



# COCKBURN AND CALROSSIE COMBINED SEWER RELIEF WORKS GEOTECHNICAL INVESTIGATION REPORT

# **FINAL**

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## 1.0 INTRODUCTION

## 1.1 GENERAL

KGS Group was retained by the City of Winnipeg Water and Waste Department to perform geotechnical investigations to facilitate the design and construction of the proposed Land Drainage System (LDS) trunk sewer pipe for the Cockburn and Calrossie Sewer Relief Works. This report outlines the geotechnical investigations completed within the alignment of Contracts 6 to 13. KGS Group has previously prepared geotechnical investigation reports for Contracts 1 to 5.

It is our understanding that LDS pipes ranging in size from 250 to 2400 mm will be installed in the Cockburn West and Southeast Jessie District as part of Contracts 6 to 13. The pipe will be installed from Poseidon Bay to Pembina Highway and from Grant Ave. to Taylor Ave.

The purpose of our investigations was to identify the subsurface soil and groundwater conditions along the route of the proposed works. This report contains a description of the geotechnical investigations program performed by KGS Group, our findings and geotechnical design recommendations for the proposed storm sewer.

### 1.2 PURPOSE OF REPORT AND LIMITATIONS

This report summarizes the geotechnical condition observed within the alignment of Contracts 6 to 13 and provides construction considerations that would form part of the basis of the design for the Work. This report includes:

- Geotechnical data collected at the project site;
- Summary of anticipated subsurface conditions along the pipe alignment; and
- A discussion of design and construction considerations including requirements for excavations, temporary support, groundwater conditions and control, settlement and trenchless tunnel construction.

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The results of the geotechnical investigation carried out at the proposed site are presented in this report. This report presents the geotechnical engineer's best judgement of the subsurface and ground conditions anticipated to be encountered at the project site during construction. The soil stratigraphy has been interpolated between the test holes that were drilled along the alignment. While the actual conditions encountered in the field are expected to be within the range of conditions presented and discussed in this document, the spatial variability of actual subsurface and groundwater conditions that would be encountered at the site may vary from the simplified interpretation presented within this report.



# 2.0 BACKGROUND INFORMATION

### 2.1 PREVIOUS SITE INVESTIGATIONS

KGS Group has completed separate geotechnical investigations for the previous contracts associated with this work. Summaries of the investigations completed for Contract 4 (Wilton St. from Taylor Ave. to Parker SRB) and Contract 5 (Taylor Ave. from Nathaniel St. to Wentworth St.) are included below.

#### 2.1.1 Contract 4

KGS Group completed a geotechnical investigation for Contract 4 along the Wilton St. alignment from Taylor Ave to the Parker Storm Retention Basin (SBR). The 2016 investigation consisted of drilling nine (9) test holes to investigate the subsurface stratigraphic conditions. Ten (10) pneumatic piezometers were installed in the clay, silt till and bedrock to monitor the groundwater levels.

The stratigraphy observed during the 2016 site investigation generally consisted of a layer of fill over an extensive layer of high plasticity clay and silt till. Silt layers were encountered within the upper 3.0 m. The top of the silt till was encountered at elevations ranging from 219 to 220.8 m±. The test hole logs from the 2016 geotechnical investigation have been included in Appendix A.

A summary of the test hole locations and groundwater monitoring results for the test holes within Contract 6 to 13 pipe alignment are included on Tables 1 and 2, respectively.

#### 2.1.2 Contract 5

KGS Group completed a geotechnical investigation for Contract 5 along the Taylor Ave. alignment from Nathaniel Street to Wentworth Street. The 2017 investigation consisted of drilling 17 test holes to investigate the subsurface stratigraphic conditions. Six (6) vibrating wire piezometers, and nine (9) standpipe piezometers were installed in the clay, silt till and bedrock to monitor the groundwater levels.



The stratigraphy observed during the 2017 site investigation generally consisted of a pavement structure overlying an extensive layer of high plasticity clay, silt till and limestone bedrock. Silt layers were encountered within the upper 3.0 m. The top of the silt till was encountered at elevations ranging from 219 to 220.5 m ±. The test hole logs from the 2017 geotechnical investigation have been included in Appendix B.

A summary of the test hole locations and groundwater monitoring results for the test holes within Contract 6 to 13 pipe alignment are included on Tables 1 and 2, respectively.

### 2.2 REGIONAL GEOLOGIC SETTING

Winnipeg geology consisted of carbonate sedimentary bedrock overlaying Precambrian era granite and gneiss. The sedimentary rock consists of limestone, dolomite and shale to a lesser extent. Local geological maps indicate karst topography caused from dissolution of the soluble rock, and a heavily fractured upper bedrock layer. The karst topography is typically infilled with mixtures of silt, sand and gravel till material.

During the last glacial advance and retreat, Winnipeg's glacial till was laid down by ice masses. Glaciolacustrine deposits suspended in glacial lakes confined by ice masses settled to overlie the tills. Additional information on the regional geology can be found in Geological Engineering Report for Urban Development of Winnipeg, University of Manitoba (Ref 1).

## 3.0 SCOPE OF THE 2018 INVESTIGATION PROGRAM

#### 3.1 GENERAL

This section provides a summary of the 2018 field investigation program, and laboratory test results.

#### 3.2 TEST HOLE DRILLING AND SOIL SAMPLING

The test hole drilling and sampling program was completed by KGS Group from April 30 to May 9, 2018. The approximate locations of the test holes drilled within the alignment of Contracts 6 to 13 are shown in Figure 1 and a summary of the locations is presented in Table 1.

The program consisted of drilling 24 test holes to investigate the subsurface stratigraphic conditions. The information obtained from the site investigations will be used to facilitate the design and construction of the various components of the storm sewer line project including the excavation of the launch and reception shafts where trenchless installations methods will be used.

Maple Leaf Drilling Enterprises of Winnipeg, Manitoba provided the drilling services using a track mounted drill rig equipped with 125 mm solid stem augers and NQ coring. Soil samples were collected directly off the auger flights typically at 1.5 m (5 ft.) intervals or at changes in soil strata encountered during drilling. The soil samples were visually inspected for material type and classified according to the Modified Unified Soil Classification System (USCS).

Standard Penetration Tests were completed in the glacial till material to evaluate the in-situ density. Clay samples were tested with a field Torvane to evaluate consistency and estimate undrained shear strengths. Upon completion of drilling, the test holes were examined for indications of sloughing and seepage, and then backfilled. Detailed test hole log records incorporating all field observations, field test results, and laboratory test results are provided in the test hole log records in Appendix C.

#### 3.3 GROUNDWATER MONITORING

A total of four (4) vibrating wire piezometers and four (4) standpipe piezometers were installed in 2018. The vibrating wire piezometers were installed in the clay strata and the standpipe piezometers were installed in the silt till and bedrock. Table 2 summarizes the installation details and the groundwater monitoring to date. The installation details of the 2018 piezometers are shown on the borehole log records provided in Appendix C.

#### 3.4 LABORATORY TESTING

A diagnostic laboratory testing program was performed on representative soil samples to determine the relevant engineering properties of the subsurface soils relative to the trenchless construction method. Diagnostic testing completed included moisture content analyses, Atterberg Limit tests, and grain size analysis. All laboratory testing was completed at a local



laboratory accredited by Standards Council of Canada and testing was performed in accordance with ASTM standards. The results of the laboratory testing are shown on the test hole logs in Appendix A.

Previous geotechnical investigations for Contracts 1 to 5 included unconfined compressive strength testing and XRD testing of the cohesive soils.



TABLE 1
SUMMARY OF TESTHOLE LOCATIONS

Test hole ID	Location	Northing (m)	Easting (m)	Approx. Ground Surface Elevation (m)	Approx. Borehole Depth (m)
TH16-08	Approx. Shaft B	5,524,036	632,399	233.3	16.15
TH16-09	Approx. Shaft C - Taylor Ave. Boulevard East of Wilton	5,524,243	632,294	232.73	15.04
TH17-03	Approximately 140 m west of Wilton St.	5,524,167	632,150	232.32	12.80
TH17-09	West of Harrow St.	5,524,380	632,538	232.12	13.87
TH17-10	East of Harrow St.	5,524,422	632,614	231.76	18.14
TH17-12	West of Stafford St.	5,524,462	632,688	231.98	15.70
TH17-13	East of Stafford St.	5,524,501	632,754	232.10	15.32
TH17-15	Wentworth St.	5,524,580	632,875	231.79	17.98
TH17-16	Approximately 40 m west of Nathaniel St.	5,523,977	631,776	232.14	15.86
TH18-01	Approximately 50 m South of Grant Avenue	5,524,056	631,200	233.00	6.10
TH18-02	Approximately 25 m East of Nathaniel Street	5,523,806	631,337	232.42	9.14
TH18-03	Approximately 650 m East of Cambridge Street	5,523,808	631,450	232.35	10.67
TH18-04	Approximately 230 m West of Wilton Street	5,524,380	631,429	232.28	7.62
TH18-05	Approximately 20 m South of Grant Avenue	5,524,302	631,569		6.10
TH18-06	Approximately 80 m East of Wilton Street	5,524,230	631,751	231.76	9.14
TH18-07	Approximately 35 m East of Wilton Street	5,524,594	631,819	232.13	7.62
TH18-08	Approximately 80 m East of Wilton Street	5,524,353	631,973	231.70	7.62
TH18-09	Approximately 20 m East of Wilton Street	5,524,602	632,069	232.60	14.17
TH18-10	Approximately 25 m South of Grant Avenue	5,524,672	632,206	232.29	6.10
TH18-11	Approximately 40 m West of Harrow Street	5,524,533	632,127	232.31	9.14
TH18-12	Approximately 25 m West of Harrow Street	5,524,531	632,299	232.21	7.62
TH18-13	Approximately 50 m East of Stafford Street	5,524,370	632,183	232.19	10.67
TH18-14	Approximately 25 m East of Wentworth Street	5,524,816	632,341	232.65	7.62
TH18-15	Approximately 25 m East of Lilac Street	5,524,680	632,397	232.55	9.14
TH18-16	Approximately 25 m East of Wentworth Street	5,524,172	632,681	231.98	16.15
TH18-17	Approximately 25 m East of Ebby Avenue	5,524,639	632,672	231.96	7.62
TH18-18	Approximately 40 m East of Stafford Street	5,524,945	632,704	231.72	15.85
TH18-19	Approximately 15 m West of Pembina Highway	5,525,047	632,890	231.93	7.62
TH18-20	Southbound Pembina to Grant Yield Island	5,524,772	632,747		10.67
TH18-21	Approximately 50 m South of Grant Avenue	5,524,807	632,945	231.75	7.62
TH18-22	Approximately 25 m East of Nathaniel Street	5,524,784	632,587	231.97	7.62
TH18-23	Approximately 650 m East of Cambridge Street	5,525,034	633,041	231.80	3.04
TH18-24	Approximately 230 m West of Wilton Street	5,525,256	633,128	232.47	15.85



# 4.0 SITE STRATIGRAPHY

The site stratigraphy in the section is based on the test holes drilled during the 2018 geotechnical investigation as well as the following test holes from the 2016 and 2017 investigations: TH16-08, TH16-09, TH17-03, TH17-09, TH17-10, TH17-12, TH17-13, TH17-15 and TH17-16.

The stratigraphy at the site consists of pavement with granular fill overlaying clay with thin silt to clayey silt deposit at shallow depths. Beneath the silt deposit is an extensive layer of highly plastic clay overlying glacial silt till and limestone bedrock.

The overburden stratigraphy has been divided into five (5) layers, as follows:

- Pavement structure;
- Fill;
- Silt;
- Clay; and
- Glacial till.

The division of the soil layers is based on visual classification in the field and laboratory testing.

# 4.1.1 Pavement Structure

The pavement structure at the site generally consists of asphalt overlying concrete and a thin layer of granular base material or concrete overlying a thin layer of granular base. The asphalt and concrete ranged in thickness from 0.2 to 0.3 m. A thin layer of granular base material was observed in test holes TH17-03, TH17-09, TH17-10, TH17-12, TH17-13, TH17-15, TH18-01, TH18-02, TH18-11, TH18-12, TH18-18, TH18-21, and TH18-22.

All of the test holes were drilled on the road surface with exception to test holes TH16-08, TH16-09, TH17-16, and TH18-24.

# 4.1.2 Clay Fill

A layer of clay fill was encountered in test holes TH17-15, TH18-02, TH18-06 to TH18-10, TH18-13, TH18-15, TH18-17, TH18-18 and TH18-23. The clay fill material ranged in thickness from 0.1 to 1.3 m± and extended to a maximum depth of 1.5 m± below grade at elevation 230.2 m±. The clay fill was black in colour, damp, stiff in consistency, of high plasticity and contained organics.

# 4.1.3 Silt (ML)

A silt to clayey silt layer approximately 0.1 to 1.2 m± thick was encountered in 23 of the test holes at elevations ranging from 229.0 to 232.2 m±. The silt to clayey silt layer was tan in colour, moist and soft to firm in consistency. Two (2) silt layers were observed in test holes TH18-05, TH18-14, TH18-20, and TH18-21. Seepage is commonly observed within this silt layer. There may be a perched groundwater table within the silt layer. The moisture content of the silt ranges from approximately 20 to 35% and the unit weight is within the range of 18.8 to 20.4kN/m³ (Ref 1).

## 4.1.4 Clay (CH)

Underlying the fill and silt is a glaciolacustrine clay deposit. In decreasing occurrence, typically the predominant mineral composition of the lacustrine clay consists of montmorillonite (a member of the smectite family), illite, kaolimite and some mica (Graham and Sheilds, 1985). An extensive layer of highly plastic clay was encountered at elevations ranging from approximately 229.6 to 232.1 m±. The thickness of the high plasticity clay ranged from 9.6 to 11.9 m±. This deposit will be encountered during the excavation for the shafts and along the proposed pipe alignment and during the excavation. The upper layer of the clay deposit was mottled brown in colour and extended to approximately elevation 224.7 to 227.7 m±. The upper clay deposit was damp to moist, of high plasticity and stiff in consistency. The consistency decreases with depth from stiff to firm. The upper clay is highly fissured with the frequency of fissures decreasing with depth. The lower clay deposit was grey, moist, of high plasticity, and soft to firm in consistency, becoming softer with depth.



The clay deposit contained some silt inclusions and trace to some fine to coarse grained sand, and fine grained gravel. These non-plastic, non-clay materials generally occur throughout the clay deposit as varves, veins, seams, inclusions or pockets that are typically less than a centimeter in diameter. The tendency for horizontal orientation of the varves, veins, and seams introduce a visible macrostructure to the clay and are a contributing cause for the observed anisotropy in horizontal permeability and strength of the deposit. Quigley (1968) offers the explanation that frozen silt lumps were rafted into glacial Lake Agassiz by icebergs and dropped into the clays as frozen lumps. Baracos (1977) provided a more likely explanation, considering the sharply defined boundaries of the inclusions, that they were deposited not frozen but as cemented or lithified material which subsequently disintegrated into silt.

Typical moisture content in the clay ranges from 30 to 60%. Atterberg Limit tests within the brown and grey clay has shown the brown clay is typically more plastic than the underlying grey clay. Liquid Limits in the brown clay typically range from 80 to 110% and the Plastic Index from 60 to 80%. Liquid Limits in the grey clay typically range from 80 to 95% and the Plastic Index ranged from 50 to 75%.

Undrained shear strengths are generally higher within the upper clay zone with strengths decreasing approximately uniformly with increasing depth below 4 to 5 m. The higher undrained shear strength within the upper brown clay and lower shear strengths at depths near the till is caused by weathering near the ground surface and decreasing over consolidation ratios to approximately normally consolidated conditions near the bottom of the deposit. The undrained shear strength, as estimated from the field Torvane, in the upper clay ranged from 30 to 100 kPa with an average of 55 kPa and 20 to 60 kPa with an average of 32 kPa in the lower grey clay. Figure 2 shows variation of undrained shear strength in clay deposit with elevation.

Unconfined compressive strength testing was completed on clay samples taken during the 2016 and 2017 investigations. The measured unconfined compressive strength ranged from 43 to 117 kPa with an average of 82 kPa. Measured values within the upper brown clay are variable due to the fissures.



Liquid and Plastic Limits, Plastic Indices, moisture contents and unconfined compressive strengths are summarized on Table 3. The majority of the laboratory testing results for the clay deposit are within the typical ranges for the Winnipeg area.

XRD analysis was completed on two (2) clay samples from within the proposed LDS alignment. The results of the testing indicated the quartz content of the clay samples ranged from 18.3 to 20.2%, the clinochlore content ranged from 13.3 to 15.7%, the muscovite content ranged from 15.4 to 20.3%, the calcite content ranged from 3.7 to 4.4%, the dolomite content ranged from 6.0 to 9.5%, and the smectite content ranged from 35.9 to 37.1%. High smectite content is often associated with high clogging potential during tunneling.

## 4.1.5 Glacial Till (ML-CL)

Silt till deposit was encountered below the clay deposit at elevations ranging from 218.9 and 222.4 m±. The silt till deposit ranged in thickness from 0.9 to 3.8m±. A layer of clay till was encountered in test hole TH16-09 below the silt till at an elevation of 218.7 m±. The silt till was found to be tan in colour, damp, loose to very dense and contained some to with fine to coarse grained sand and gravel. Boulders and cobbles are commonly found within the till layer and should be anticipated within the deposit at the project site.

The Standard Penetration Test (SPT) blow counts for 300 mm ranged from 5 to greater than 50 blows. The till was classified as very dense (greater than 50 blows for 300 mm) for five (5) SPT and SPT refusal was encountered during four (4) tests on suspected boulders. A summary of the uncorrected SPT N values recorded in the silt till are presented in Table 4 of this report.

Unconfined compressive strengths ranging from 3.4 to 3.6 MPa have been reported for very dense silt tills with a moisture content of about 5% (Ref 1). Young's moduli typically range from 170 to 240 MPa (Ref 1). The tills are highly variable in terms of thickness, density and boulder content.

#### 4.1.6 Boulders

Cobbles and boulders were not directly observed during the geotechnical investigation. Premature refusal of SPT spoons in the test holes within the till deposit typically indicate the presence of cobbles and boulders in the silt till or at the bedrock surface. Occasional cobbles and boulders were observed within the clay layer during previous tunneling projects within the vicinity of this project. The LDS pipe will be installed within the clay layer, a minimum of 5 m above the silt till interface. The tunneling should not be impacted by the cobbles and boulders within the silt till; however, occasional cobbles may be encountered in the clay layer.

### 4.2 BEDROCK

The majority of the bedrock encountered at the site was dolomite with dolomite limestone, limestone and interbedded shale and dolomite observed in some of the core holes. The elevation of bedrock varied from El. 215.8 to 219.6 m±. The bedrock will not be encountered during the pipe installation.

### 4.3 SEEPAGE, SLOUGHING AND GROUND WATER CONDITIONS

Water infiltration was observed in four (4) of the test hole after drilling. The elevation of the water immediately after drilling ranged from 219.6 to 225.4 m±. Some sloughing was observed during the drilling program, test holes TH18-04 and TH18-06 sloughed to elevations 227.7 and 226.6 m± respectively.

As mentioned above, a total of four (4) pneumatic piezometers, eight (8) vibrating wire piezometers and ten (10) standpipe piezometers were installed. The piezometric levels are summarized in Table 2. It should be noted that groundwater levels will fluctuate seasonally and following precipitation events.

In general a slight downwards gradient from the clay into the silt till and bedrock was observed from most of the groundwater monitoring data. The groundwater readings ranged from elevation 224.3 to 231.4 m in the clay, elevations 224.8 to 227.2 m in the silt till and elevations 224.5 to

228.1 m in the bedrock. Details of the piezometer installations are included on the borehole logs.



TABLE 2
GROUNDWATER MEASUREMENTS

Test Hole:	TH16-08 TH16-09		TH17-10		TH17-12		TH17-13	TH17-13 TH17-15		TH17-16		TH18-09		TH18-16		TH18-18		TH18-24					
Ground Elevation (m):	23:	233.30		233.30 232.73		231.76	231.76	231.76	231.98	231.98	232.10	231.79	231.79	232.14	232.14	233	2.60	231.98		231.72		232.47	
Piezometer No.:	36896	36893	36897	36889	1700050	Standpipe	Standpipe	1700049	Standpipe	Standpipe	1700048	Standpipe	1702738	Standpipe	1800934	Standpipe	1800937	Standpipe	1500935	Standpipe	1800932	Standpipe	
Tip Elevation (m):	226.0	218.4	224.2	218.1	224.1	218.5	213.6	226.5	216.3	217.5	224.2	213.8	223.9	217.0	225.6	220.0	224.4	216.2	225.6	218.0	225.2	216.8	
Monitoring Zone:	Clay	Bedrock	Clay	Bedrock	Clay	Silt Till	Bedrock	Clay	Bedrock	Silt Till	Clay	Bedrock	Clay	Silt Till	Clay	Silt Till	Clay	Bedrock	Clay	Silt Till	Clay	Bedrock	
Date									<del>.</del>	<del>.</del>		<del>-</del>		<del>-</del>		<del>-</del>		<del>.</del>					
25-May-16	230.57	225.22	226.42	225.72																			
17-Jun-16	230.50	224.86	226.42	225.65																			
26-Aug-16			224.32	224.86																			
6-Oct-16			225.62	225.36																			
9-May-17			227.42	227.22	230.31	225.19	226.57	228.78	226.43	226.48	231.37	228.12											
14-Jun-2017			227.42	225.79	229.99	225.66	225.46	228.65	225.21	225.87	230.92	225.67											
25-Sep-2017			227.40	225.29	229.73	225.14	224.65	228.96	224.52	224.75	230.86	225.21											
16-Oct-2017													226.79	225.22									
29-May-2018															227.17	227.19	226.71	225.89	227.45	227.11	227.45	225.05	
6-June-2018					228.96	225.21	224.92	228.94	225.71		230.87		227.31	224.99									

## 5.0 DESIGN AND CONSTRUCTION CONSIDERATIONS

### 5.1 TRENCHLESS PIPE CONSTRUCTION METHODS

It is our understanding a portion of the work will be large diameter pipe installed by trenchless methods. The two (2) most viable trenchless pipe methods suitable for the proposed work and readily available locally for installing large diameter pipe are Microtunneling and Auger/Thrust Boring.

## 5.1.1 Microtunneling

Microtunneling is a remotely-controlled, guided, pipe-jacking operation that provides continuous support to the excavation face by applying mechanical or fluid pressure to balance groundwater and earth pressures. Support at the excavation face is a key feature of microtunneling, distinguishing it from traditional open-shield pipe-jacking. Microtunnel Boring Machines (MTBMs) have been used extensive and successfully to install gravity flow sewer lines requiring precise line and grade in weak clay soil deposits

Microtunneling installation technique requires a jacking shaft from which the pipe installation starts and a reception shaft at the opposite end of the pipeline to retrieve the MTBM which would be used to excavate underground along the pipe alignment. The MTBM is pushed into the earth by hydraulic jacks mounted and aligned in the jacking shaft. The jacks are then retracted and the slurry lines and control cables are disconnected. The pipe or casing to be installed is lowered into the shaft and inserted between the jacking frame and the MTBM or previously jacked pipe. Slurry lines and power and control cable connections are made, and the pipe and MTBM are advanced another drive stroke. This process is repeated until the MTBM reaches the reception shaft. Upon drive completion, the MTBM and trailing equipment are retrieved and all equipment removed from the pipeline.

MTBMs have a rotating cutting head to excavate the ground material; the spoil is transported through conveyor or piping system back to the jacking/launching shaft. The cutting head is turned by a hydraulic or electric motor while a pressurized slurry mixing chamber behind the cutter head maintain face stability. MTBMs are capable of independently counter-balancing



earth and hydrostatic pressures. Earth pressure is counter-balanced by careful control of advance rates and excavation rates of spoil materials. Groundwater pressure is counter-balanced by using pressurized slurry in the soil-mixing chamber of the MTBM.

