pipe Fitting Insulation	PF	Good				
Kitoboo Hollwov	Mastic - Pipe - Above Ceiling	MA	Good	Tested	May'10	25-50	
Kitchen Hallway	Pipe Fitting Insulation - Above Ceiling	PF	Good	Tested	May'10	0.1-1	
Dispetate Area	Pipe Insulation - Above Ceiling	PI	Good				25-50
Dispatch Area	Pipe Fitting Insulation - Above Ceiling	PF	Good				25-50
Dispetate Currentians Office	Pipe Insulation - Above Ceiling	PI	Good				25-50
Dispatch Supervisor Office	Pipe Fitting Insulation - Above Ceiling	PF	Good				25-50
Turned	Pipe Insulation - Above Ceiling	PI	Good				25-50
Tunnel	Pipe Fitting Insulation - Above Ceiling	PF	Good				25-50
Boiler Room	Pipe Fitting Insulation	PF	Removed				
Stairwells	Stucco - Walls	ST	Needs Repair	Tested	May'09	0	
Admin Area- Main Floor							
Foyer (Inside Heater)	Mastic - Pipe	MA	Good				10
	Stucco - Ceiling	ST	Good				0
Foyer	Mastic - Pipe - Above Ceiling	MA	Good				10
	Pipe Fitting Insulation - Above Ceiling	PF	Good				5-10
	Stucco - Ceiling	ST	Good	Tested	Apr/'11	0	
Front Reception	Mastic - Pipe - Above Ceiling	MA	Good	~			10
	Pipe Fitting Insulation - Above Ceiling	PF	Good				5-10
North Offices (Inside Heater	Pipe Fitting Insulation	PF	Good				5-10
Cabinets)	Mastic - Pipe	MA	Good				10
South Offices (Inside Heaters)	Mastic - Pipe	MA	Good				10
South Offices	Pipe Fitting Insulation - Above Ceiling	PF	Needs Repair	Tested	Feb/ 11	5-10	
	Mastic - Pipe - Above Ceiling	MA	Good	Tested		10	
Control Office (Inside Heater)	Mastic - Pipe	MA	Good				10

Material Location	Material Description	Drawing Label	Material Condition	Testing Status	Date M/Y	Test %	Est. %
Control Office	Mastic - Pipe - Above Ceiling	MA	Good				10
	Pipe Fitting Insulation - Above Ceiling	PF	Good				5-10
	Stucco - Walls	ST	Good	Tested	Nov/ 12	0	
East Offices (Inside Heaters)	Mastic - Pipe	MA	Good				10
East Offices	Pipe Fitting Insulation - Above Ceiling	PF	Good				5-10
	Mastic - Pipe - Above Ceiling	MA	Good				10
West Offices (Inside Heaters)	Mastic - Pipe	MA	Good				10
West Offices	Pipe Fitting Insulation	PF	Good				5-10
	Mastic - Pipe	MA	Good				10
West Corridor	Pipe Fitting Insulation - Above Ceiling	PF	Good				5-10
	Mastic - Pipe - Above Ceiling	MA	Good				10
Men's Washroom	Pipe Fitting Insulation - Above Ceiling	PF	Good				5-10
	Mastic - Pipe - Above Ceiling	MA	Good				10
	12x12 Floor Tile	F12	Good				
Women's Washroom	Pipe Fitting Insulation - Above Ceiling	PF	Needs Repair				5-10
	Mastic - Pipe - Above Ceiling	MA	Good				10
	12x12 Floor Tile	F12	Good				
Janitor's Room	Mastic - Pipe	MA	Good				10
	12x12 Floor Tile	F12	Good				
Photocopy Room	Pipe Fitting Insulation	PF	Good				5-10
	Mastic - Pipe	MA	Good				10
	12x12 Floor Tile	F12	Good				
Hallway By Bathrooms	Pipe Fitting Insulation - Above Ceiling	PF	Good				5-10
	Mastic - Pipe - Above Ceiling	MA	Good				10
Admin Area- 2nd Floor							
Offices (All Heaters and Heater	Pipe Fitting Insulation	PF	Needs Repair				5-10
Cabinets)	Mastic - Pipe	MA	Good				10
2 North Offices (inside cabinets)	Pipe Fitting Insulation	PF	Removed01/13				5-10
(Site:Confirm offices)	Mastic - Pipe	MA	Good				10
Men's Washroom	Pipe Fitting Insulation - Above Ceiling	PF	Good				5-10
	Mastic - Pipe - Above Ceiling	MA	Good				10
	12x12 Floor Tile	F12	Good				
Women's Washroom	Pipe Fitting Insulation - Above Ceiling	PF	Good				5-10
	Mastic - Pipe - Above Ceiling	MA	Good				10
	Duct Insulation - Above Ceiling	DI	Good	Tested	Nov/ 10	10	
	12x12 Floor Tile	F12	Good				
Janitor's Room	Roof Drain	RD	Good				
	12x12 Floor Tile	F12	Good	Tested	Nov/ 10	3	
Photocopy Room	Roof Drain	RD	Good			~	