Large diameter sewer line with drive lengths up to 410 m have been successfully completed for Contract 4 of this Work using MTBM.

# 5.1.2 Auger/Thrust Boring

Auger boring is ideal for installing pipe in relatively soft stable ground conditions such as clay located above the water table. The soil within the pipe is retained during auger boring to reduce the likelihood of ground settlement from excavation, making auger boring a popular installation method for installing utilities under highways, railways and levies where potential settlement is a concern.

The auger boring process uses an auger boring machine to rotate an auger placed within the pipe and fitted to a cutter head at the front of the pipe. The rotating cutter head, which is slightly larger in diameter than the pipe, excavates the soil in front of the pipe. The soil is transported back to the launching where it is removed by hand or machine. The auger boring machine advances along a track, which is aligned to drive the casing pipe on the designed grade. Once the machine reaches the end of the track arrangement, the auger chain is disconnected from the machine and the machine is moved back to the original starting point on the track where a new casing pipe segment and auger chain is connected to the machine and to the existing chain/cutter head. The excavation and thrust process is repeated until the project is completed. The auger chain is then withdrawn from the casing pipe and the pipe is cleaned of all remaining soil and ready to use.

### 5.2 LAUNCHING AND RECEIVING SHAFTS

For trenchless installation of the pipe launching and receiving shafts are required. The shafts will be constructed primarily within the clay deposit and may extend into the underlying till. General design and construction considerations are outlined below:



- The shaft locations will be used to launch and/or receive the TBM and provide space for construction activities;
- The shaft will be excavated through the clay and shoring may penetrate into the silt till.
- The Contractor is responsible for the design of the shoring and temporary support systems at the shaft locations;
- The temporary support systems must be designed to resist lateral earth pressures, lateral hydrostatic pressures, surcharge of equipment/material stockpiled adjacent to the shaft and control ground movements;
- Groundwater monitoring data is included on Table 2. A base slab capable of resisting buoyance and basal heave is required at the shaft locations unless the Contractor can demonstrate that heave is not a concern and that pressures can be relieved in a controlled manner;
- The design of the shaft complies with Manitoba Workplace Safety and Health Act and Regulation. The Contractor shall be required to submit design details and drawings for their shafts to the City of Winnipeg for approval; and
- All seepage water pumped from the shaft locations will be discharged according to City of Winnipeg requirements.

#### 5.2.1 Base Heave

The base of excavation and shoring should be designed to achieve a minimum factor of safety of 1.5 with respect to basal heave. Installation of groundwater monitoring wells may be required at shaft locations to measure the piezometric elevation in the vicinity of the shaft during construction. Depending on the groundwater conditions at the time of construction, groundwater depressurization may be required to achieve the specified factor of safety against basal heave.

#### 5.2.2 Care and Control of Water

In order to maintain safe working conditions in the excavation and to protect against instability of the excavation base, water will not be allowed to accumulate anywhere within the excavations. Effective drainage and sump pump systems will be required below the base of excavation to maintain a firm, dry working surface. The Contractor shall design the internal drainage system to efficiently collect groundwater seepage and all water inflow draining into the excavation shall be pumped out and treated or use a watertight concrete slab designed to resist uplift. The Contractor will be responsible to prevent surface runoff from entering the excavation.



### 5.3 TUNNELLING

Trenchless large diameter pipe installation may be required for a portion of the work. General design and construction considerations for the tunnel are outlined below:

- The Contractor must pick suitable equipment to properly handle the excavated material;
- The tunnel will be installed within the clay layer, a minimum of approximately 5.0 m above the glacial silt till deposit;
- The clay layer has a very high swelling potential, mitigation measures such as increasing the size of the overcut may be required depending on the trenchless pipe installation method selected by the Contractor. Furthermore, any activity that may result in a drastic change in the moisture content of the clay (drying or wetting) may aggravate the potential for swelling and should be avoided; and
- The Contractor is required to collect and discharge groundwater flows according with City of Winnipeg requirements.

### 5.3.1 Stickiness Potential and Clogging Risks

The clay deposit present at the site has a tendency to develop sticky behavior (adhesion of clay material to each other or to a metal surface). This stickiness may result in the clogging and blockage of the cutterhead, tooling, work chamber, screw conveyors (EPBM), muck carts, conveyors, slurry lines or prevent the shield advancement due to excessive friction.

The potential for clogging while tunneling through the clay formation was evaluated using the chart suggested by Hollmann and Thewes (2013). Atterberg limits (Liquid limit, Plastic limit, and natural moisture content) of clay samples tested in the Laboratory and their Plasticity Indices were plotted on Figure 3 to determine the corresponding clogging potential of the clay. It should be noted that the Hollmann and Thewes chart (Figure 3) was developed from data collected from fluid supported shield drives but are assumed to be applicable to other tunneling methods. Based on the Hollmann and Thewes chart the clay deposit at the site has high stickiness and strong clogging potential.

The additional effort that will be required for cleaning clogged components may lead to significant reduction in productivity and increased cost. Therefore, the tunneling system and separation plant (for a slurry supported shield drive) used for this project should be designed to

mitigate this potential clogging problem. Thewes and Burger (2004) suggested the following upgrades to the design of the TBM to mitigate the risk of clogging:

- Enlarge passages and other obstructions in the transport of clay chips from the tunnel face to the slurry line;
- Increase the ratio of suspension flow rate to the volume of excavated soil to prevent accumulation of clay in the chamber (circuit and flushing concepts);
- Avoid clay agglomeration by increasing agitation in areas prone to material settlement;
   and
- Avoid closed-type cutting wheels.

Other mitigating measures include optimizing the cutting tools' penetration to get a favorable clay chip size, the use chemical additives and provision of high pressure water jets in the cutter head chamber.

## 5.4 EXCAVATIONS

Temporary excavations will be required to facilitate the construction of the proposed LDS pipe sewer. All excavation work are required to be performed in accordance with the Workplace Safety and Health Act and Part 26 of the Manitoba Workplace Safety and Health Regulation, M.R. 217/2006.

Excavations performed adjacent to the existing roadway or infrastructure, require temporary shoring or bracing. Excavations deeper than 1.5 m are required to be designed and approved prior to construction by an experienced professional engineer with an expertise in geotechnical engineering. The shoring design should account for all applicable surcharge loads. Opening and voids behind shoring lagging or sheet piles will be backfilled with cement grout.

The silt layers are known to be water bearing and are susceptible to strength loss when subjected to mechanical disturbance and sloughing from wetting. All open excavation side slopes will be covered with water proof material to prevent saturation of the soil and all surface runoff will be directed away from the excavations. The Contractor will maintain all surcharge

loads such as stockpiled soil, equipment, etc. a minimum of 10 m away from the edge of excavations.

During the site investigations water infiltration was observed in some of the test holes as discussed in Section 3.7. Temporary pumping may be required as well as potential shoring. Design of the above measures depends on the size, depth and extent of the excavation.

### 5.4.1 IMPACT ON EXISTING STRUCTURES

Excavation support systems will be designed by the Contractor to control ground movement/subsidence around the perimeter of the excavation. Potential settlement of the ground surface adjacent to temporary shoring system should be recognized and accounted for in the design. Any resulting movement/settlement around the perimeter of the excavation and of utilities, roadways, and buildings must be kept within acceptable limits.

The excavation and shoring system will be designed by a professional engineer with extensive relevant experienced and the works must be inspected and certified by the same professional engineer to verify that the temporary structure has been installed according to the design.

#### 5.4.2 BASE HEAVE

The stability of the bottom of the excavation could be compromised if the high plastic clay is overstressed and allowed to shear. The base of excavation and shoring should be designed to achieve a minimum factor of safety of 1.5 with respect to basal heave.

#### 5.4.3 CARE AND CONTROL OF WATER

The base of the excavations may to be below the groundwater level during construction. In order to maintain safe working conditions in the excavation and to protect against instability of the excavation base, the water should not allowed to accumulate anywhere within the excavations or to within 0.5 m below the lowest point within the excavation. Therefore, it will be important to have an effective drainage and sump pump system below the base of excavation,



and to maintain a firm, dry working surface. The drainage system should be designed to efficiently collect groundwater seepage and surface water drainage within the excavation so it can be pumped out and treated. Surface run-off resulting from rainfall should be controlled and prevented from entering into the excavation.

### 5.5 LATERAL EARTH PRESSURES

For design purposes the soils may be assigned active, at-rest and passive lateral earth pressure coefficients as shown in Table 5.

TABLE 5
LATERAL EARTH PRESSURE COEFFICIENTS

Backfill Material	ф'	Ka	K <sub>0</sub>	<b>K</b> <sub>p</sub>
Till	25 <sup>°</sup>	0.41	0.58	2.46
Native Clay	18 <sup>°</sup>	0.53	0.69	1.89
Well Graded Compacted Granular	35°	0.27	0.43	3.69

#### 5.6 GROUNDWATER MANAGEMENT AND SPOIL DISPOSAL

The Contractor is expected to be familiar with and follow all local spoil disposal regulations including all monitoring, analysis, permits and treatment required by the City of Winnipeg. Transportation and disposal of the spoil material is required to comply with all applicable laws and regulations. The Contractor will be required to obtain all necessary permits/approvals for the discharge of groundwater. Routine monitoring of groundwater discharge quality by the Contractor will be required during construction.

#### 5.7 FROST PENETRATION

The expected depth of frost penetration has been estimated assuming a design freezing index of 2680°C days, taken as the coldest winter over a ten (10) year period. The estimated maximum depth of frost penetration is 2.5 m assuming no insulation cover.

## 5.8 CORROSION POTENTIAL

The degree of exposure of concrete in contact with soils to sulphate attack is classified in CAN/CSAA23.1-M94 (Concrete Materials and Methods of Concrete Construction) as moderate (S-3), severe (S-2) or very severe (S-1). All concrete utilized in foundation elements should have a minimum specified 28 day compressive strength of 35 MPa and class of exposure of S-1, corresponding to very severe sulphate attack. A maximum water to cement ratio of 0.40 should be specified in accordance with Table 2, CSA A23.1-09 for concrete with very severe sulphate exposure (S-1). Concrete which may be exposed to freezing and thawing should be adequately air entrained to improve freeze-thaw durability in accordance with Table 4, CSA A23.1-09.



## 6.0 CLOSURE

The geotechnical investigation conducted by KGS Group describes the underlying soil and groundwater conditions along the proposed alignment for Contracts 6 to 13 at the test hole locations. This report presents the geotechnical engineer's best judgment of the subsurface and ground conditions anticipated to be encountered at the project site during construction. In order to develop the design, it was necessary to interpolate between the test holes that were drilled at the site. While the actual conditions encountered in the field are expected to be within the range of conditions discussed in this document, the spatial variability of subsurface and groundwater conditions that would be encountered at the site may be more complex than the simplified interpretation presented in this report.

To facilitate project design, certain assumptions were made with respect to the construction methods and on the level of workmanship that can reasonably be expected for the construction of a large diameter sewer project. It should be noted that the Contractor's selected equipment, means, methods, and workmanship will influence the behaviour and performance of the subsurface soils encountered at the site.

Full time inspection by qualified geotechnical personnel is recommended during construction to ensure that design intent is achieved and to address any issue that may arise due to variability in soils condition.



# 7.0 REFERENCES

1. Department of Geological Engineering, the University of Manitoba, (1983). Geological Engineering Report for Urban Development of Winnipeg.



## 8.0 STATEMENT OF LIMITATIONS

### 8.1 THIRD PARTY USE OF REPORT

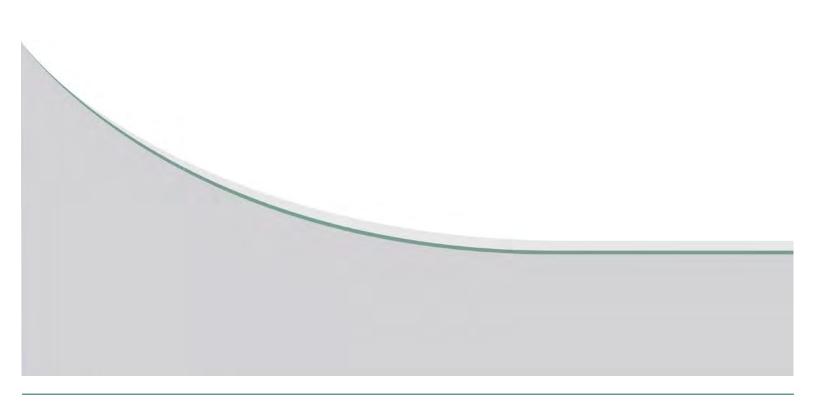
This report has been prepared for the City of Winnipeg to whom this report has been addressed and any use a third party makes of this report, or any reliance on or decisions made based on it, are the responsibility of such third parties. KGS Group accepts no responsibility for damages, if any, suffered by any third party as a result of decisions made or actions undertaken based on this report.

#### 8.2 GEOTECHNICAL INVESTIGATION STATEMENT OF LIMITATION

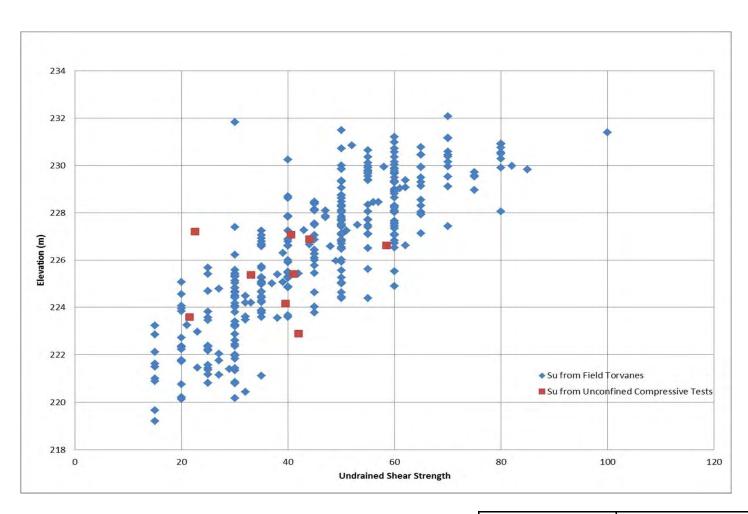
The geotechnical investigation findings and recommendations of this report were prepared in accordance with generally accepted professional engineering principles and practice. The findings and recommendations are based on the results of field and laboratory investigations, combined with an interpolation of soil and groundwater conditions found at and within the depth of the test holes drilled by KGS Group at this site. If conditions encountered during construction appear to be different from those shown by the test holes drilled by KGS Group or if the assumptions stated herein are not in keeping with the design, this office should be notified in order that the recommendations can be reviewed and modified if necessary.



# **FIGURES**







NOTES:





Cockburn/ Calrossie Combined Sewer Relief Project

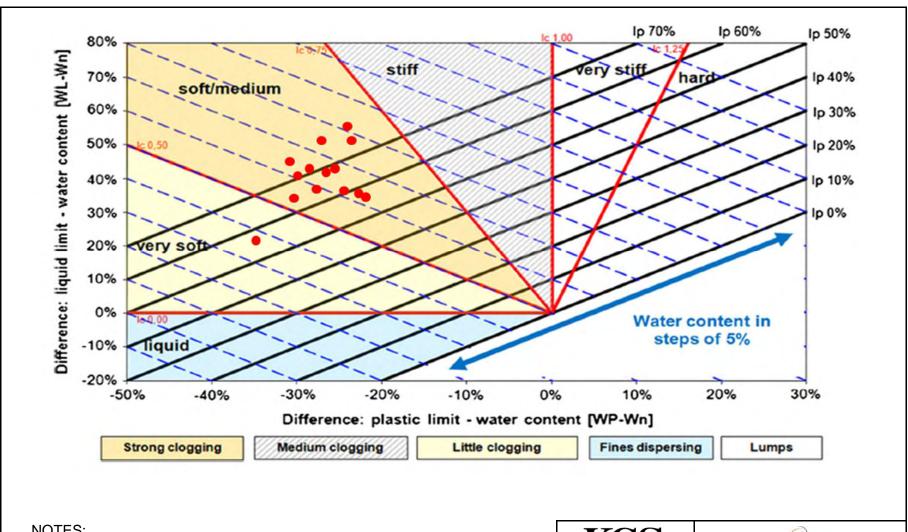
## Geotechnical Factual Report

Undrained Shear Strength of Clay Deposit

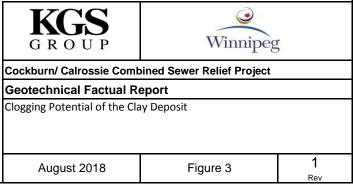
August 2018

Figure 2

1 Rev



NOTES:



August 2018 KGS 11-0107-18

# **TABLES**

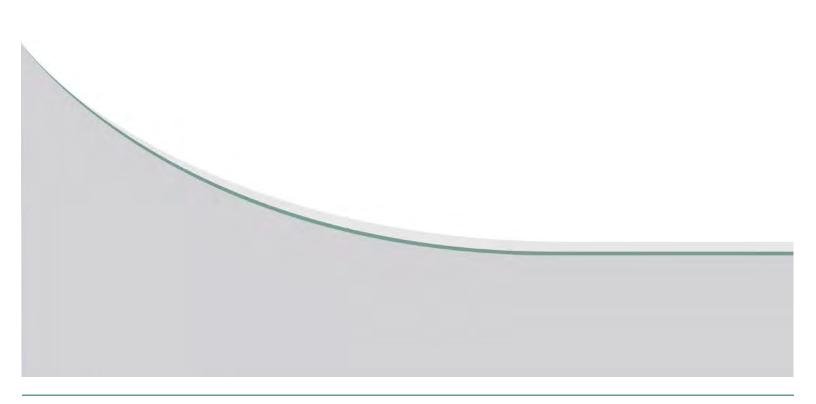




Table 3
Summary of Laboratory Testing Results

	Sample				Unconfined			Grain Siz	ze Analyses			Att	erberg Lin	rberg Limit				
Testhole ID		Sample Depth (m)	Description	Moisture content (%)	Compressive Strength (kPa)	Gravel (> 4.75 mm)	Coarse Sand (2- 4.75 mm)	Medium Sand (0.425-2 mm)	Fine Sand (0.075-0.425 mm)	Silt (0.002- 0.075 mm)	Clay (<0.002 mm)	Liquid Limit (%)	Plastic Limit (%)	Plastic Index				
	S3	2.0	Silt	24.8														
	S5	3.1	Clay	51														
TH16-08	S7	5.3	Clay	57.5								100	30	70				
11110-08	S8	6.1	Clay	52.9	45	0	0	0.1	0.3	18.2	81.4	95	29	66				
	S11	9.1	Clay	58.1	79							81	23	58				
	S13	12.2	Clay	47.9														
	S3	3.7	Clay	52.2														
TH16-09	S6	6.1	Clay	57.4	117	0	0.1	0.3	0.5	18.2	80.9	98	29	69				
1010-09	S9	9.1	Clay	46.5	43							85	25	60				
	S12	12.2	Silt Till	54.1														
TH17-09	S10	12.8 to 13.1	Silt till	22.8														
1017-09	S11	13.4 to 13.7	Silt till	13.1		9.4	6.2	10	14.9	39.2	20.3							
	S1	0.9 to 1.2	Silty clay	34.2														
	S3	3.7 to 4.0	Silty clay	54.2								106	31	75				
TH17-10	S6	6.1 to 6.7	Silty clay	47.8	66							86	24	62				
11117-10	S9	8.2 to 8.5	Silty clay	53.0														
	S11	11.3 to 11.6	Silty clay	48.5								88	24	64				
	S12	13.1 to 13.4	Silt till	14.8		3.5	6.4	11.3	14.8	46.9	17.1							
TH17-12	S4	4.6 to 5.2	Silty clay	54.0	81													
1017-12	S8	7.6 to 8.2	Silty clay	50.9	84													
	S1	1.2 to 1.5	Silty clay	36.0														
T1147.45	S4	4.6 to 5.2	Silty clay	51.8	88							108	28	80				
TH17-15	S6	6.1 to 6.7	Silty clay	50.4	82							91	26	65				
	S12	12.8 to 13.1	Silt till	13.0														
	S3	1.2 to 1.5	Clay	34.1														
TH18-01	S5	3.8 to 4.1	Clay	50.4														
	S6	5.3 to 5.6	Clay	46.9														



П					<u> </u>			T	<del>                                     </del>			1	
TH18-03	S1	0.8 to 1.1	Silt	26.2									
	S3	2.3 to 2.6	Clay	47.9									
	S5	5.3 to 5.6	Clay	10.8									
	S7	8.4 to 8.7	Clay	49.7							96	22	74
	S9	10.4 to 10.7	Clay	21.7									
	S1	0.8 to 1.1	Clay	31.3									
TH18-04	S3	3.5 to 3.8	Clay	62.1									
	S4	6.4 to 6.7	Clay	53.6									
	S3	2.3 to 2.6	Clay	48.6									
TH18-06	S5	5.5 to 5.8	Clay	47.5									
	S6	7.0 to 7.3	Clay	52.0									
	S2	1.2 to 1.5	Clay	36.7									
	S4	3.8 to 4.1	Clay	50.4									
TH18-09	S5	5.3 to 5.6	Clay	49.8							100	24	76
1110-09	S7	8.4 to 8.7	Clay	43.3									
	S8	9.8 to 10.1	Clay	50.7									
	S11	11.4 to 11.7	Silt Till	16.3	3.8	6.1	11.1	15.7	49.8	13.5			
	S3	1.1 to 1.4	Clay	31.9									
TH18-13	S6	3.8 to 4.1	Clay	47.6									
	S8	7.0 to 7.3	Clay	46.6									
	S3	1.5 to 1.8	Clayey silt	23.1									
	S4	2.4 to 2.7	Clay	45.7									
TH18-14	S6	3.1 to 3.4	Clay	51.3									
	S8	3.8 to 4.1	Clay	54.2									
	S10	7.3 to 7.6	Clay	47.0									
	S2	0.9 to 1.2	Clayey Silt	17.2									
TU40.45	S3	2.3 to 2.6	Clay	45.6									
TH18-15	S5	3.8 to 4.1	Clay	49.3									
	S6	6.7 to 7.0.	Clay	53.1									
	S2	2.3 to 2.6	Clay	50.2									
T1140 40	S4	3.8 to 4.1	Clay	49.3									
TH18-16	S6	8.4 to 8.7	Clay	49.7							86	29	57
	S8	11.3 to 11.6	Clay	44.6									



	S9	11.9 to 12.2	Silt Till	25.0									
	S11	13.1 to 13.4	Silt Till	12.9	12.6	6.3	8.1	13.6	42.9	16.5			
	S2	0.9 to 1.2	Clay Fill	31.4									
	S3	2.3 to 2.6	Clay	51.9									
	S5	3.8 to 4.1	Clay	56.3							93	26	67
TH18-18	S7	8.4 to 8.7	Clay	52.9									
	S9	11.3 to 11.6	Clay	51.8									
	S11	12.8 to 13.1	Silt Till	19.2									
	S12	13.4 to 13.7	Silt Till	14.3	8.5	6.1	9.1	13.4	45.0	17.9			
	S1	0.3 to 0.6	Clayey silt	29.0									
TH18-19	S4	2.8 to 3.1	Clay	52.2									
	S6	3.8 to 4.1	Clay	49.4									
	S1	0.8 to 1.1	Clay	34.9									
	S2	1.7 to 2.0	Clayey silt	42.4									
TH18-20	S3	2.5 to 2.8	Clay	48.9									
11110-20	S5	4.9 to 5.2	Clay	52.1									
	S7	7.0 to 7.3	Clay	51.5									
	S9	10.0 to 10.3	Clay	54.1									
	S2	0.8 to 1.1	Clayey Silt	27.0									
TH18-24	S5	2.5 to 2.8	Clay	43.5									
11110-24	S6	3.8 to 4.1	Clay	53.7									
	S7	5.2 to 5.5	Clay	56.0									