Material Location	Material Description	Drawing Label	Material Condition	Testing Status	Date M/Y	Test %	Est. %
	12x12 Floor Tile	F12	Good				
Hallway By Bathrooms	Pipe Fitting Insulation - Above Ceiling	PF	Good				5-10
	Mastic - Pipe - Above Ceiling	MA	Good				10
	Roof Drain	RD	Good				
Stores Area (102)							
Stores Area (102)	Pipe Fitting Insulation	PF	Good				
	Pipe Insulation	PI	Good				
	Roof Drain	RD	Good				
Uniform Stores Mezzanine	12x12 Floor Tile	F12	Good	Tested	Nov/ 10	0	
Tire Storage	Pipe Fitting Insulation	PF	Good				
	Pipe Insulation	Pl	Good				
	Plaster - Columns	PL	Needs Repair	Tested	Jan/ 12	0	
Receiving Bay	Spray On Insulation - Steel Beam	SO	Needs Repair	Tested		40-60	
	Pipe Insulation	PI	Good				
	Pipe Fitting Insulation	PF	Good				
Northwest Corner	Tank Insulation	TI	Good	Tested		POS	
	Pipe Fitting Insulation	PF	Good	Tested		POS	
	Pipe Insulation	PI	Good	Tested		NEG	
	Asbestos Fabric - Isolation Gasket	AF	Needs Repair	~ ·····			
Above Washroom	Pipe Fitting Insulation	PF	Removed 2011	Tested	Jan/ 12	5	
	Pipe Insulation	PI	Removed 2011				
Offices Beside Washroom	12x12 Floor Tile	F12	Removed'13	Tested	Nov/ 10	3	
	Sheet Flooring	SF	Removed'13				
Electrical & Engine Repair Area (103)							
Electrical & Engine Repair Area (103)	Pipe Fitting Insulation	PF	Good				
5 1 (,	Pipe Insulation	PI	Good				
Washroom	24x48 Ceiling Tile	C48	Removed	Tested	May/09	0	
	Pipe Fitting Insulation - Above Ceiling	PF	Good				
Battery Room	Pipe Fitting Insulation	PF	Good	1			
	Pipe Insulation	PI	Good				
<u>Unit Rebuild Area (104)</u>							
Unit Rebuild Area (104)	Pipe Fitting Insulation	PF	Good	1			
	Pipe Insulation	PI	Good				
North Area	Pipe Fitting Insulation	PF	Good				
	Pipe Insulation	PI	Good				
	Duct Insulation	DI	Good	Tested	Nov/ 10	0	

Material Location	Material Description	Drawing Label	Material Condition	Testing Status	Date M/Y	Test %	Est. %
Money Meter Room	Pipe Fitting Insulation	PF	Good				
	Pipe Insulation	PI	Good				
Engine Room	Pipe Fitting Insulation	PF	Good				
	Pipe Insulation	PI	Good				
Inspection Area (105)				~			
Inspection Area (105)	Wall Plaster- Top of Wall	PL	Good				1-2
	Stucco - On Ledge	ST	Good	Tested		1-2	
	Pipe Fitting Insulation	PF	Good				POS
	Pipe Insulation	PI	Good	~			NEG
	Drywall Compound - Top Of Wall	DC	Good				
	Roof Drain	RD	Good				
Sprinkler Room	Pipe Fitting Insulation	PF	Removed'14				
	Pipe Insulation	PI	Removed'14				
Sprinkler Room Mezzanine	Pipe Fitting Insulation	PF	Good	Tested	Jul/ 10	60	
	Pipe Insulation	PI	Good	Tested	Jul/ 11	0	
	Asbestos Fabric - Isolation Gasket	AF	Good				
Body Repair Area (106)							
Body Repair Area (106)	Pipe Fitting Insulation	PF	Good				
	Pipe Insulation	PI	Needs Repair				
	Plaster - Columns	PL	Good	Tested	May/09	0	
	Roof Drain	RD	Good	Tested	Aug/11	85	
Foreman's Office	Sheet Flooring	SF	Good	Tested	Jan/12	0	
Body Repair Area (106A)	5			~			
Body Repair Area (106A Weldig Shop)	Wall Plaster- Top of Wall	PL	Good	Tested		1-2	
	Roof Drain	RD	Good				
Aisleway East of Paint Booth #4	Spray On Insulation - Steel Beam	SO	Removed 2011	Tested		1-2	
2	Plaster - Columns	PL	Needs Repair	Tested	Sep/12	0	
	Plaster - Columns	PL	Good	Tested	Sep/14	<1	
Locker Area & Washroom	24x48 Ceiling Tile	C48	Needs Repair	Tested	00p/ 1 /	0	
	Pipe Fitting Insulation - Above Ceiling	PF	Good				
	Pipe Insulation - Above Ceiling	PI	Good				
	12x12 Floor Tile	F12	Removed 2011	Tested	Nov/10	2	
Carpenter Shop	Pipe Fitting Insulation	PF	Good				
· ·	Duct Insulation	DI	Good	-			
	Asbestos Fabric - Isolation Gasket	AF	Needs Repair	Tested	Sep/'14	60	
Paint Shop- Main Area	Pipe Fitting Insulation	PF	Good	Tested		15	
	Pipe Insulation	PI	Good	Tested	Aug/10	0	