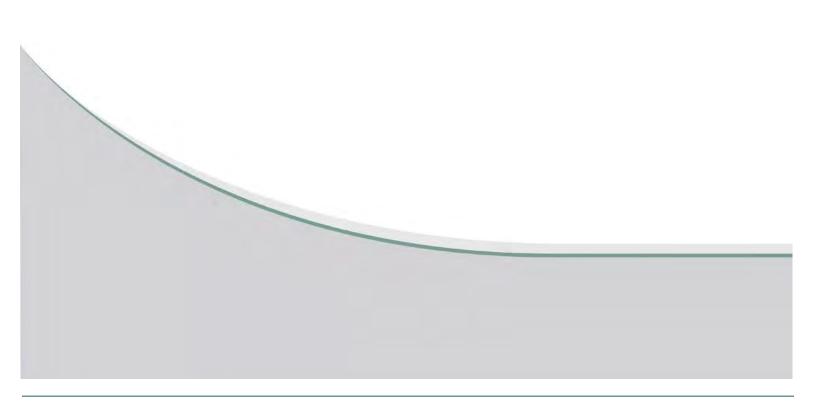


## TABLE 4 GLACIAL TILL – SPT SUMMARY

Density	Frequency
Very Loose (0-4 blows/0.3 m)	1
Loose (4-10 blows/0.3 m)	2
Compact (10-30 blows/0.3 m)	4
Dense (30-50 blows/0.3 m)	0
Very Dense (greater than 50 blows/0.3 m)	3
Spoon Refusal ( greater than 50 blows for less than 0.3 m)	6



## APPENDIX A 2016 TEST HOLE LOGS





## KGS GROUP

## SOIL DESCRIPTION CRITERIA

## PRINCIPAL AND MINOR SOIL COMPONENTS

And 35-50% With 20-35% Some 10-20% Trace 0-10%

Occasional Trace of very local concentration

## FIELD MOISTURE CONTENT

Dry No moisture visible or to touch when fresh exposure is examined

Damp Slightly wet to touch Moist Fresh exposure wet to touch

Wet A film of water is readily visible around particles of granular soils, cohesive soils can readily be smeared or remolded; water can be squeezed

out

Saturated Water can easily be squeezed out

Free Water Water completely separated from the soil particles

#### DEPOSITIONAL STRUCTURE

Massive Structureless soil

Stratified (Layered) Different soils or visible variations in soil constituents arranged in layers, generally but not necessarily parallel to one another,

and not necessarily in horizontal position, at least 6 mm thick

Varved Glaciolacustrine deposits with annual pairs of fine and coarser laminae (thin laminae of alternately deposited inorganic silt and

clay)

Laminated Closely spaced, regularly alternating layers of differing soils and/or colours, or shades of similar gradation, relatively consistent in

thickness and consisting of sand, silt, or clay

Lens Inclusions of a different soil within surrounding soils, which thins out horizontally and may not be continuous over any

significant distance

Pocket A different soil type of very limited thickness or lateral extent (a small lens)

Inclusions Small pockets

Nuggety A different soil type in the form of small lumps Parting Paper thin separation of one type by another

## POST DEPOSITIONAL STRUCTURE

Fissured A soil breaks along definite, pre-existing planes or fracture with little resistance to fracturing

Slickensided Polished or glossy, sometimes striated surfaces resulting from movement of a material block relative to the adjacent blocks
Blocky/Friable/Platy Cohesive soil that can be broken down into angular larger fragments (blocky), small fragments (friable), or thin plate-like

fragments (platy) which resist further breakdown

Cemented Soil particles or fragments held together by cemented materials, often chemical precipitants, or deposits within overall soil mass

## GRAIN SIZE DISTRIBUTION IN COARSE GRAINED SOIL

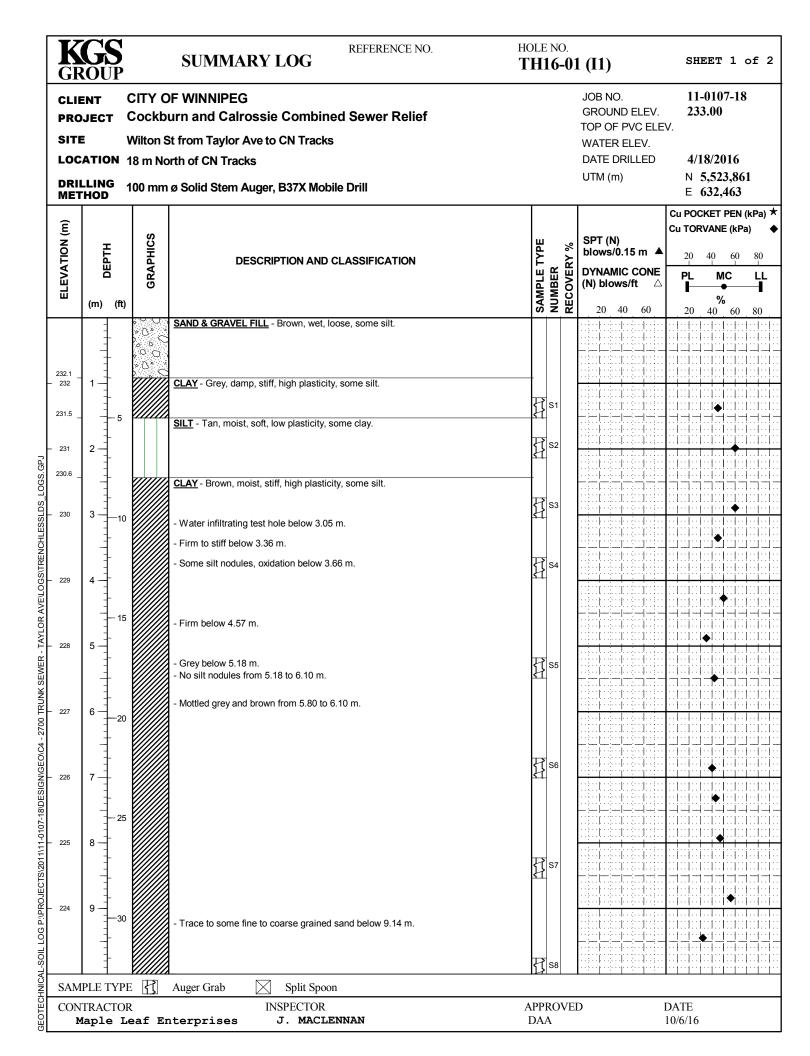
 $\begin{array}{lll} \mbox{Boulders} & >& 200 \mbox{ mm } \mbox{\o} \\ \mbox{Cobbles} & 75-200 \mbox{ mm } \mbox{\o} \\ \mbox{Coarse Grained Gravel} & 19-75 \mbox{ mm } \mbox{\o} \\ \mbox{Fine Grained Sand} & 4.75-19 \mbox{ mm } \mbox{\o} \\ \mbox{Coarse Grained Sand} & 2-4.75 \mbox{ mm } \mbox{\o} \\ \mbox{Medium Grained Sand} & 0.425-2 \mbox{ mm } \mbox{\o} \\ \mbox{Fine Grained Sand} & 0.075-0.425 \mbox{ mm } \mbox{\o} \\ \mbox{\o} \end{array}$ 

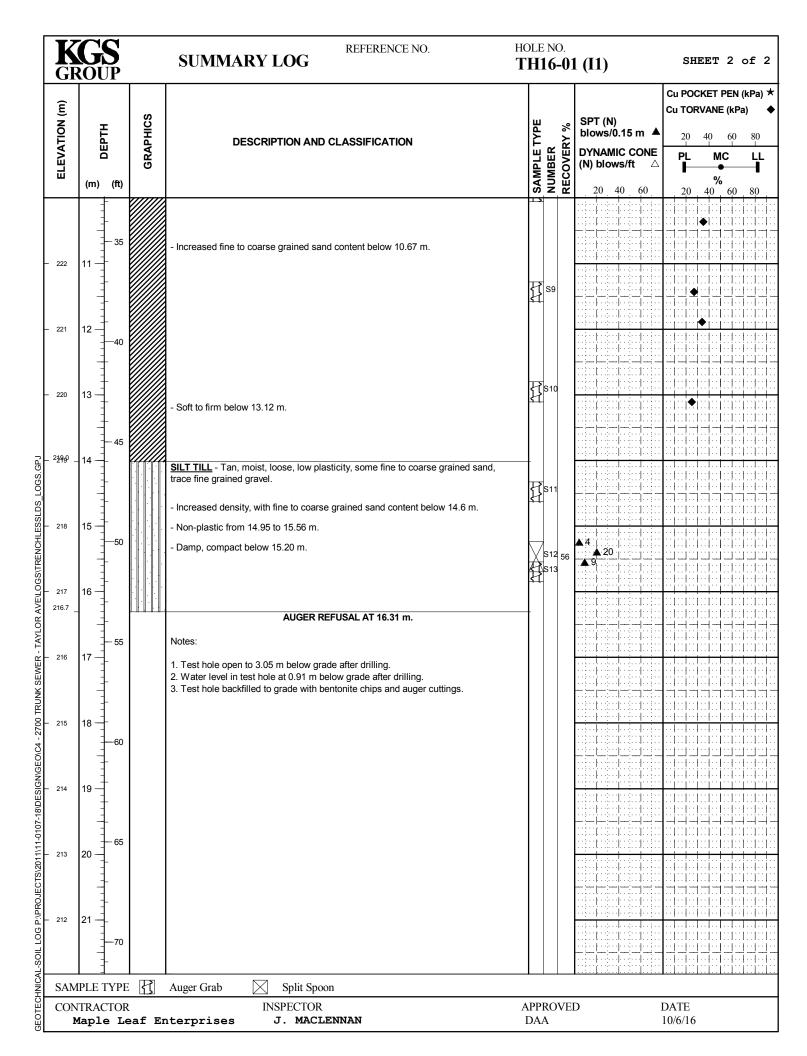
## DENSITY OF GRANULAR SOIL

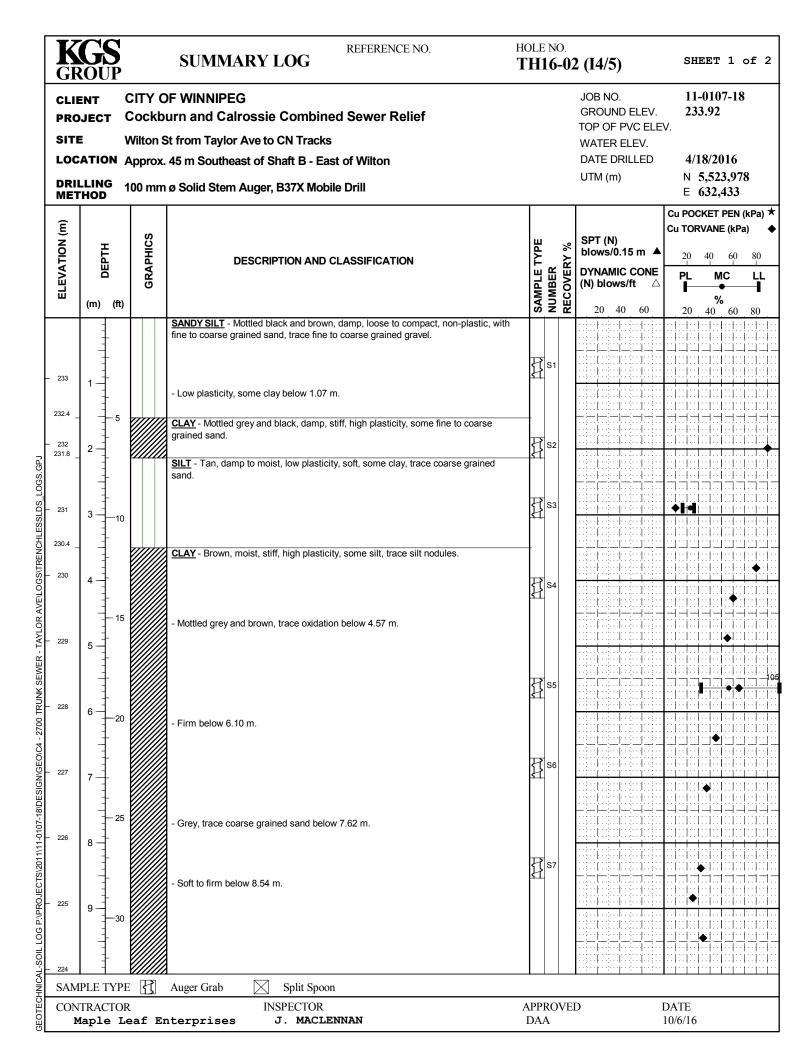
Description	Standard Penetration Test	Relative Density
Very Loose	0-4 Blows Per $0.3$ m	<15%
Loose	4 – 10 Blows Per 0.3 m	15 - 35%
Compact	10 - 30 Blows Per 0.3 m	35 - 65%
Dense	30 - 50 Blows Per 0.3 m	65 - 85%
Very Dense	>50 Blows Per 0.3 m	>85%

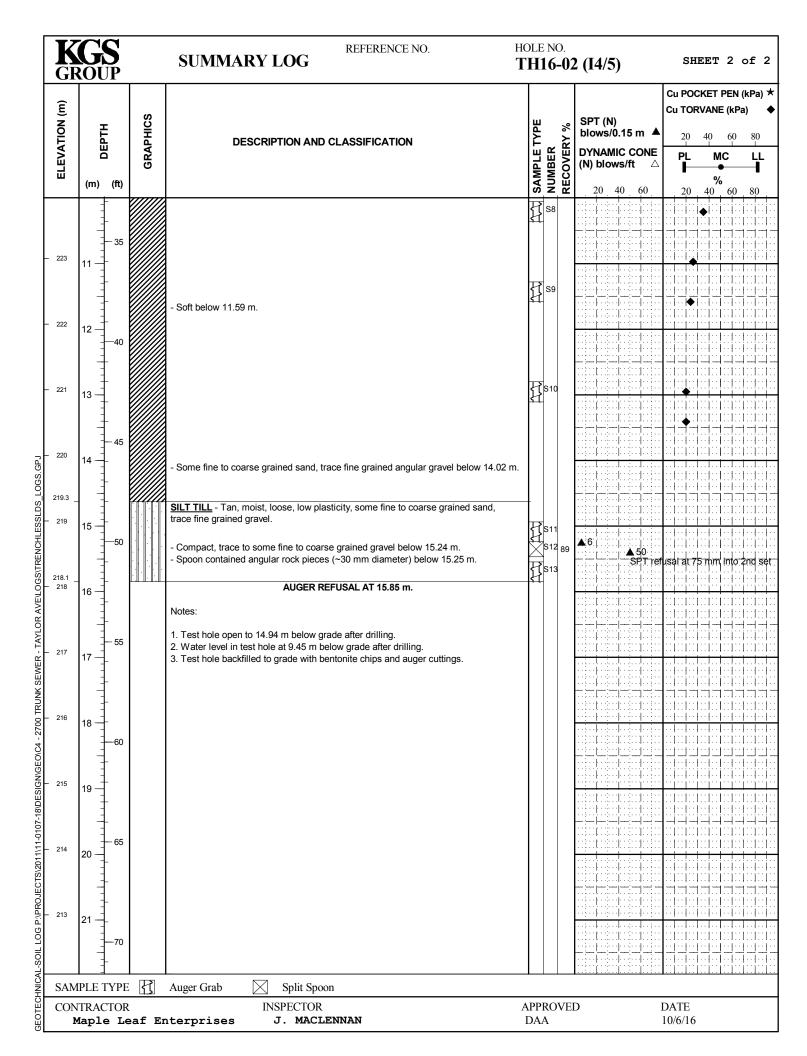
#### CONSISITENCY OF COHESIVE SOILS

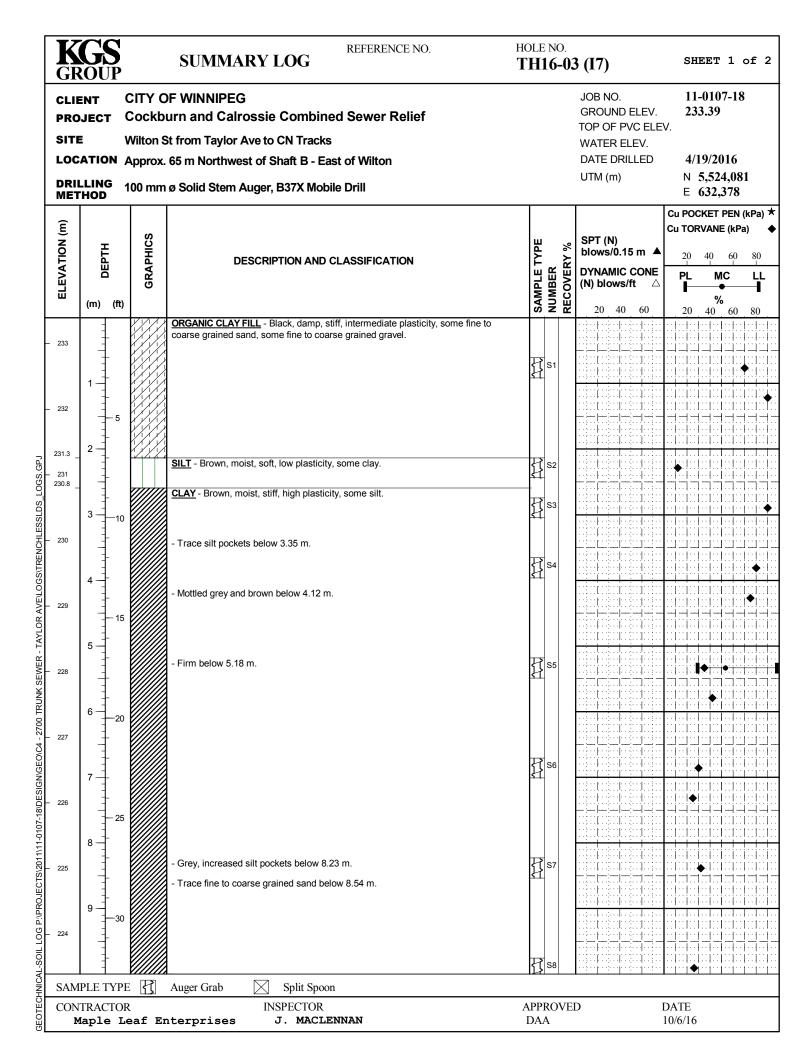
Description	Torvane	Standard Penetration Test
Very Soft	<12 kPa	<2
Soft	12 – 25 kPa	2 - 4
Firm	25 - 50  kPa	4 - 8
Stiff	50 - 100  kPa	8 - 15
Very Stiff	100 - 200  kPa	15 - 30
Hard	>200 kPa	>30

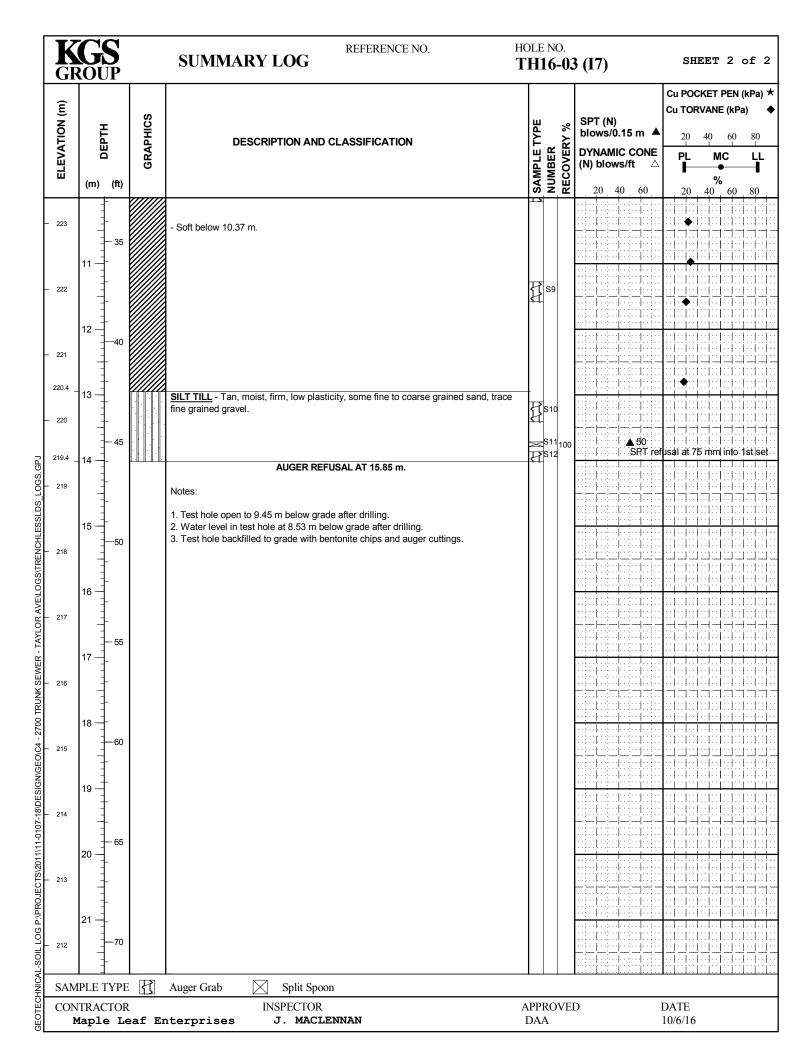


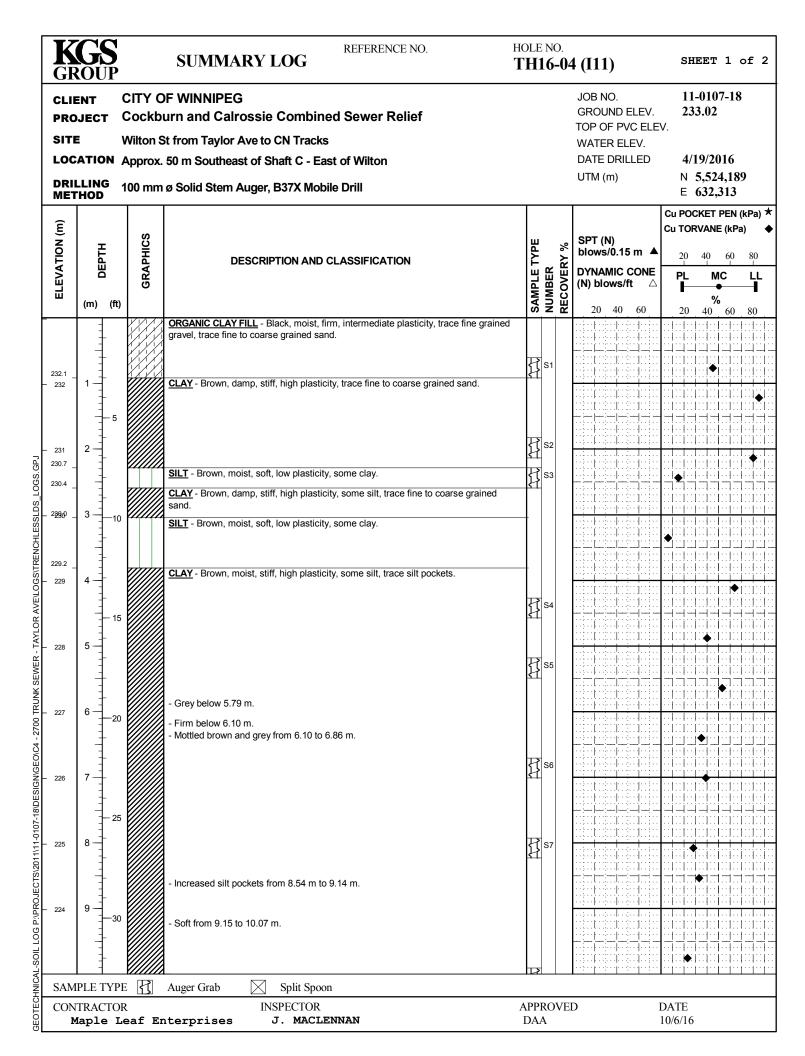


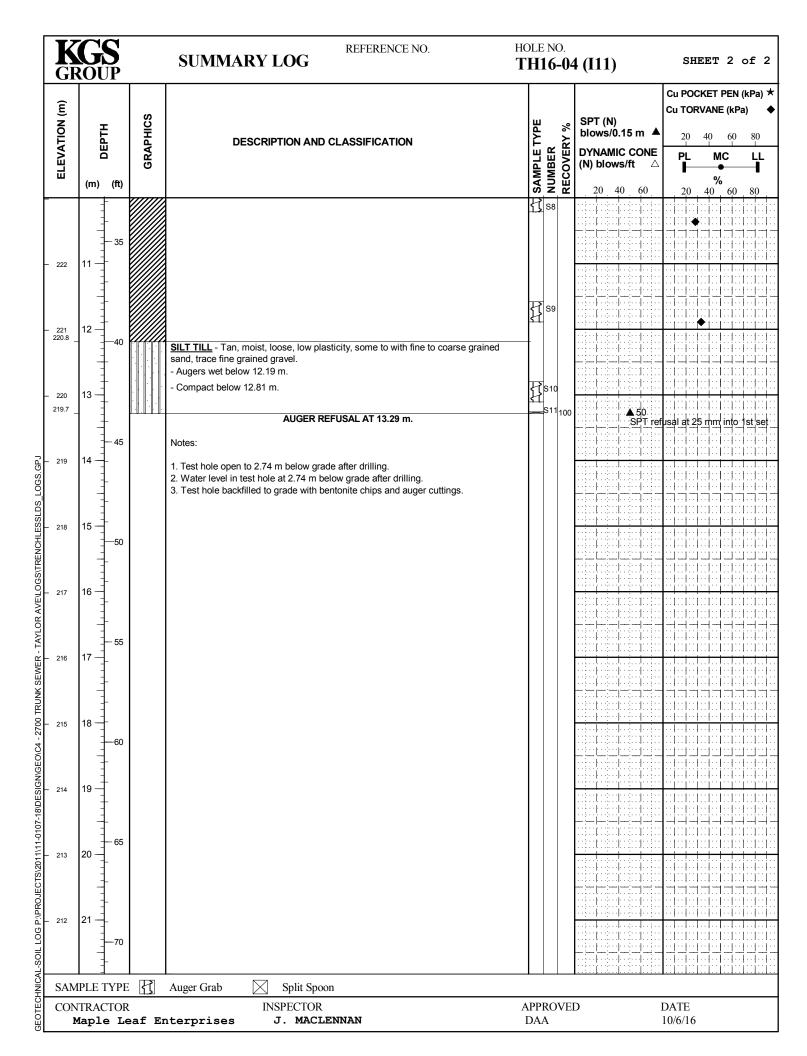


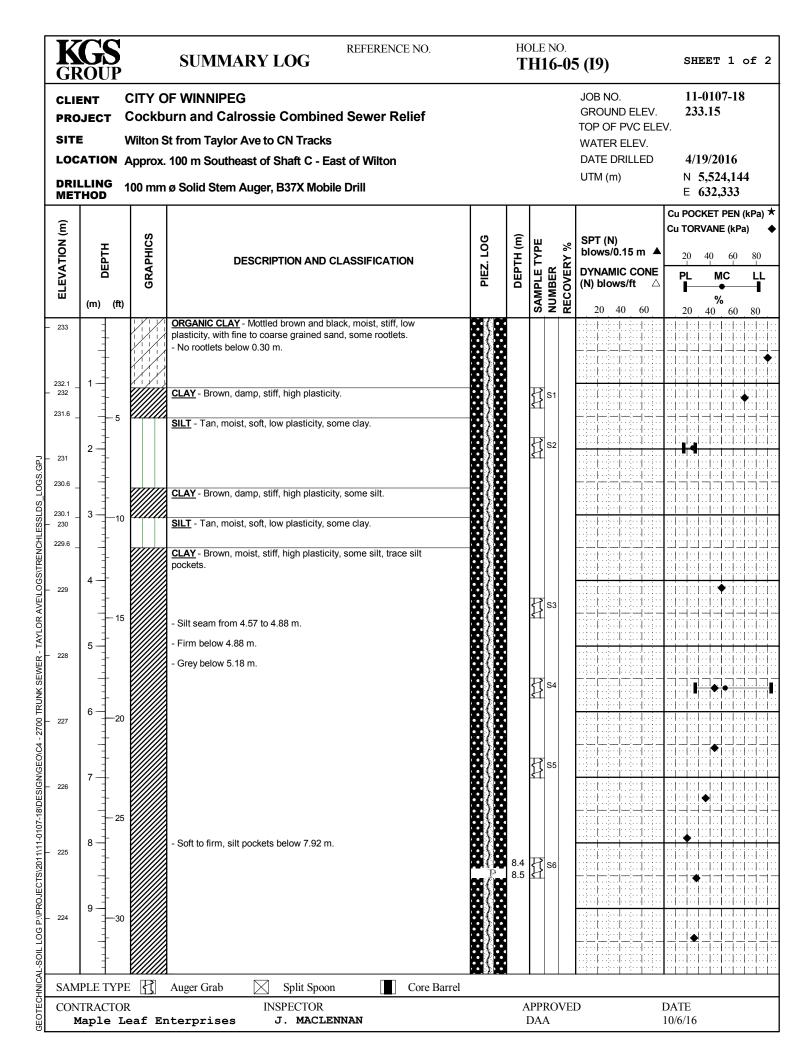


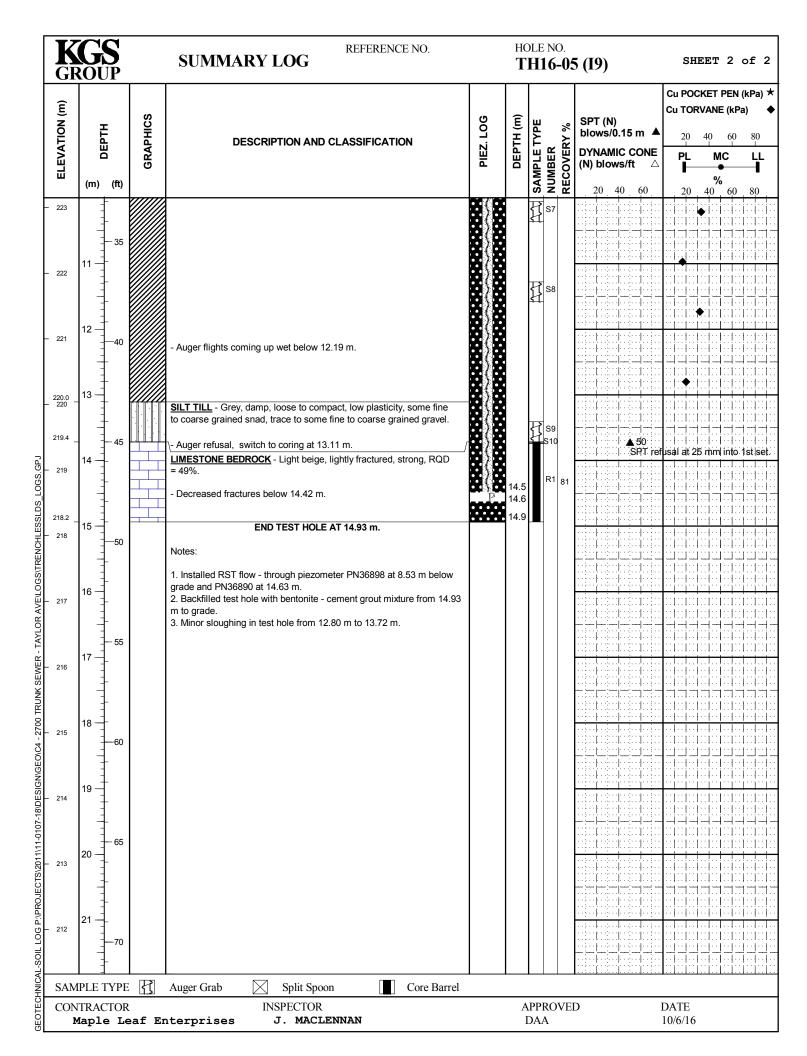


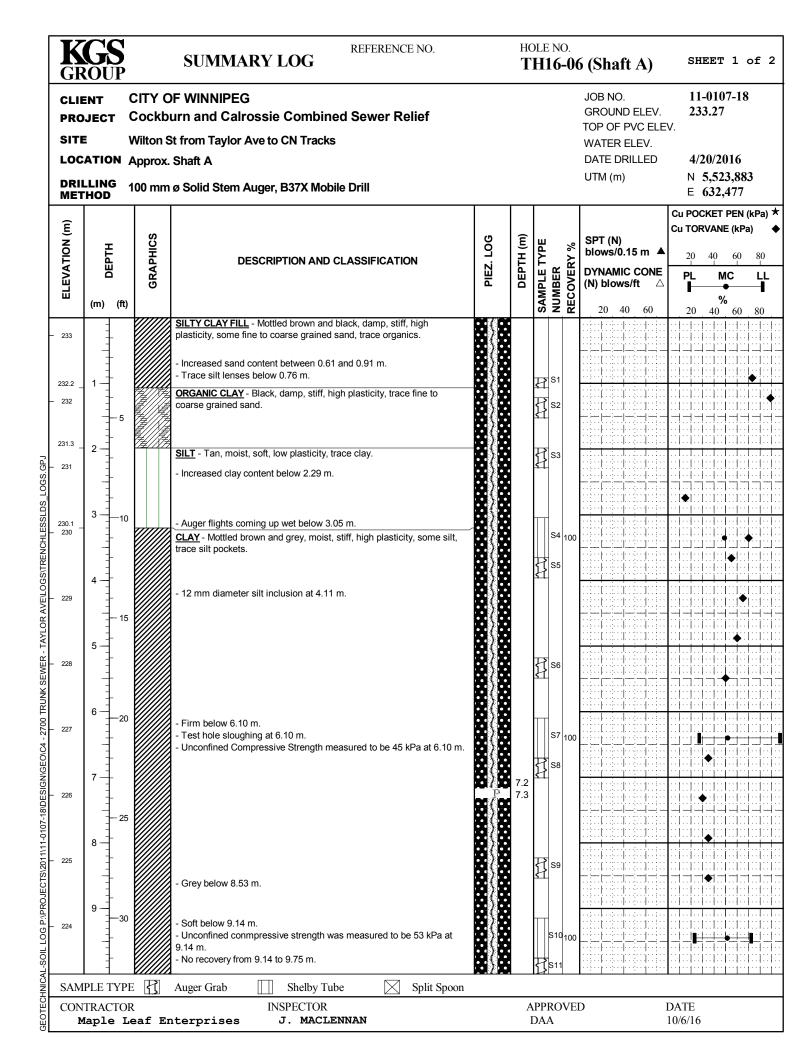


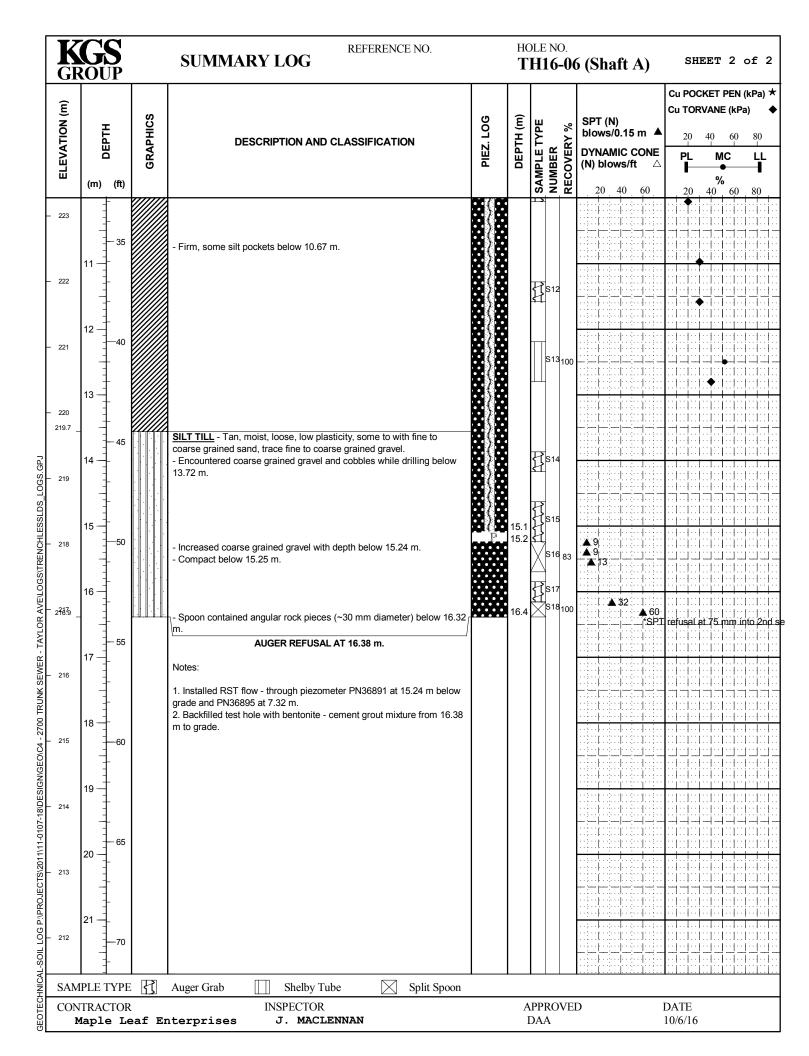


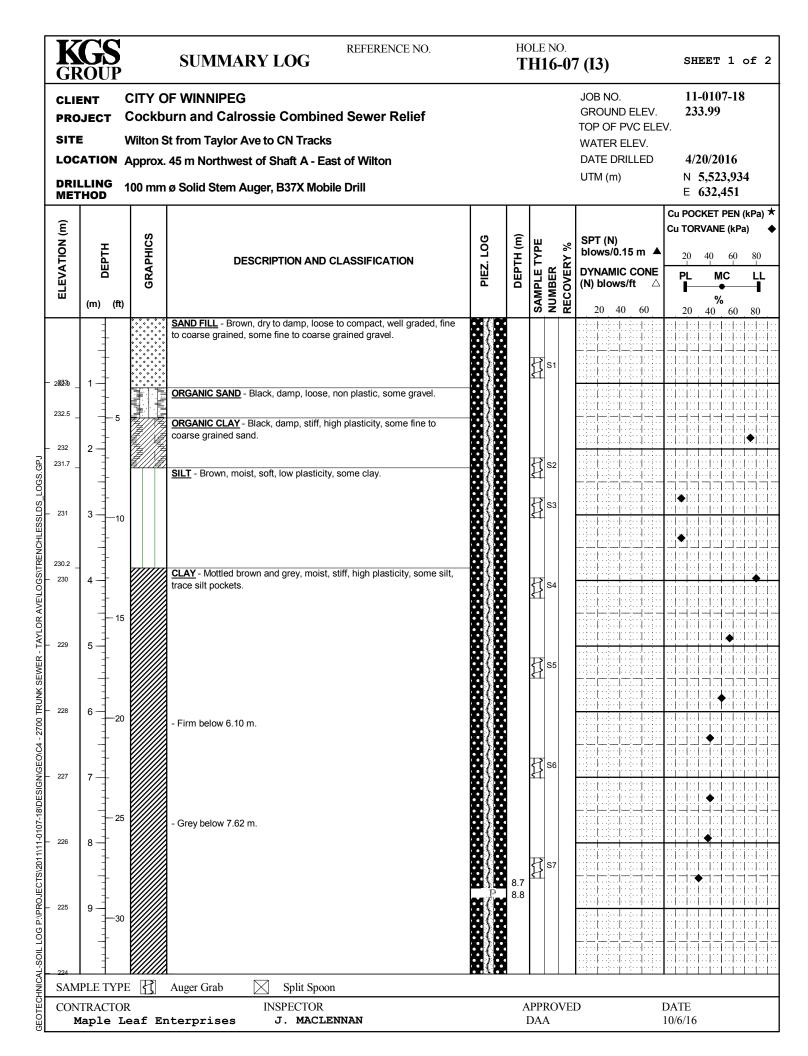


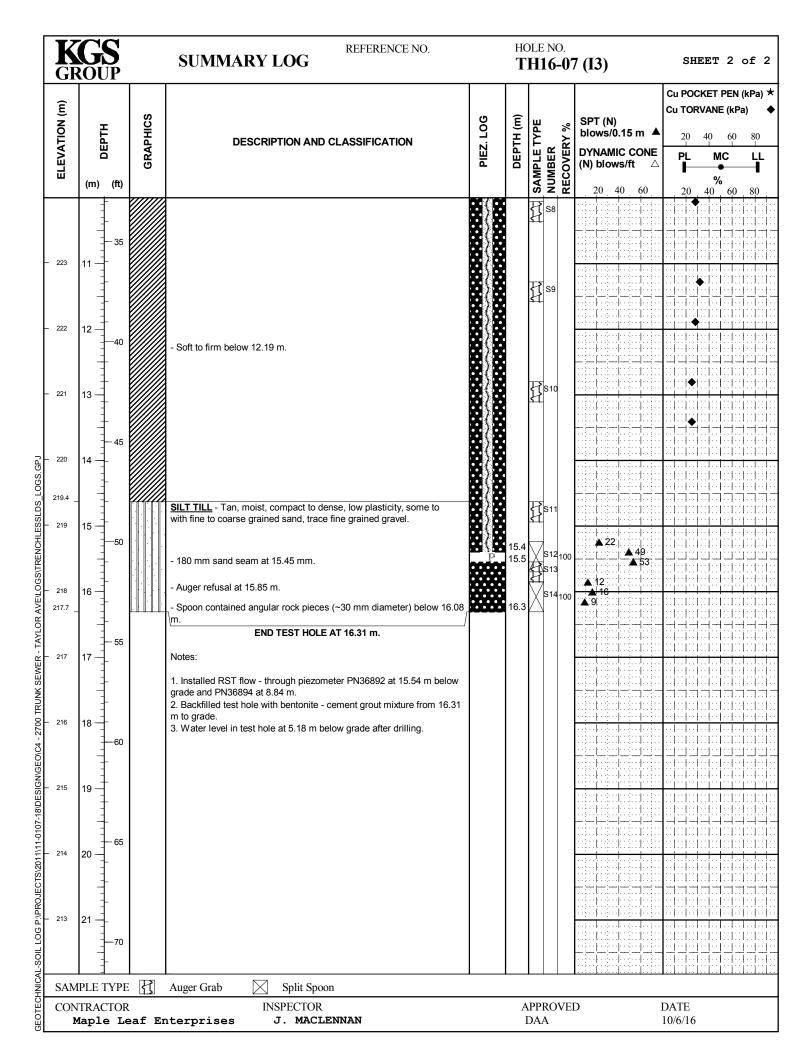


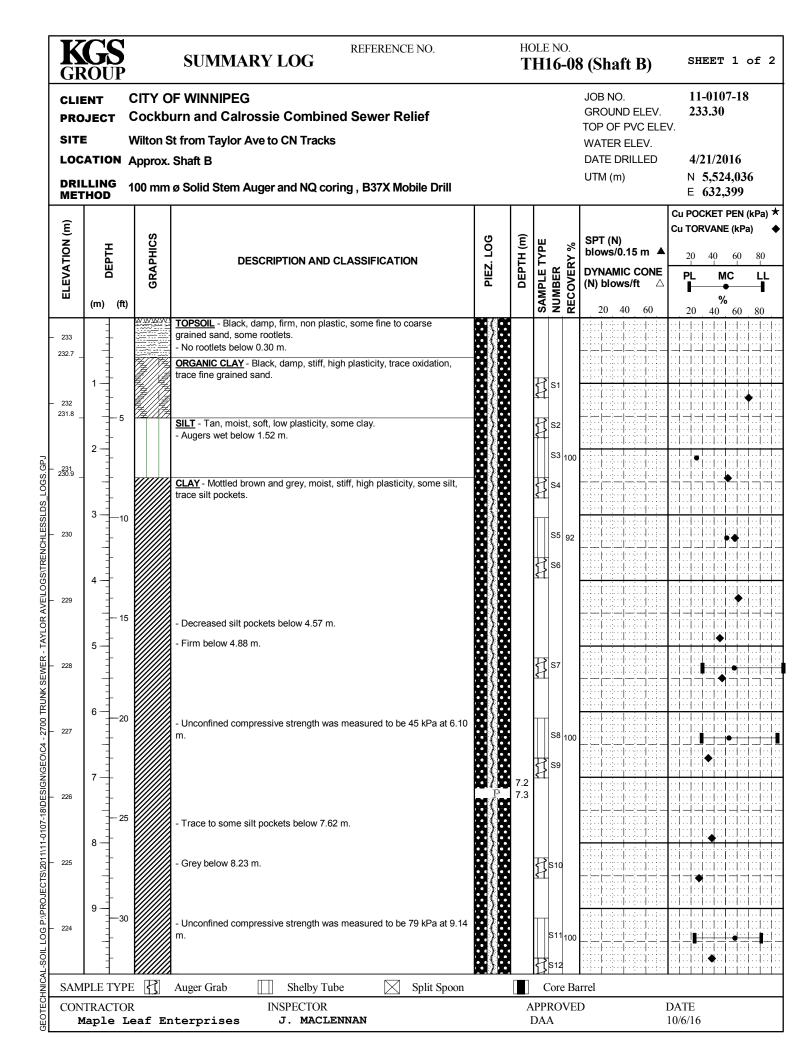


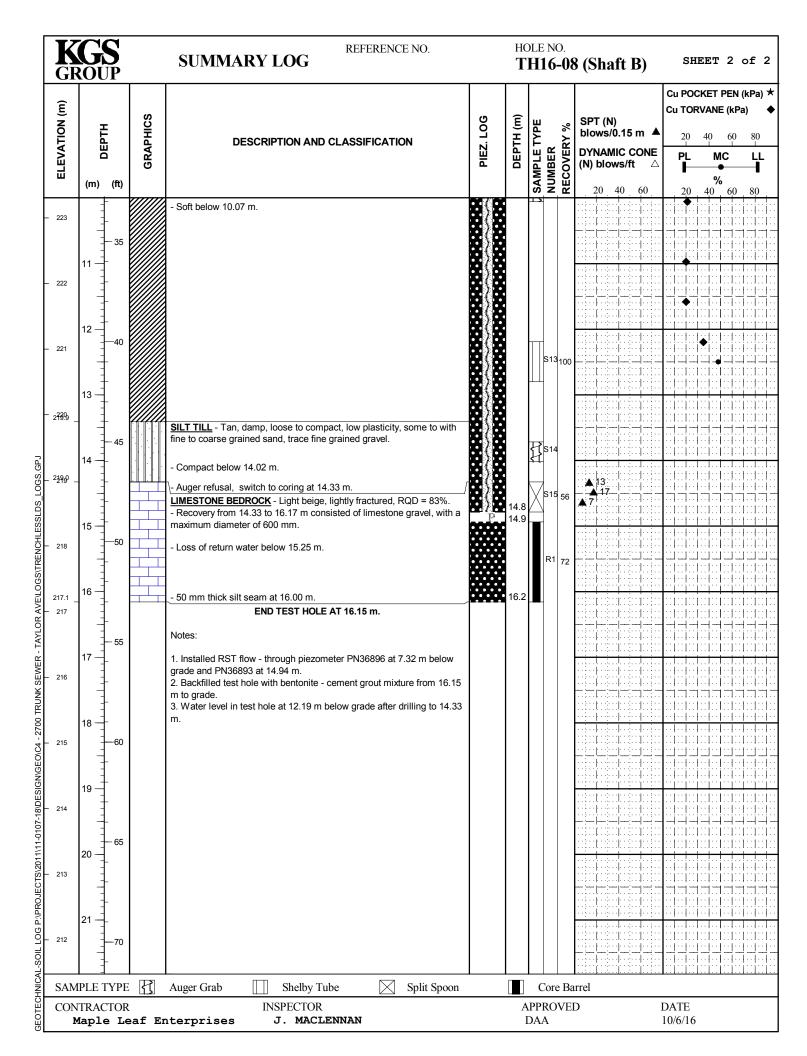


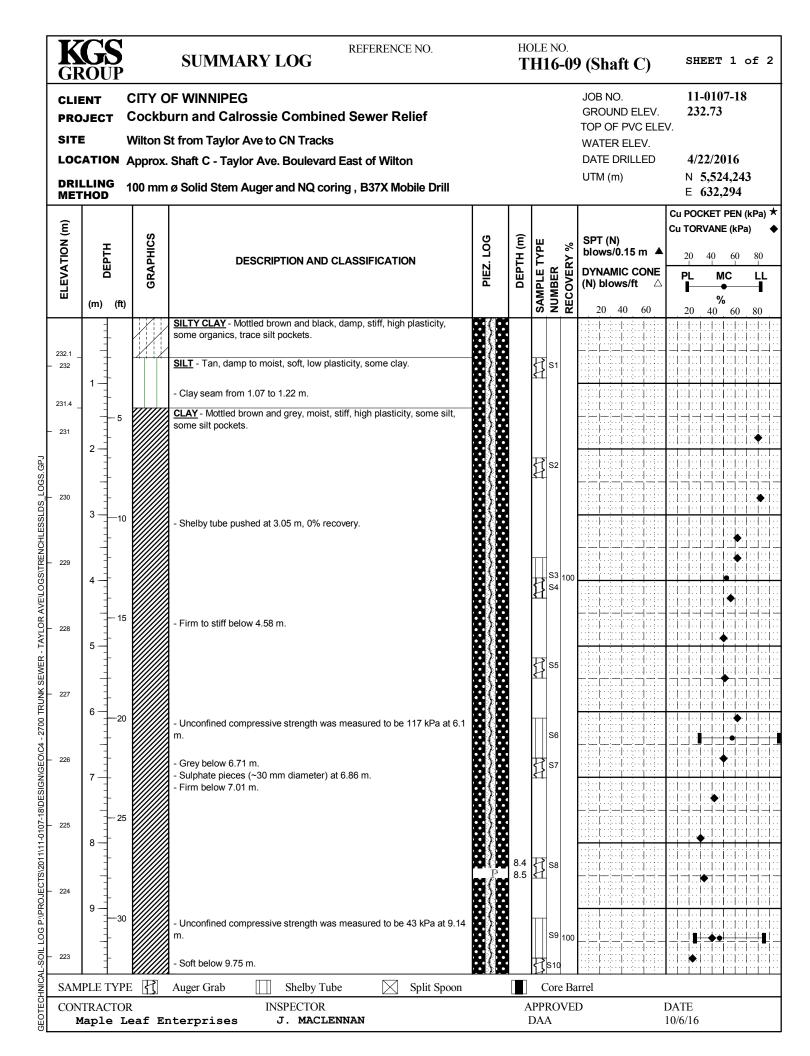


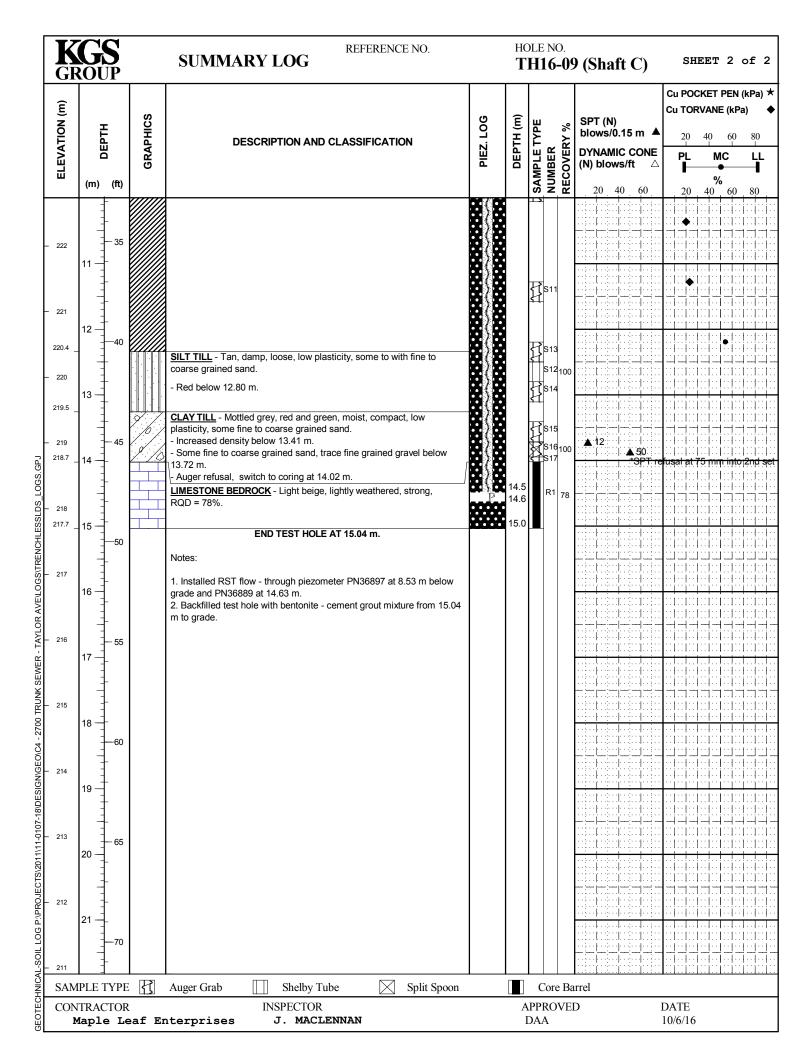




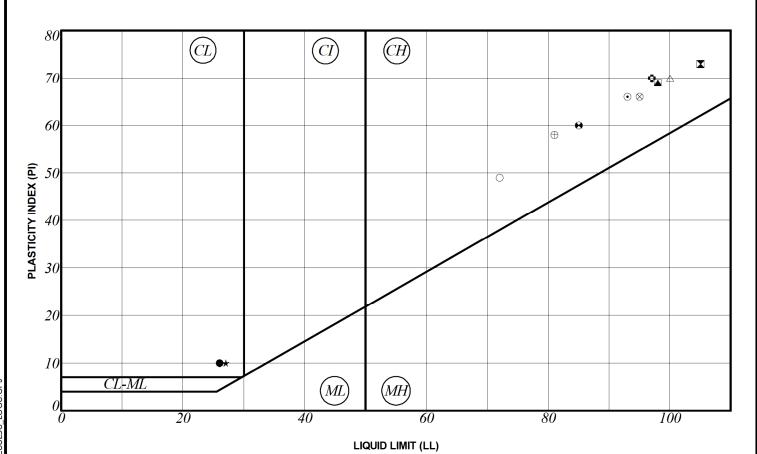












SYMBOL	HOLE	DEPTH (m)	SAMPLE#	LL	PL	PI	% SAND	% SILT	% CLAY	% MC	CLASSIFICATION
•	TH16-02 (I4/5)	2.9	S3	26	16	10				22.9	CL
	TH16-02 (I4/5)	5.6	S5	105	32	73				56.3	CH
<b>A</b>	TH16-03 (I7)	5.3	S5	98	29	69				53.4	CH
*	TH16-05 (I9)	2.0	S2	27	17	10				25.0	CL
•	TH16-05 (I9)	5.6	S4	93	27	66				53.1	CH
•	TH16-06 (Shaft A	A) 6.1	S7	97	27	70	0.5	19.4	80.1	51.8	CH
0	TH16-06 (Shaft A	A) 9.1	S10	72	23	49				51.5	CH
$\triangle$	TH16-08 (Shaft E	3) 5.3	S7	100	30	70				57.5	CH
$\otimes$	TH16-08 (Shaft E	3) 6.1	S8	95	29	66	0.4	18.2	81.4	52.9	CH
$\oplus$	TH16-08 (Shaft E	3) 9.1	S11	81	23	58				58.1	CH
	TH16-09 (Shaft 0	C) 6.1	S6	98	29	69	0.9	18.2	80.9	57.4	CH
0	TH16-09 (Shaft 0	C) 9.1	S9	85	25	60				46.5	CH

Notes:

ML - Low Plasticity Silt ML - Low Plasticity Silt
MH - High Plasticity Silt
CL-ML - Silty Clay
CL - Low Plasticity Clay
Cl - Intermediate Plasticity Clay
CH - High Plasticity Clay
LL - Liquid Limit

PL - Plastic Limit PI - Plasticity Index MC - Moisture Content

NP - Non-Plastic



## **CITY OF WINNIPEG**

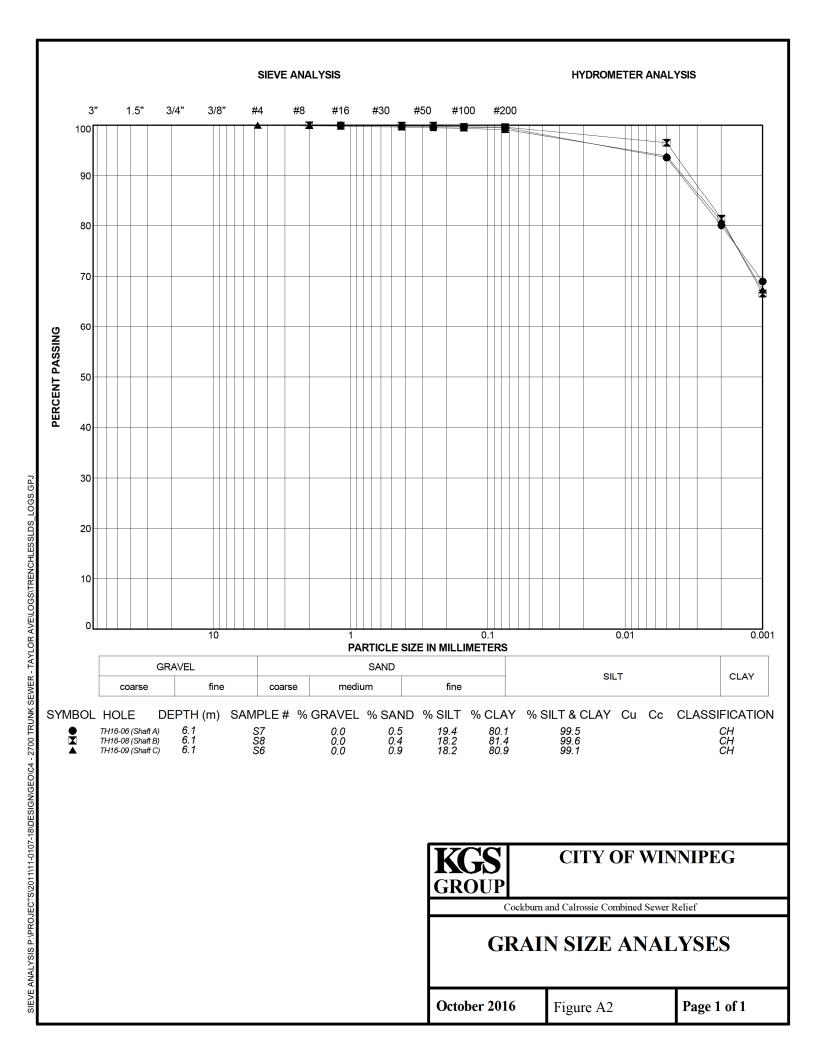
Cockburn and Calrossie Combined Sewer Relief

## **A-LINE PLOT**

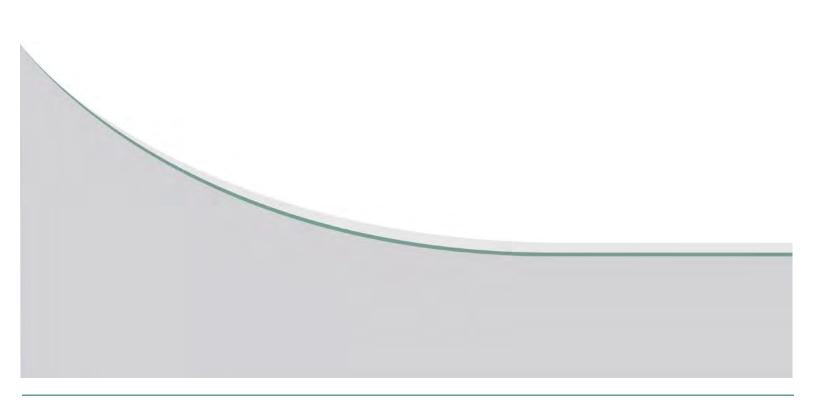
October 2016

Figure A1

Page 1 of 1



# APPENDIX B 2017 TEST HOLE LOGS





## KGS GROUP

## SOIL DESCRIPTION CRITERIA

## PRINCIPAL AND MINOR SOIL COMPONENTS

And 35-50% With 20-35% Some 10-20% Trace 0-10%

Occasional Trace of very local concentration

## FIELD MOISTURE CONTENT

Dry No moisture visible or to touch when fresh exposure is examined

Damp Slightly wet to touch Moist Fresh exposure wet to touch

Wet A film of water is readily visible around particles of granular soils, cohesive soils can readily be smeared or remolded; water can be squeezed

out

Saturated Water can easily be squeezed out

Free Water Water completely separated from the soil particles