Material Location	Material Description	Drawing Label	Material Condition	Testing Status	Date M/Y	Test %	Est. %
	roof drain	RD	Good				
	Spray On Insulation - Steel Beam	SO	Removed 2001	Tested	Sep/12	0	
Paint Boths #1-3	Drywall Compound - Ceiling	DC	Good				3
	Duct Insulation	DI	Needs Repair				75
	Duct Insulation - Above Ceiling	DI	Good				75
	Plaster - Columns	PL	Needs Repair	Tested	Sep/12	1	
	Spray On Insulation - Steel Beam - Above Ceiling	SO	Removed 2001				0
Paint Booth #4	Drywall Compound - Ceiling	DC	Removed 2012	Tested	Oct/11	3	
	Spray On Insulation - Steel Beam - Above Ceiling	SO	Removed 2012				
	Duct Insulation	DI	Removed 2012	Tested	Jul/12	75	
	Duct Insulation - Above Ceiling	DI	Removed 2012				75
	Plaster - Columns	PL	Removed 2012	Tested	Sep/12	2	
Paint Booth Fan Room	Duct Insulation	DI	Good	Tested	May/09	0	
	Spray On Insulation - Steel Beam - Above Ceiling	SO	Good				85
Brake Shop Area (107)							
Brake Shop Area (107)	Wall Plaster- Top of Wall	PL	Good				1-2
	Roof Drain	RD	Good	~			
	Stucco - On Ledge	ST	Good				1-2
	Pipe Fitting Insulation	PF	Good				
<u>General Repair Area (108)</u>							
General Repair Area (108)	Wall Plaster- Top of Wall	PL	Good	Tested	Mar/11	1-2	
	Stucco - On Ledge	ST	Good				1-2
	Pipe Fitting Insulation	PF	Good	Tested		POS	
	Pipe Insulation	PI	Good	Tested		NEG	
	Roof Drain	RD	Good	~			
Sprinkler Room	Pipe Fitting Insulation	PF	Removed'14				
	Pipe Insulation	PI	Removed'14				
Sprinkler Room Mezzanine	Pipe Fitting Insulation	PF	Good	Tested		60	
	Pipe Insulation	PI	Good	Tested		0	
	Asbestos Fabric - Isolation Gasket	AF	Good				
Washroom	Plaster - Walls	PL	Needs Repair	Tested	May/14	0	
nstruction Area (9)				~			
Hallway	12x12 Floor Tile	F12	Good	Tested	May/09	2-5	
	Mastic - Floor Tile	MA	Good	Tested	May/09	2-5	
Traffic Services Area (112)					- , 9		
Traffic Services Area (112)	Drywall Compound - Top Of Wall	DC	Good	-			1-2
	Pipe Insulation	PI	Good				0
	Pipe Fitting Insulation	PF	Good	-			15

Material Location	Material Description	Drawing Label	Material Condition	Testing Status	Date M/Y	Test %	Est. %
	Roof Drain	RD	Good	Tested	Aug/11	60	
Sign Shop	Drywall Compound - Top Of Wall	DC	Good				1-2
	Drywall Compound - Ceiling	DC	Good	Tested	Mar/11	2-3	
	Pipe Insulation	PI	Good	Tested		0	
	Pipe Fitting Insulation	PF	Good	Tested		15	
	Roof Drain	RD	Removed				
	Asbestos Fabric - Lined Safe	AF	Good				
	Spray On Insulation - Behind Steel Beam	SO	Good	Tested		5-30	
Offices	12x12 Floor Tile - Under Carpet	F12	Removed 2014				1-2
Parking Meter Repair Room	12x12 Floor Tile	F12	Needs Repair				1-2
	Sheet Flooring on Workbench	FS	Removed 2011	Tested	Nov/ 10	0	
	Asbestos Fabric - Lined Safe	AF	Removed				
	Sheet Flooring on Workdesk	FS	Removed 2011	Tested	Feb/11	4-15	
	Asbestos Fabric - Fireproof Cabinet	AF	Removed				
Communications Area (113)							
Garage Area	Pipe Fitting Insulation	PF	Good				
	Pipe Insulation	PI	Good				
Mezzanine	Roof Drain	RD	Good				
Office Hallway	12x12 Floor Tile	F12	Removed 2014	Tested	Nov/10	2	
Storage Area	Pipe Insulation	PI	Good				
	Pipe Fitting Insulation	PF	Good				

NOTES:

2. There may be asbestos containing materials present that were not located during asbestos inspections.

2. There may be asbestos containing materials present that were not located during asbestos inspections.

3. Floor tile and sheet flooring installed before 1990 may contain asbestos and must be treated as an asbestos containing material.

4. Vermiculite insulation may contain pockets of asbestos. All vermiculite insulation must be treated as an asbestos containing material.

5. For asbestos related inquiries, call Central Control at 204-986-2382