#### DEPOSITIONAL STRUCTURE

Massive Structureless soil

Stratified (Layered) Different soils or visible variations in soil constituents arranged in layers, generally but not necessarily parallel to one another,

and not necessarily in horizontal position, at least 6 mm thick

Varved Glaciolacustrine deposits with annual pairs of fine and coarser laminae (thin laminae of alternately deposited inorganic silt and

clay)

Laminated Closely spaced, regularly alternating layers of differing soils and/or colours, or shades of similar gradation, relatively consistent in

thickness and consisting of sand, silt, or clay

Lens Inclusions of a different soil within surrounding soils, which thins out horizontally and may not be continuous over any

significant distance

Pocket A different soil type of very limited thickness or lateral extent (a small lens)

Inclusions Small pockets

Nuggety A different soil type in the form of small lumps Parting Paper thin separation of one type by another

## POST DEPOSITIONAL STRUCTURE

Fissured A soil breaks along definite, pre-existing planes or fracture with little resistance to fracturing

Slickensided Polished or glossy, sometimes striated surfaces resulting from movement of a material block relative to the adjacent blocks
Blocky/Friable/Platy Cohesive soil that can be broken down into angular larger fragments (blocky), small fragments (friable), or thin plate-like

fragments (platy) which resist further breakdown

Cemented Soil particles or fragments held together by cemented materials, often chemical precipitants, or deposits within overall soil mass

## GRAIN SIZE DISTRIBUTION IN COARSE GRAINED SOIL

 $\begin{array}{lll} \mbox{Boulders} & >& 200 \mbox{ mm } \mbox{\o} \\ \mbox{Cobbles} & 75-200 \mbox{ mm } \mbox{\o} \\ \mbox{Coarse Grained Gravel} & 19-75 \mbox{ mm } \mbox{\o} \\ \mbox{Fine Grained Sand} & 4.75-19 \mbox{ mm } \mbox{\o} \\ \mbox{Coarse Grained Sand} & 2-4.75 \mbox{ mm } \mbox{\o} \\ \mbox{Medium Grained Sand} & 0.425-2 \mbox{ mm } \mbox{\o} \\ \mbox{Fine Grained Sand} & 0.075-0.425 \mbox{ mm } \mbox{\o} \\ \mbox{\o} \end{array}$ 

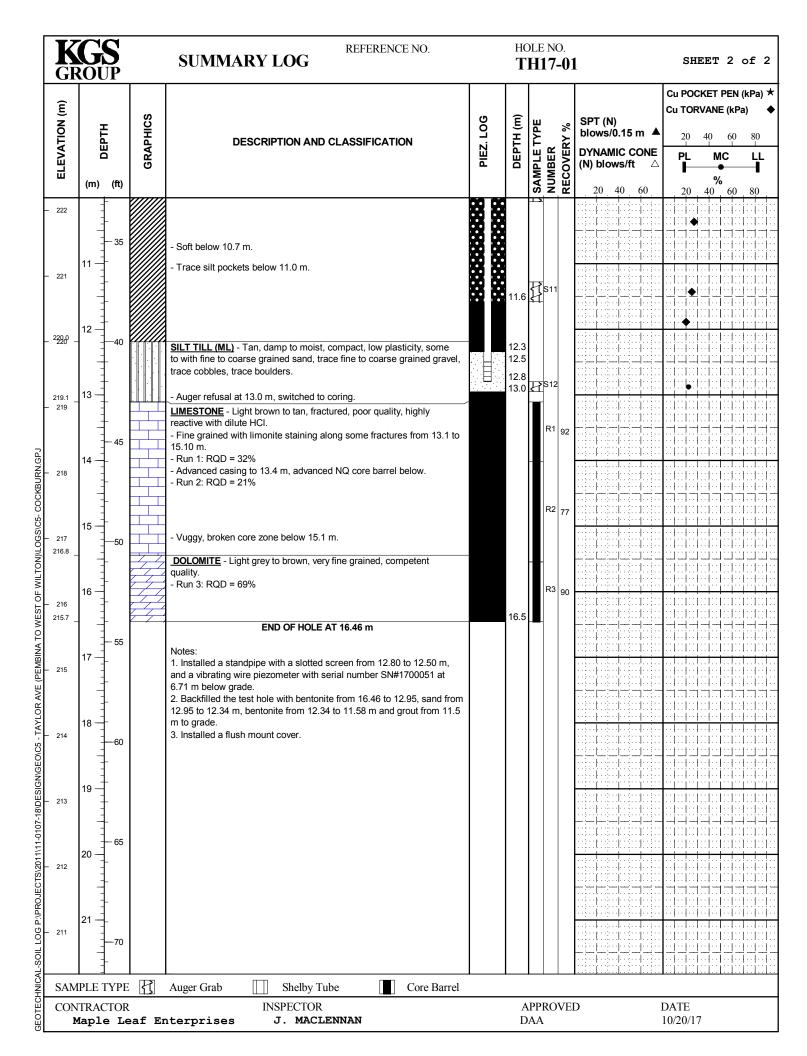
## DENSITY OF GRANULAR SOIL

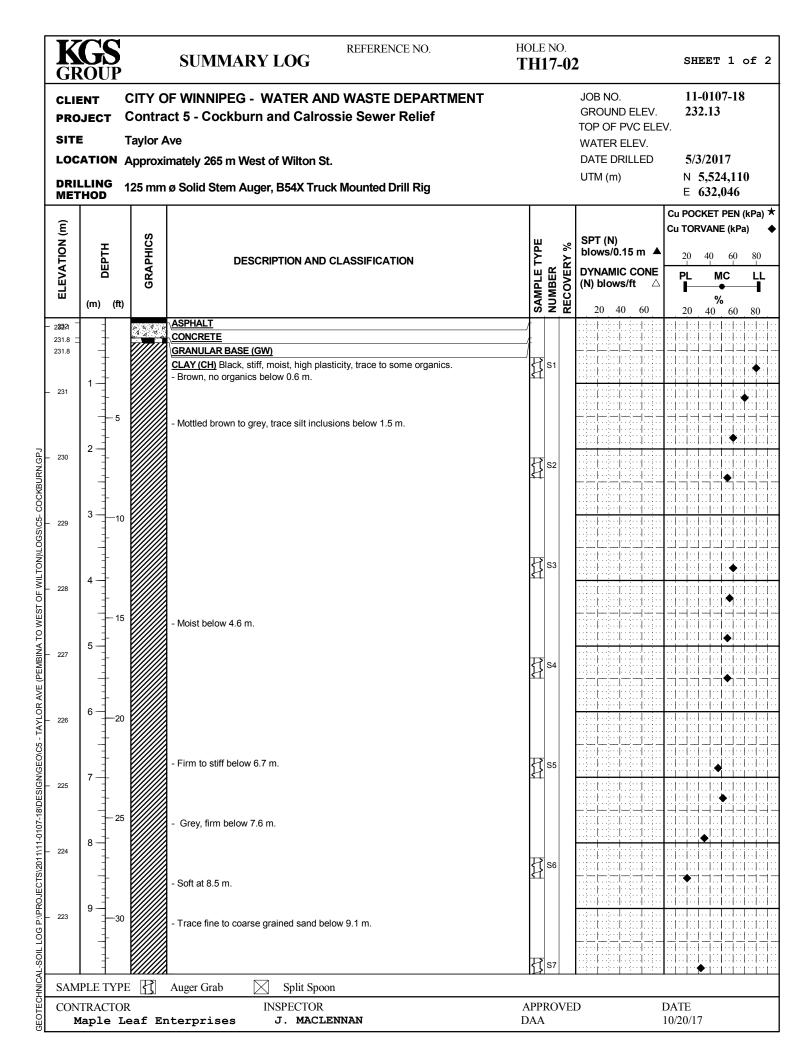
Description	Standard Penetration Test	Relative Density
Very Loose	0-4 Blows Per $0.3$ m	<15%
Loose	4 – 10 Blows Per 0.3 m	15 - 35%
Compact	10 - 30 Blows Per 0.3 m	35 - 65%
Dense	30 - 50 Blows Per 0.3 m	65 - 85%
Very Dense	>50 Blows Per 0.3 m	>85%

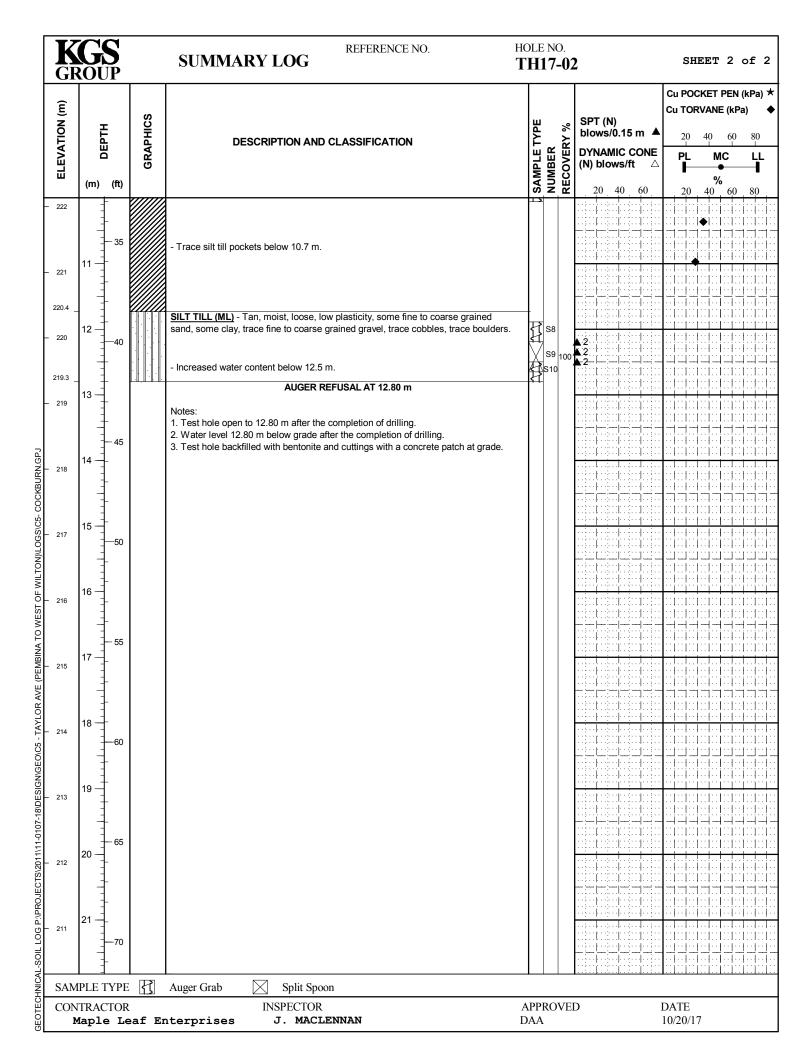
#### CONSISITENCY OF COHESIVE SOILS

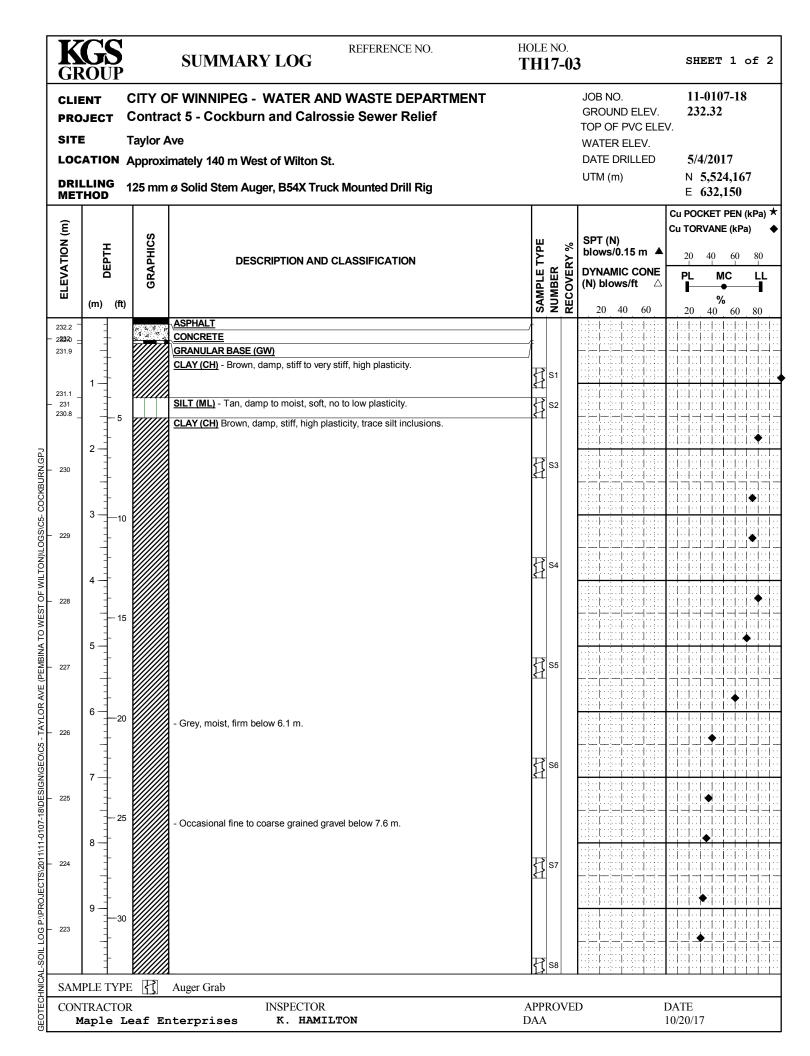
Description	Torvane	Standard Penetration Test
Very Soft	<12 kPa	<2
Soft	12 – 25 kPa	2 - 4
Firm	25 - 50  kPa	4 - 8
Stiff	50 - 100  kPa	8 - 15
Very Stiff	100 - 200  kPa	15 - 30
Hard	>200 kPa	>30

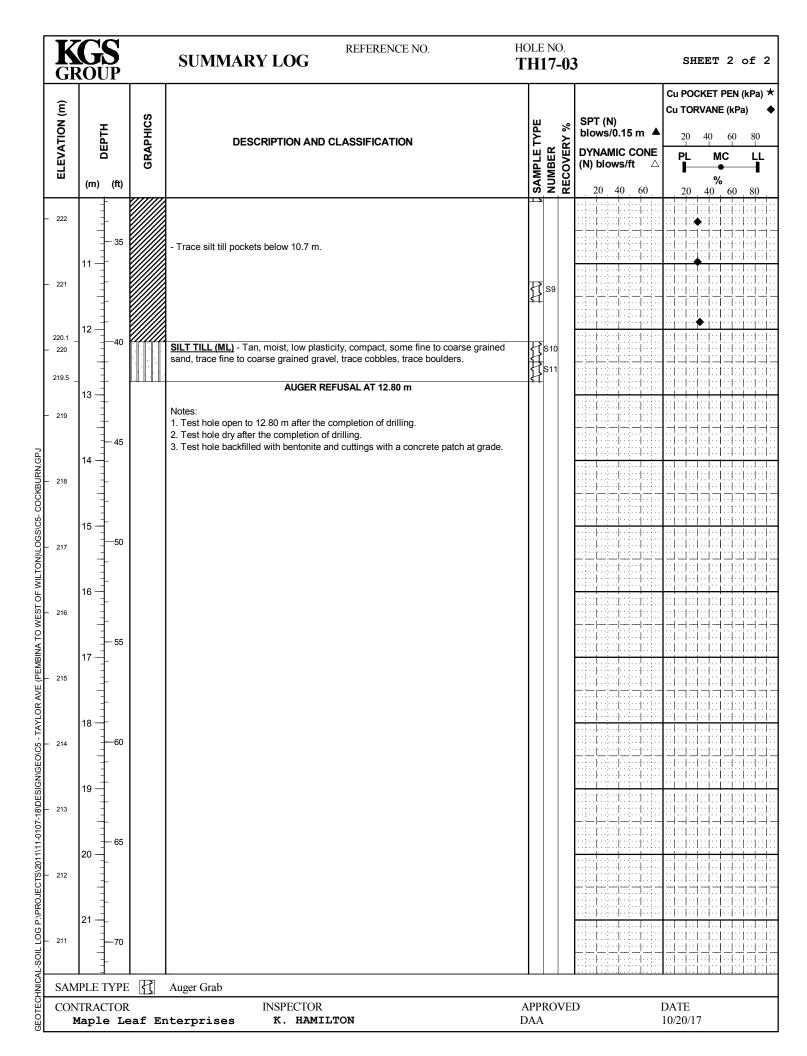
	K	G	S JP		SUMMARY LOG REFERENCE NO.			DLE N		1	SHEET 1 of 2		
Ī	CLIE	_	F WINNIPEG - WATER AND WASTE DEPAR ct 5 - Cockburn and Calrossie Sewer Relief	TMENT			JOB NO. GROUND ELEV. TOP OF PVC ELE						
	LOC DRII MET	ATIC	ON A		ove mately 320 m West of Wilton St. ø Solid Stem Auger, and NQ coring, B54X Truck Mou	unted Drill Riç	3			WATER ELEV. DATE DRILLED UTM (m)	5/3/2017 N 5,524,081 E 631,992		
	ELEVATION (m)			GRAPHICS	DESCRIPTION AND CLASSIFICATION	PIEZ. LOG	DEPTH (m)	SAMPLE TYPE	RECOVERY %	SPT (N) blows/0.15 m ▲ DYNAMIC CONE (N) blows/ft △ 20 40 60	Cu POCKET PEN (kPa) * Cu TORVANE (kPa)    20 40 60 80  PL MC LL  % 20 40 60 80		
F	23221 231.9 =	-	-		ASPHALT CONCRETE GRANULAR FILL (GW) CLAY (CH) - Brown trace black, damp, stiff, high plasticity, trace								
	231	1	_ _ 5		organics Brown, no organics below 0.6 m.  - Trace silt inclusions below 1.5 m.			₹ s					
CKBURN.GPJ	230	2 -	  -  -		- 75 mm clayey silt pocket at 2.2 m Mottled brown to grey below 2.3 m.	88888888888888888888888888888888888888		₹} s:	2				
WEST OF WILTON)/LOGS/C5- COCKBURN.GPJ	229	3 —	—10 -		- Moist below 3.1 m.	8888		₽°.	3				
	228	4	- - 15		- Unconfined Compressive Strength was measured to be 117 kPa			s:					
AVE (PEMBINA TO	227	5	- - -		4.6 m Grey below 4.9 m Firm below 5.5 m.			S s	<sup>4</sup> 100				
EO/C5 - TAYLOR	226	6	—20 -				6.7 6.9		6 <sub>79</sub>				
1107-18\DESIGN\G	225	7 —	_ 25					 					
GEOTECHNICAL-SOIL LOG P.\PROJECTS\2011/11-0107-18\DESIGN\GEO\C5 - TAYLOR AVE (PEMBINA TO	224	8	<u>-</u>		- Unconfined Compressive Strength measured to be 48 at 7.9 m.			S:					
-SOIL LOG P:\PRC	223	9	—30 - -		- Trace fine to coarse grained sand, trace silt pockets below 9.1 n			₹{s1	0				
CHNICAL	SAM				Auger Grab Shelby Tube Core Ba	18.80 18.80							
GEOTE	CON M				INSPECTOR terprises J. MACLENNAN			PPRO AA	OVE		DATE 10/20/17		

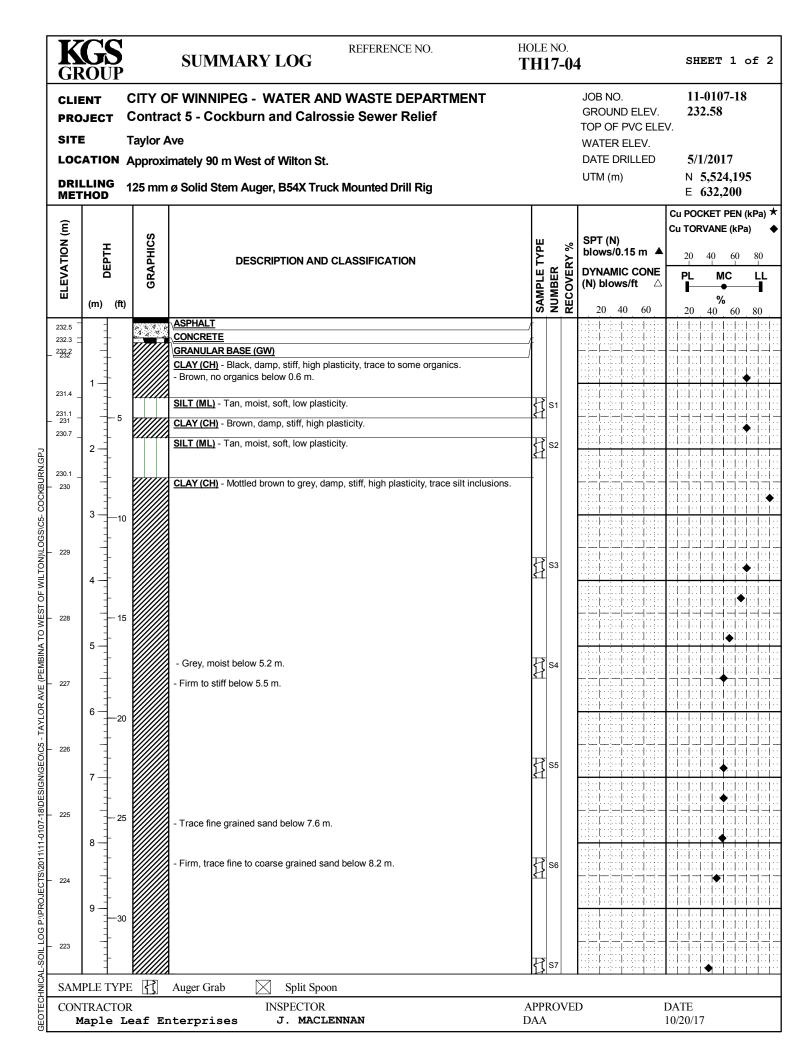


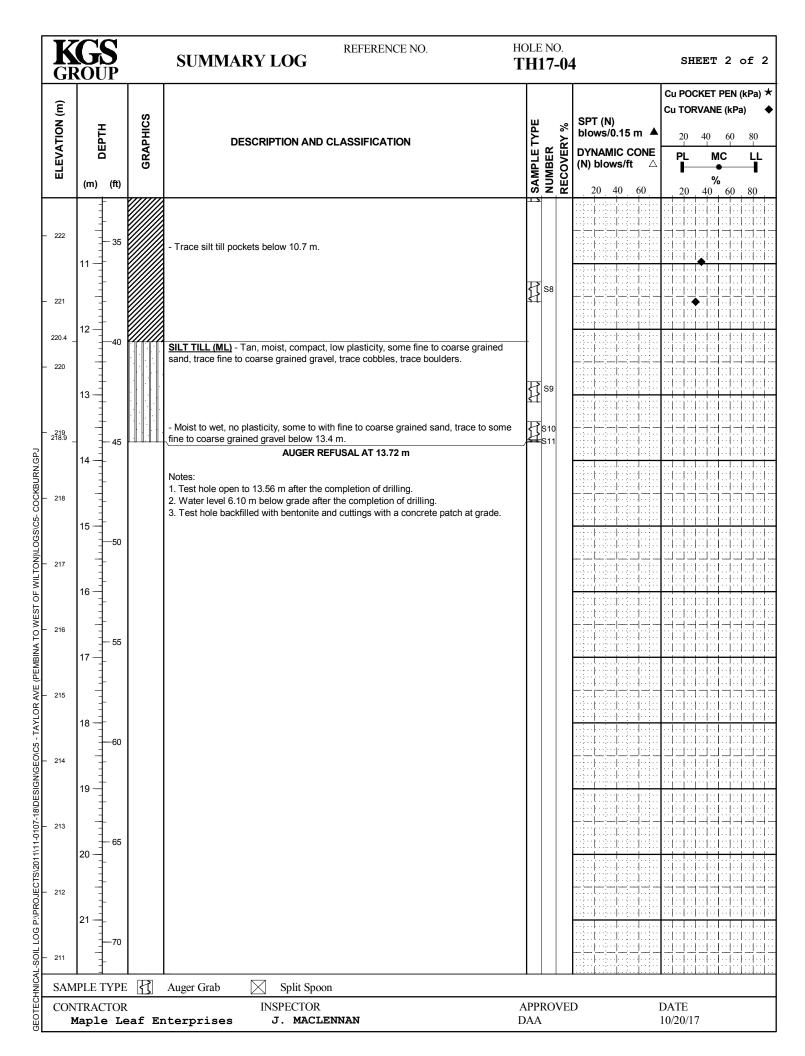


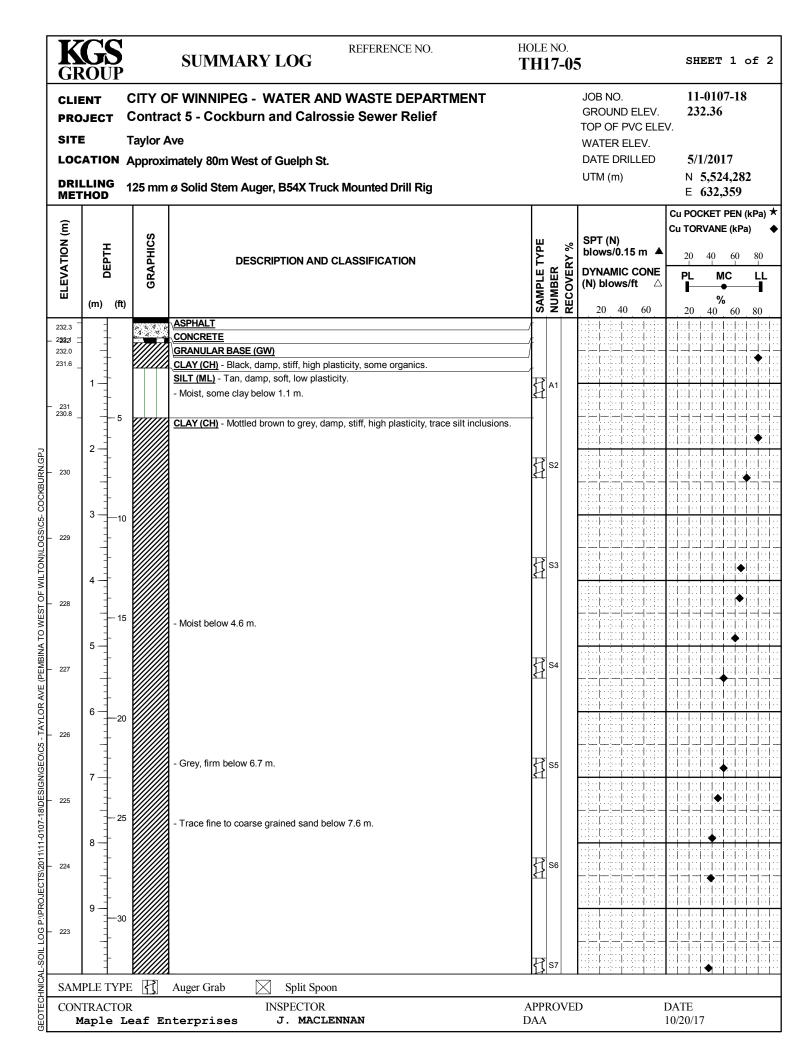


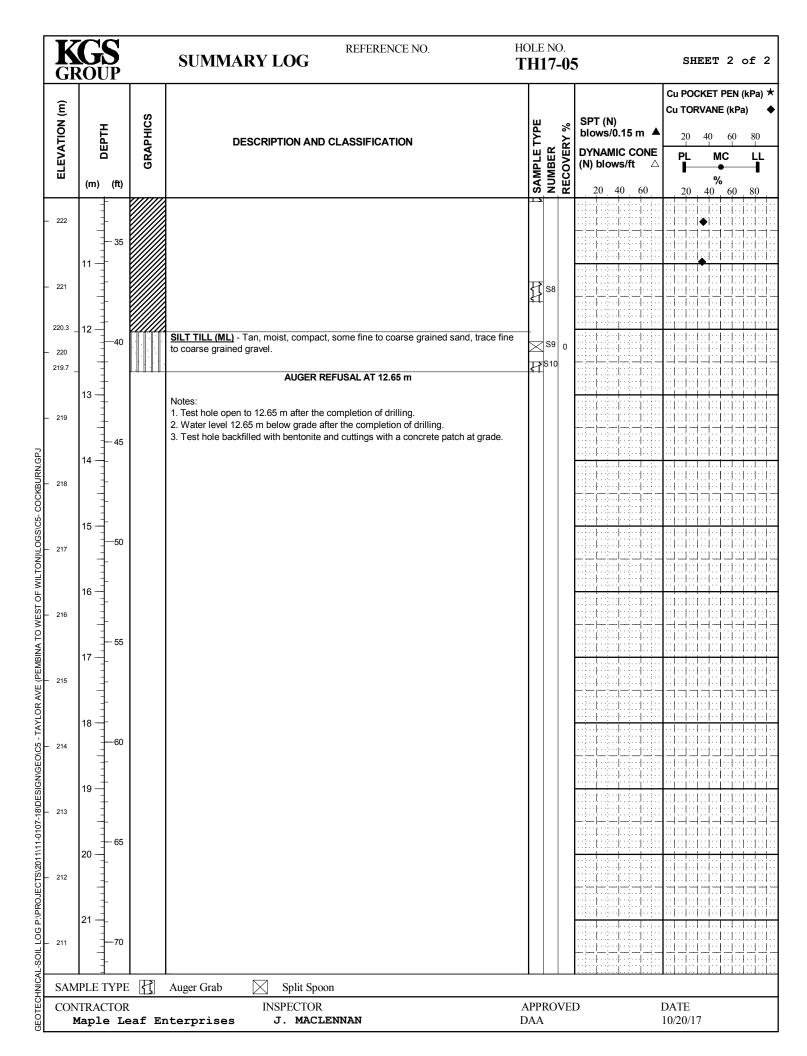




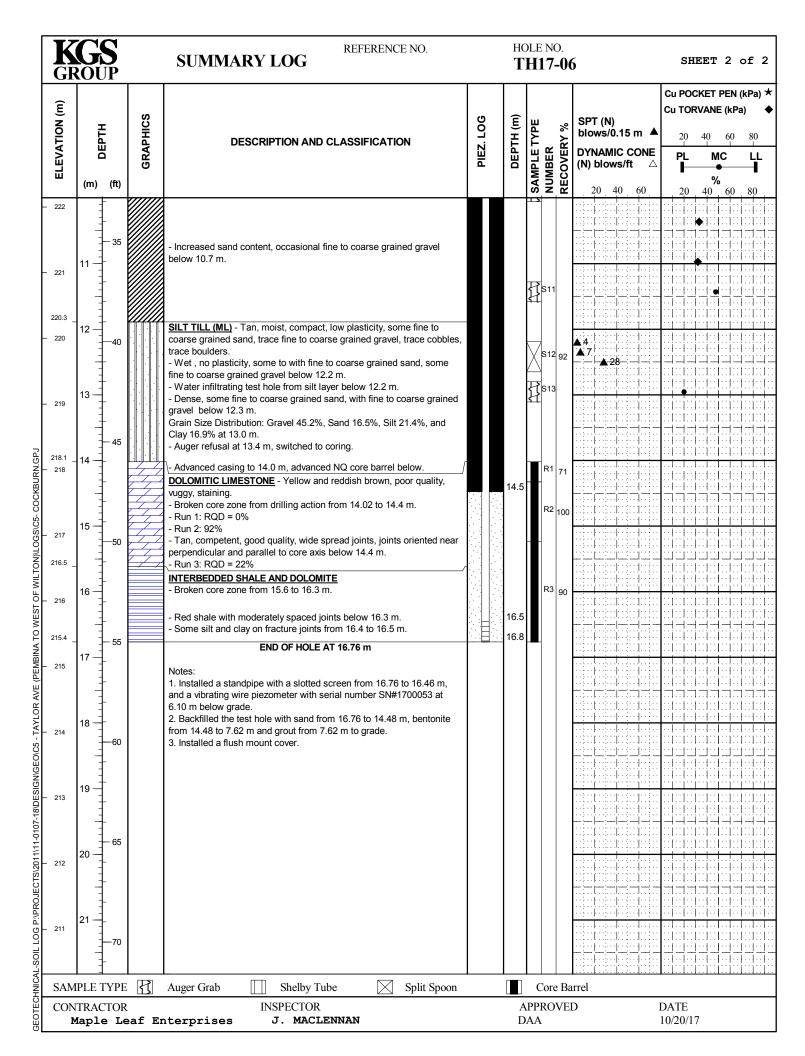


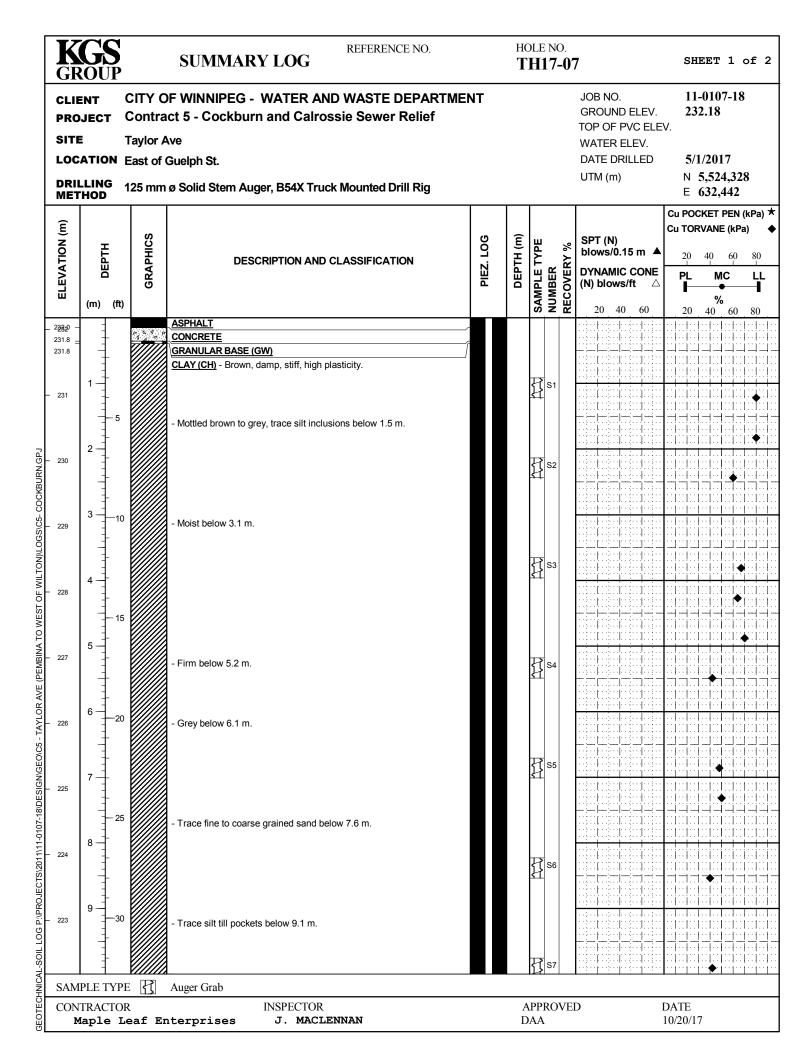


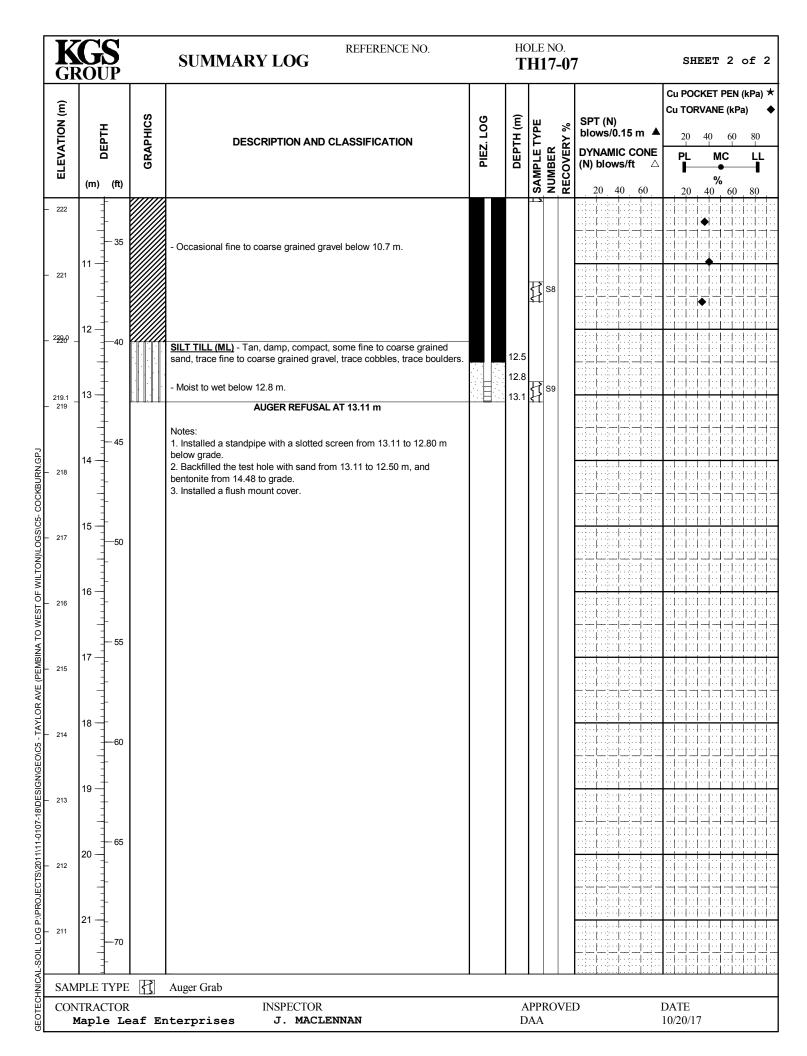


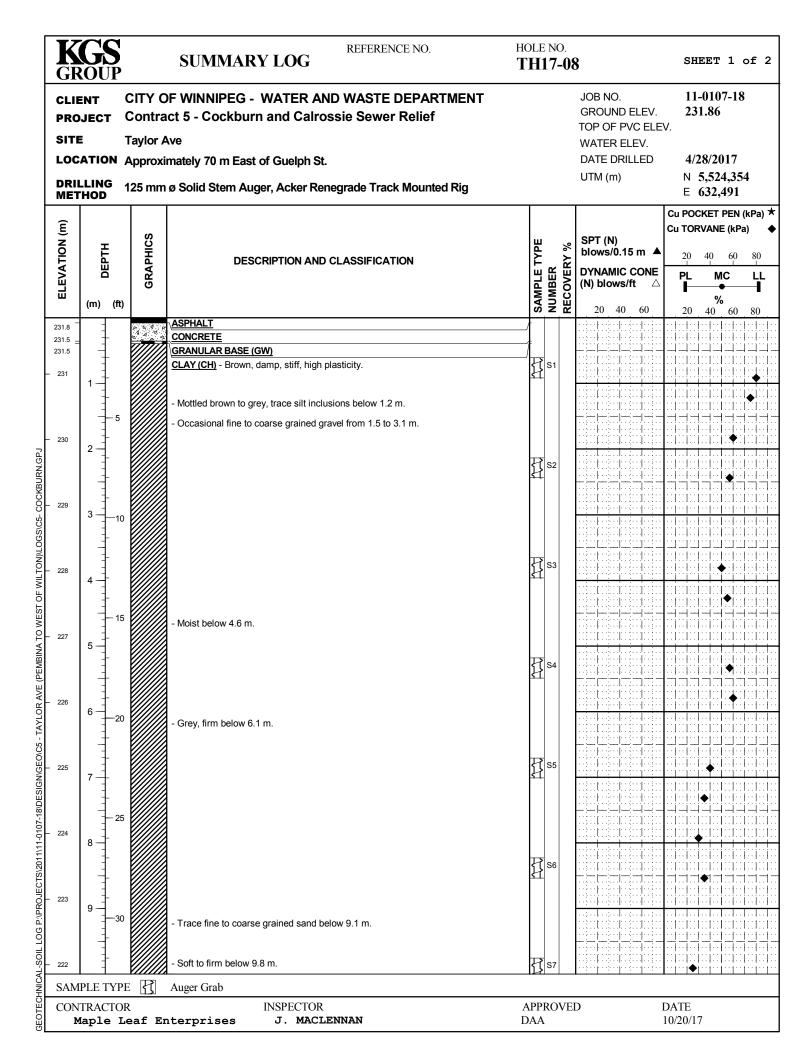


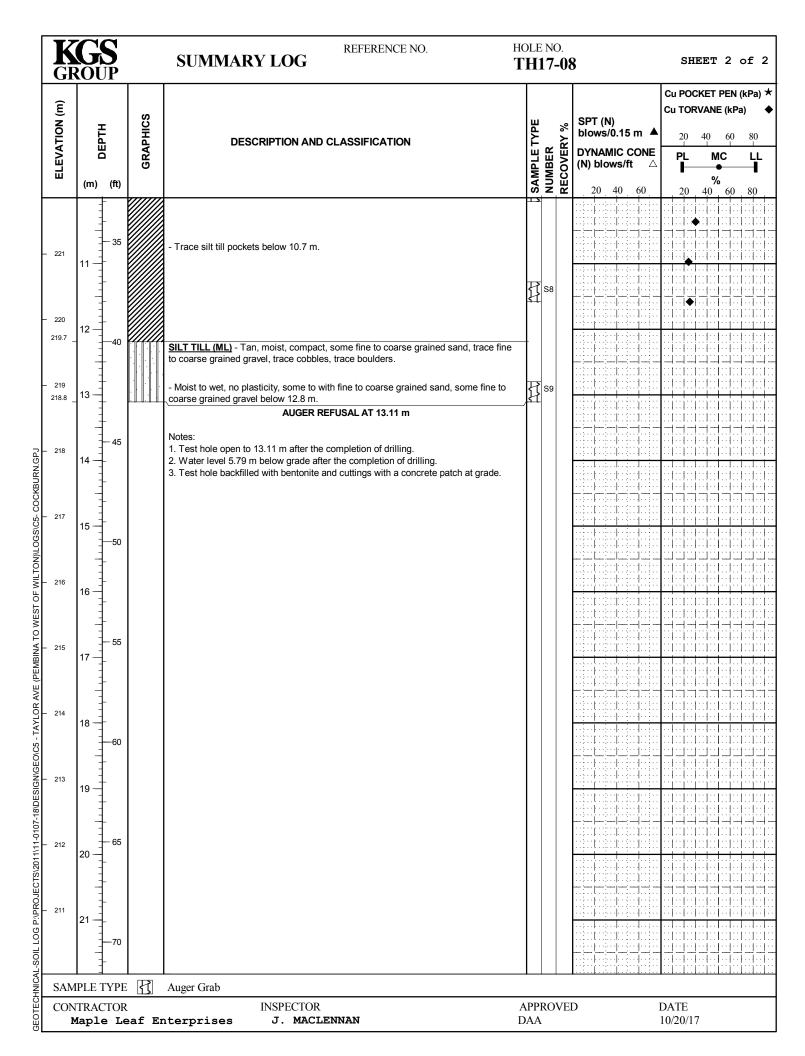
	K	G	S		SUMMARY LOG REFERENCE NO.			DLE NO. <b>H17-0</b>	6	SHEET 1 of 2
•	CLIE	NT	(	_	F WINNIPEG - WATER AND WASTE DEPARTME ct 5 - Cockburn and Calrossie Sewer Relief	NT			JOB NO. GROUND ELEV. TOP OF PVC ELE	11-0107-18 232.14
		ATIO	N V		ove Guelph St. ø Solid Stem Auger, and NQ coring, B54X Truck Mounted	l Drill Riç	9		WATER ELEV. DATE DRILLED UTM (m)	5/2/2017 N 5,524,316 E 632,420
•	ELEVATION (m)	(m)	i i (ft)	GRAPHICS	DESCRIPTION AND CLASSIFICATION	PIEZ. LOG	DEPTH (m)	SAMPLE TYPE NUMBER RECOVERY %	SPT (N) blows/0.15 m ▲ DYNAMIC CONE (N) blows/ft △ 20 40 60	Cu POCKET PEN (kPa) * Cu TORVANE (kPa)   20 40 60 80  PL MC LL  % 20 40 60 80
	- 2 <b>33</b> 21	=		0 4 9 0	ASPHALT	<b>22 23</b>				
	231.9		-		CONCRETE GRANULAR BASE (GW)					
	231.8		-		CLAY (CH) - Brown, damp, stiff, high plasticity.	笠 笠				
-	- 231	1	- - 5 -		- Mottled brown to grey, trace silt inclusions.			<b>∏</b> S1		
- COCKBURN.GPJ	- 230	2 —	-			83888888 83888888888888888888888888888		S2		
WEST OF WILTON)\LOGS\C5- COCKBURN GPJ	- 229 - 228	4-	—10 - - -		- Moist below 3.4 m.	333333333 3333333333333333333333333333		\$3 \$3		
	- 227	5 —	- 15 - -		- Unconfined Compressive Strength was measured to be 102 kPa at 4.9 m.			S4 96		<b>→ → → → → → → → → →</b>
C5 - TAYLOR AVE (F	- 226	6 —	- - 20 -		- Unconfined Compressive Strength was measured to be 71 kPa at 6.4	VW	6.1 6.2	S6 <sub>100</sub>		
7-18\DESIGN\GEO\	- 225	7	- - - - 25		m Grey below 6.7 m Firm below 7.3 m Shelly tribe pushed at 7.6 m had 0% recovery	888888888	7.6	S7		
CTS\2011\111-0107	- 224	8 —	-		- Shelby tube pushed at 7.6 m had 0% recovery.			S8 <sub>100</sub>		
GEOTECHNICAL-SOIL LOG PAPROJECTS/2011/11-0107-18/DES/GN/GEO/C5 - TAYLOR AVE (PEMBINA TO	- 223	9 —	30 		- Trace fine to coarse grained sand 9.1 m.			S9 S10		
ICAL	CARE	DI E T	VDF	[]]]	Augus Crah Challey Tuka Culti C				arrol	<u> </u>
GEOTECHN	SAM CON	TRAC	TOR		Auger Grab Shelby Tube Split Spoon INSPECTOR Aterprises J. MACLENNAN			Core B PPROVE AA	D I	DATE 10/20/17



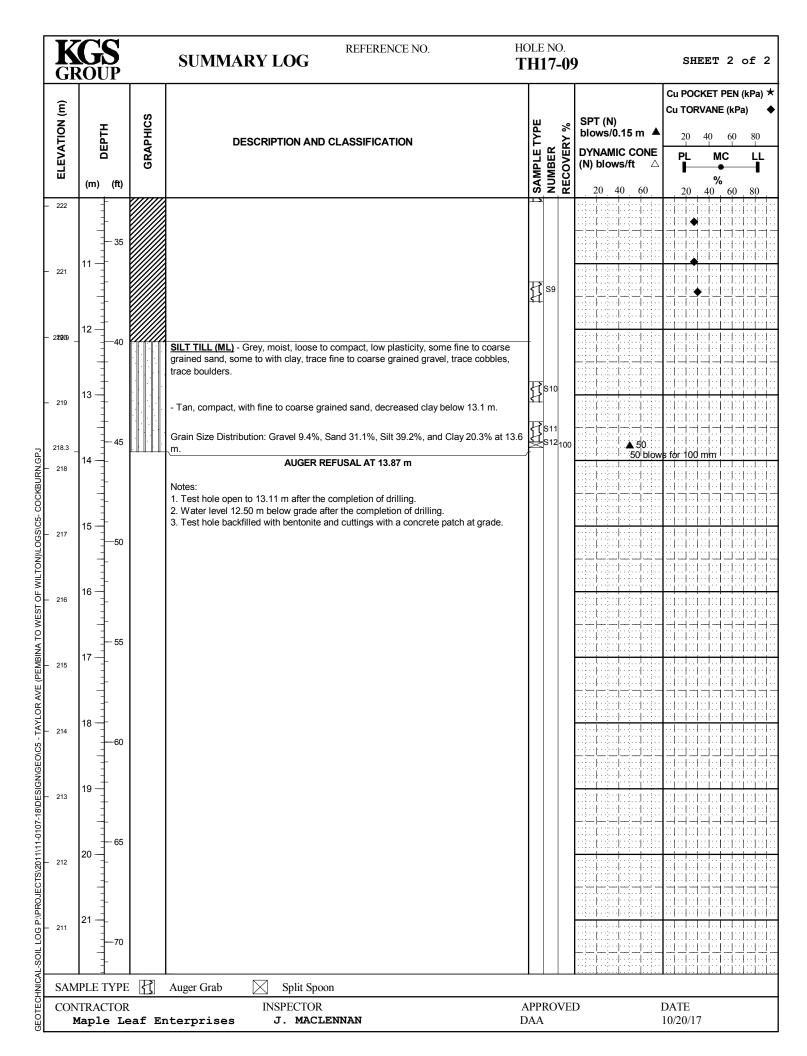


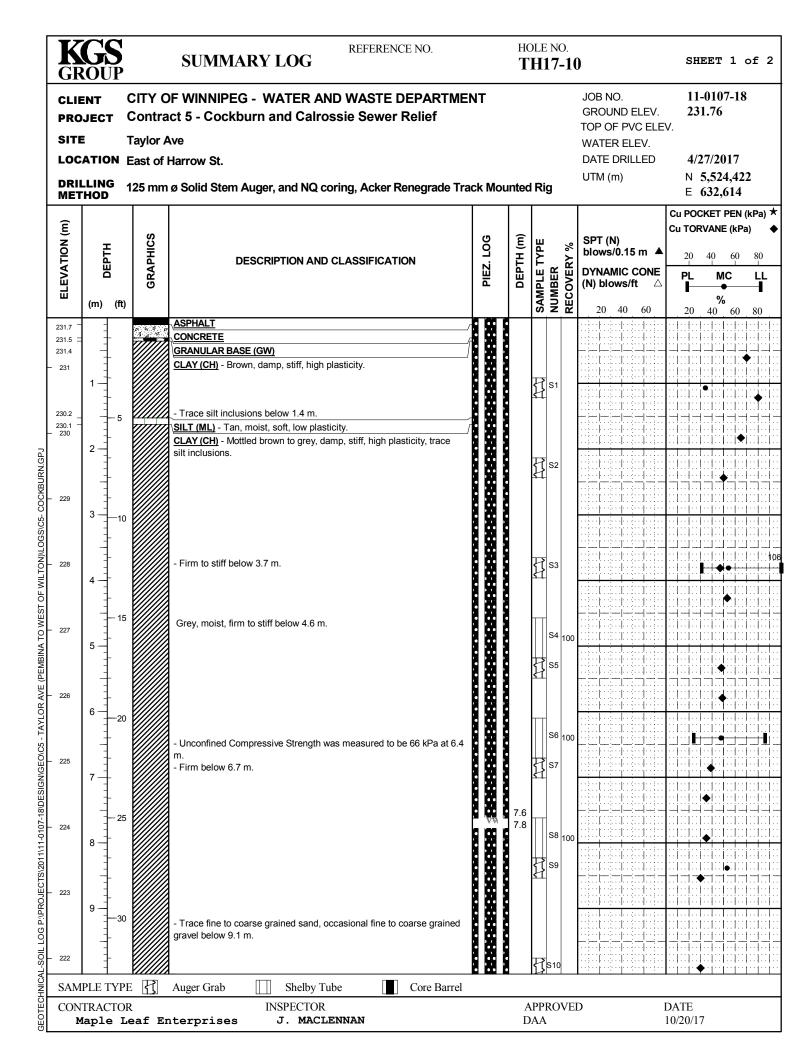


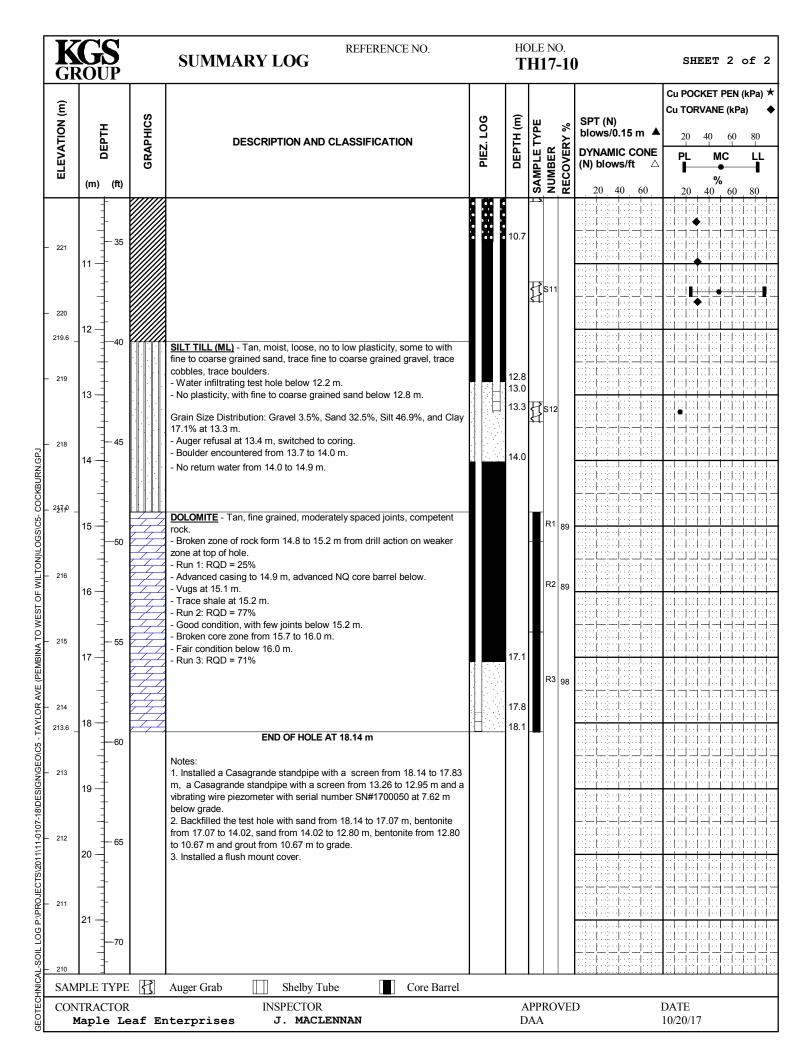


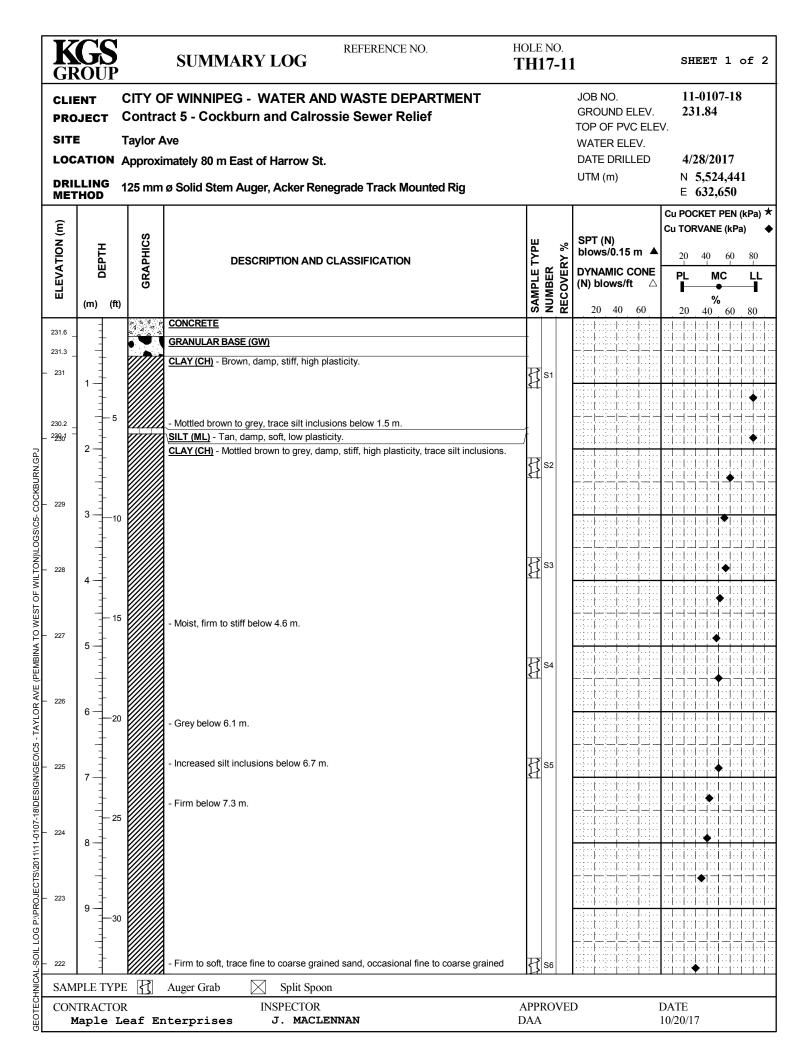


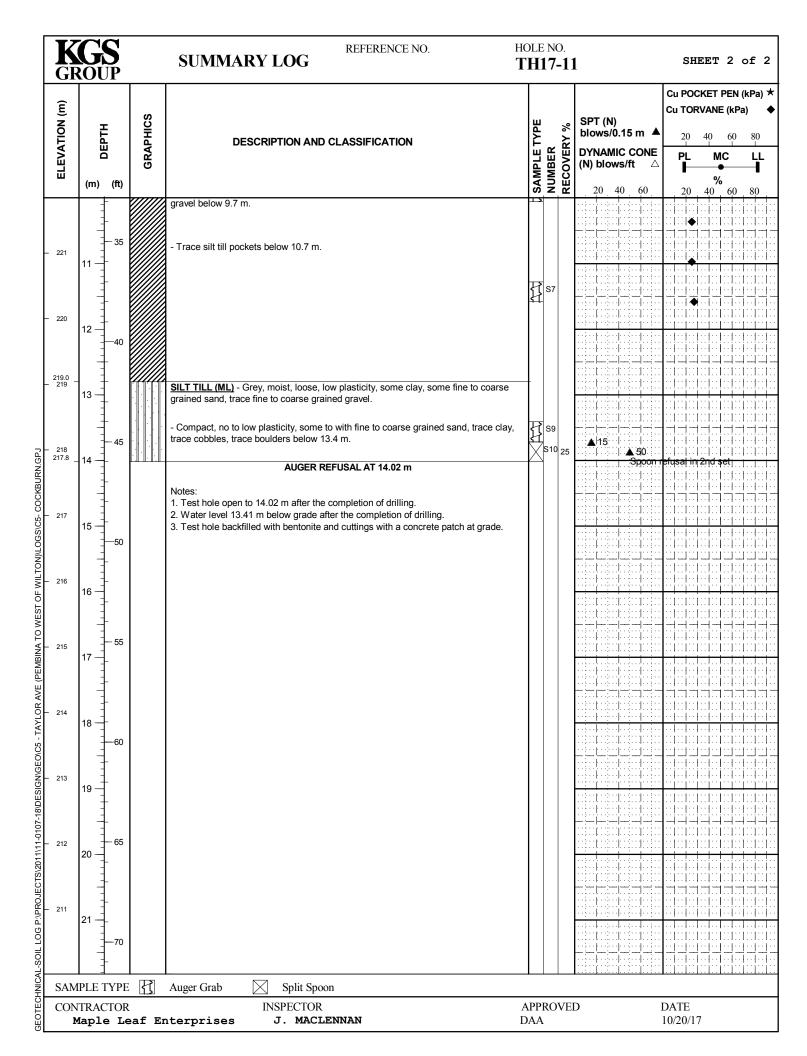
CLIE	OU ENT JECT	(		SUMMARY LOG  PF WINNIPEG - WATER AND WASTE DEPARTMENT act 5 - Cockburn and Calrossie Sewer Relief	HOLE TH	NO. 1 <b>7-0</b> 9	JOB NO	ND EI				ET 1 0107- .12		f 2
DRIL	ATIOI	N \		Ave Harrow St. ø Solid Stem Auger, B54X Truck Mounted Drill Rig			TOP OF WATER DATE D UTM (m	R ELE	V.	1	N 5	2017 ,524,, 32,53	380	)
ELEVATION (m)	DEPTH		GRAPHICS	DESCRIPTION AND CLASSIFICATION	AMPLE TYPE	NUMBER RECOVERY %	SPT (N) blows/0 DYNAM (N) blow	0.15 I IIC C	ONE	Cu F	POCK ORV	KET PE	EN (k kPa)	
	(m)	(ft)		∖asphalt	\ <u>\s_\</u>	Z Z	20	40	60	2	20		50	80
28220 Z	1		4 4 4	CONCRETE	_[								1	
231.7	1			GRANULAR BASE (GW)					1==		1111	111	17	44
				CLAY (CH) - Black, moist, high plasticity, stiff, some organics, trace fine to coarse		S1		4.30	J		1 I .   -	.11 H-H-	1 I . 1 1 -	[]  
231.1	1-			grained sand.	1		<u> </u>	1000	1	1	<del>                                     </del>	ځنن	<b>₽</b>	<del></del>
231	‡			SILT (ML) - Tan, damp, soft, low plasticity.	- 33	S2		ф. ;;;; ф. ;;;;	1		1	1	1[. 1[.	4.4
230.6	- 1	- 5	<i>,,,,,,,</i>	CLAY (CH) - Mottled brown to grey, damp, stiff, high plasticity, trace silt inclusions.	41			- :-	1		1-1-		1-1:	$\dashv$
	1			CEAT (CIT) - Mothed brown to grey, damp, shin, high plashorty, hace shit inclusions.				1	ļ		· ·   ·		· · · ·	
230	2-1				<b>}</b>	S3						•		
229	3 - 1	-10		- Moist below 3.1 m.		S4		1 3 1						
228	4-1	- 15		- Firm below 4.3 m.	\$1									
227	5			- Grey below 5.2 m.	<b>1</b>	S5					1	* 1	1	
226	6	-20				S6								
224	8 - 1	- 25		- Trace fine to coarse grained sand, trace silt pockets below 7.6 m.	<b>1</b>	S7								
223	9 - 1	-30			B	\$8								
SAMI	PLE T	YPI	E <b>[</b> ]	Auger Grab Split Spoon										
	TRAC:			INSPECTOR	APP	ROVE	D			DAT	E			



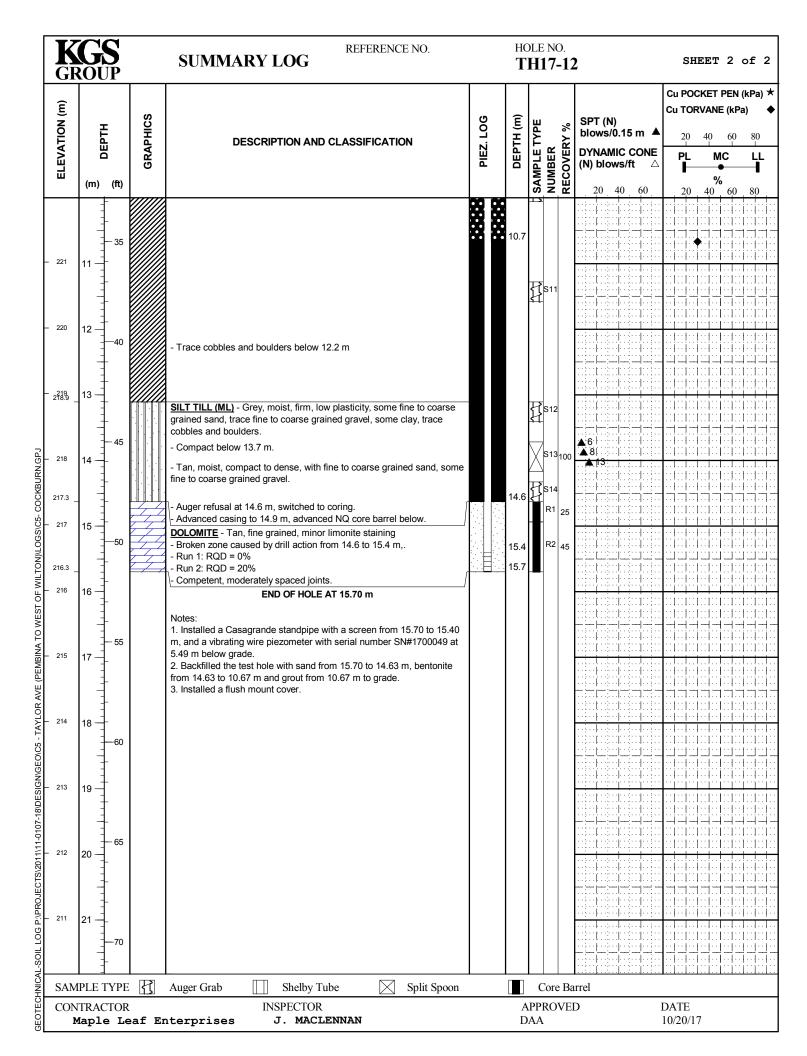




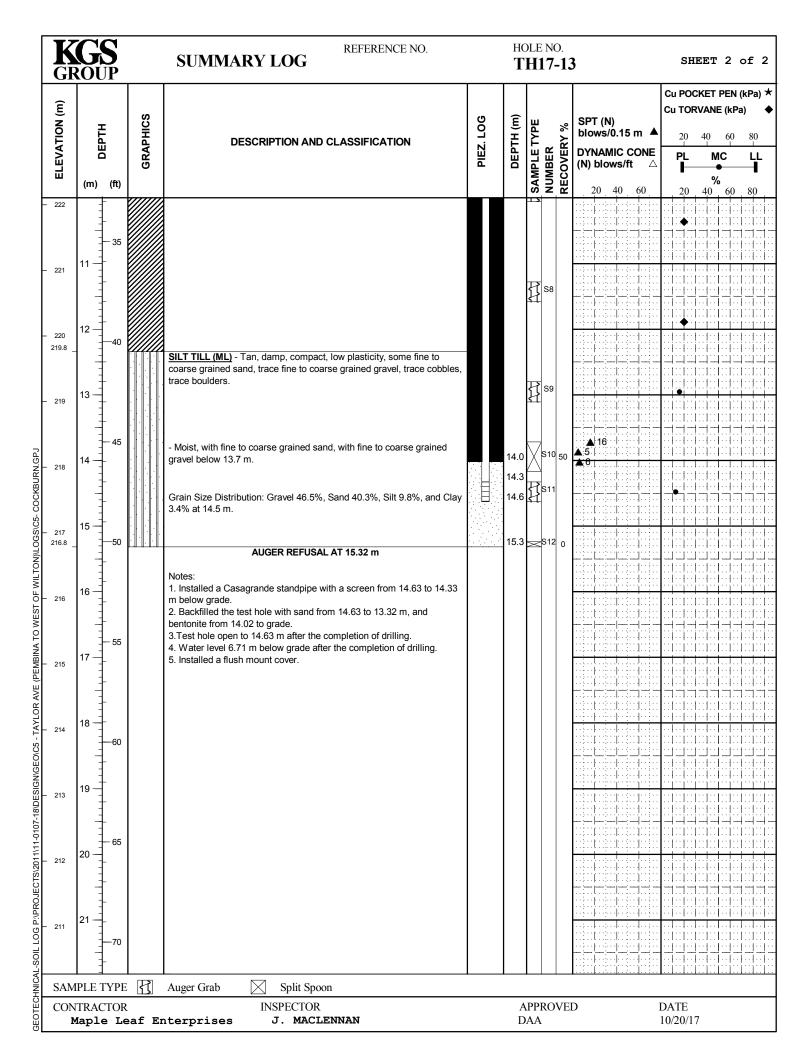




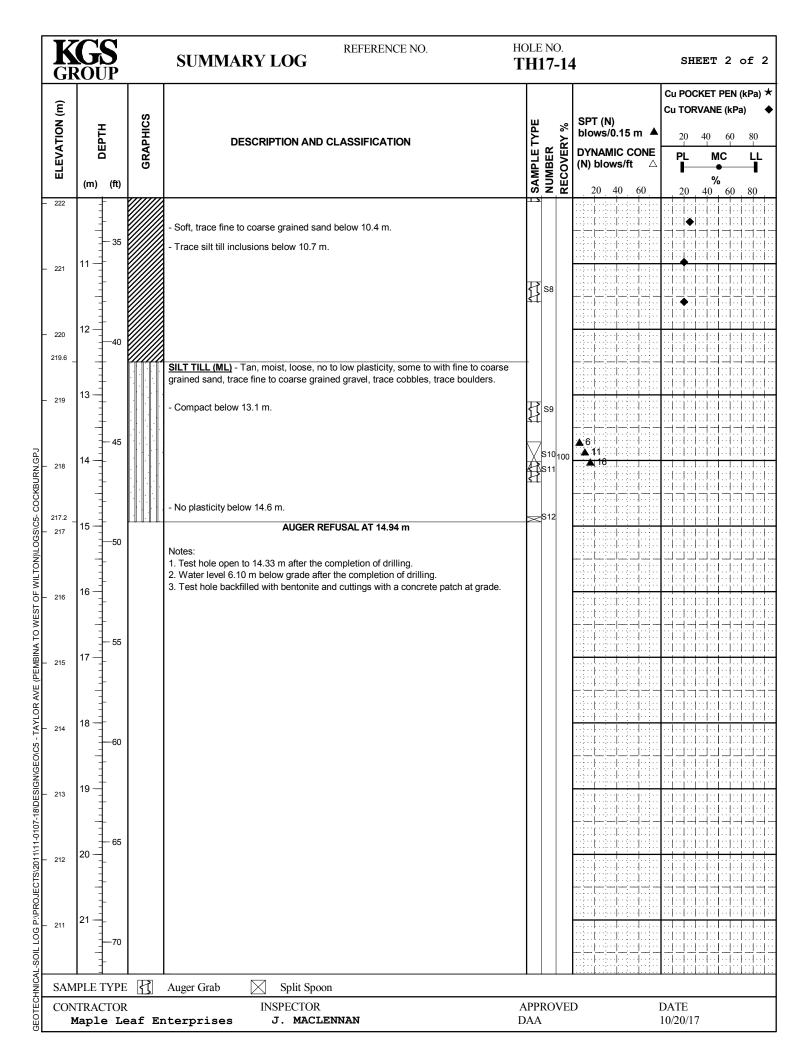
SITE	JECT	C Ta	ontra aylor A	F WINNIPEG - WATER AND WASTE DEPARTME ct 5 - Cockburn and Calrossie Sewer Relief ve Stafford St.	NT				GRO TOP WA <sup>T</sup> DAT	3 NO. OUND I OF PV TER EL TE DRII	C ELE .EV.	EV.	<ul><li>231.</li><li>4/26</li></ul>	5/201	17	
	LING HOD	12	5 mm	ø Solid Stem Auger, and NQ coring, B40X Truck Mounted	d Drill Ri	g			UTN	/I (m)				,524, 32,68		2
ELEVATION (m)	(3)	(ft)	GRAPHICS	DESCRIPTION AND CLASSIFICATION	PIEZ. LOG	DEPTH (m)	SAMPLE TYPE	NUMBER RECOVERY %	DYN (N) I	「(N) ws/0.15 NAMIC (blows/f	CONE	Cu T	20 4 PL	MC %	( <b>kPa</b> )	
231.9	=	io.	600	ASPHALT	20 23			<u> </u>				:: ::	1:: :	10.	:   : :	80
231.6 <u>=</u> 231.6	1		inin	CONCRETE  GRANULAR BASE (GW)	<b>183 18</b>											
201.0	‡			CLAY (CH) - Brown, damp, stiff, high plasticity.	<b>B B</b>		<b>1</b> 3	S1					Į::i:ī	dai:	gaj	::i::ī
231	11												1111	111	44	
					89 89								į::j::		iiii	•
	‡	5			<b>83 83</b>				 			   -	11 <del>  </del> -	.11   -	. I I ⊢ <b>♦</b> ⊢	
230.2					<b>88 8</b>									-		
230	2 —			SILT (ML) - Tan, moist, soft.	22 23								1		1	
					88 88			52					<u> </u>			
	-				88 88				;				ini	iii	11	
229.1	1		,,,,,	OLAV (OLD MAIN ALL MA	88 88								11			
229	3 —	10		CLAY (CH) - Mottled brown to grey, damp, stiff, high plasticity, trace silt inclusions.	<b>88 8</b>								Till:	<del>iii</del>	111	
	+				<b>88 88</b>								1	1	1111	
	]						ъ,	23						1.1:	10	
228	4 -				<b>22</b> 53		<b>!</b>	55					1	1		
	1				88 88											
		15			<b>88 8</b>											4-
								54 <sub>100</sub>					1	-  -    -  -  -  -  -  -  -  -  -  -	.     .	
227	5 🚽			- Unconfined Compressive Strength was measured to be 81 kPa at 4.9 m									<del>                                      </del>		1	<del></del>
	1			- Firm below 5.2 m.	82 83	5.5	17	S5						<b>♥</b> : ::		
	十				A 44	I 5.6	2.1						iti	iii:	iii	<u> </u>
226					88 88									.	.	
220	6-1	20		- Grey, moist below 6.1 m.	89 89		Н						Ţj	<u> </u>		
	1			- Water infiltrating test hole below 6.1 m.	88			100						111		
	1						<u> </u>	S7					11.	:     :   : -   :	·   · ·   . ] ]	
225	7 🕂						1	,				1	•	<u> </u>	<del></del>	
	1												11			
	1	25			80 80						44-	- -	<u>       -</u>	-  -	11	4-
	{	~ [					$\  \ _{\epsilon}$	58 100					11	. 1 1 :1::1	.11 :1::1	
224	8-			- Unconfined Compressive Strength was measured to be 84 kPa at 7.9 m.	<b>88 8</b>			100				1	++-	+	+++	
	}			m.			<b>[</b> ]	59								
					88 88		2.1		;				1.7.	1.1.		
223	9 —				89 89								<u>                                      </u>	<u> </u>	<u> </u>	<u> </u>
-		30		- Soft to firm, trace fine to coarse grained sand below 9.1 m.								<del> </del>	1T 1T	4. T. 1111		
	]			-							444		111	44.	11	
							 {{}s	10					• •   • • • • • • • • • • • • • • • •			
222					<b>SA S</b>	<u> </u>	114					1	1	1-1-	11	1
SAM	PLE TY	PΕ	<b>}</b>	Auger Grab Shelby Tube Split Spoon			Co	ore Ba	ırrel							
0.0	TRACT			INSPECTOR			DP-	OVE.				DAT				



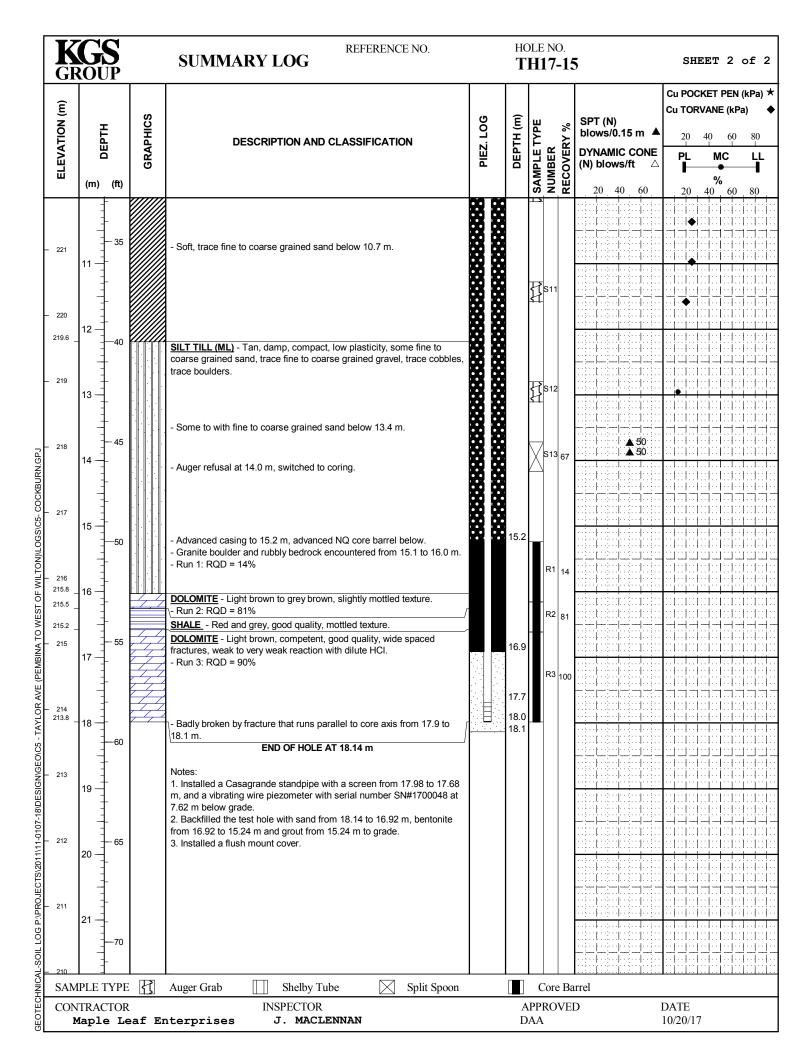
	K	Gi	S JP		SUMMARY LOG REFERENCE NO.			LE NO. <b>H17-1</b> 3	3	SH	EET	1 of	f 2
	CLII	ENT JEC		_	OF WINNIPEG - WATER AND WASTE DEPARTM act 5 - Cockburn and Calrossie Sewer Relief	IENT			JOB NO. GROUND ELEV. TOP OF PVC ELE	23	-0107 2.10	-18	
	SITI	E	٦	Taylor A	Ave				WATER ELEV.				
	LOC	ATIC	ON E	East of	Stafford St.				DATE DRILLED		25/201		
		HOD		25 mm	ø Solid Stem Auger, B40X Truck Mounted Drill Rig				UTM (m)	E	5,524 632,7	54	
	ELEVATION (m)		<u> </u>	GRAPHICS		907	DEPTH (m)	SAMPLE TYPE NUMBER RECOVERY %	SPT (N) blows/0.15 m	Cu POG Cu TOF	RVANE	(kPa)	<b>Pa) ★</b>
	VAT	L FOST	ב ב	RAP	DESCRIPTION AND CLASSIFICATION	PIEZ. LOG	EDT	ER.	DYNAMIC CONE	PL	MC		LL
		<b>.</b>		g				IMB ICO	(N) blows/ft △	⊩	%		-
		(m)	(ft)	e vestiva vest				S N N	20 40 60	20		60 8	80
	- 2 <del>332</del> 9 = 231.9	-			CONCRETE GRANULAR FILL (GW)								
		-			CLAY (CH) - Brown, damp, stiff, high plasticity.								
	231.3	-			SILT (ML) - Tan, moist, soft, low plasticity.								
	- 231	1 –			- Some clay from 0.8 to 1.1 m Water infiltrating test hole from granular base material.			₹ s1					
		-	— 5		3						13.13.13. 1-4-4-	:1::1:: 	11111
	230.3	-									    -		
3PJ	- 230	2 –	_		CLAY (CH) - Mottled brown to grey, damp, stiff, high plasticity, trace silt inclusions.							1	1
JRN.G		-						\$2 S2				: :: ::   <b></b>  -:	
CKBL		-											
S CO		3 —	—10								· ·   · ·   ·	1	1.1.
SS/CE	- 229	-	10		- Moist, firm below 3.1 m.								
WILTON)\LOGS		-											
TON-		=						<b>₹</b> 3			<b>♦</b>		-     -
OF WIL	- 228	4 —											
STO		-	15								: <b>Y</b> :   :    -	11:1:	
O WE		-	15										
INA	- 227	5 —										<del>                                      </del>	<del>.     .</del>
(PEMBINA TC		-						\$3 S4			• :: :		
VE (F		- -					İ	1				7.7.	
LORA		6 —										1	
TAYL	- 226	=	<del>-20</del>		- Grey below 6.1 m.								
\C2 -		-											
/GEC		<u>-</u>					İ	<b>₹</b> 55		• • • • •			
SIGN	- 225	7 —										1:1:	
18/DE		-										14-	14-
)107-′		-	— 25 —		- Increased silt inclusions below 7.6 m.								
1/11-0	- 224	8 —										++-	+++
3/201		-						₹ S6					
JECT.		-					Ì			<b>♦</b>			
PRO,	- 223	9 —									-    -	.11	.11.
)G P:\	223	=	<del>-30</del>		- Occasional fine to coarse grained gravel below 9.1 m.								
		=									- - -		
AL-SC		=			- Soft below 9.8 m.			₹ s7		::   •	-    -	<u> </u>	<u> </u>
Ú H H	SAM	PLE 7	ΓΥΡΕ	<u> </u>	Auger Grab Split Spoon								
TEC		TRAC			INSPECTOR			PPROVE		DATE			
Й	l N	ıap⊥	e Le	eaf Ei	nterprises J. MACLENNAN		D	AA		10/20/1	/		



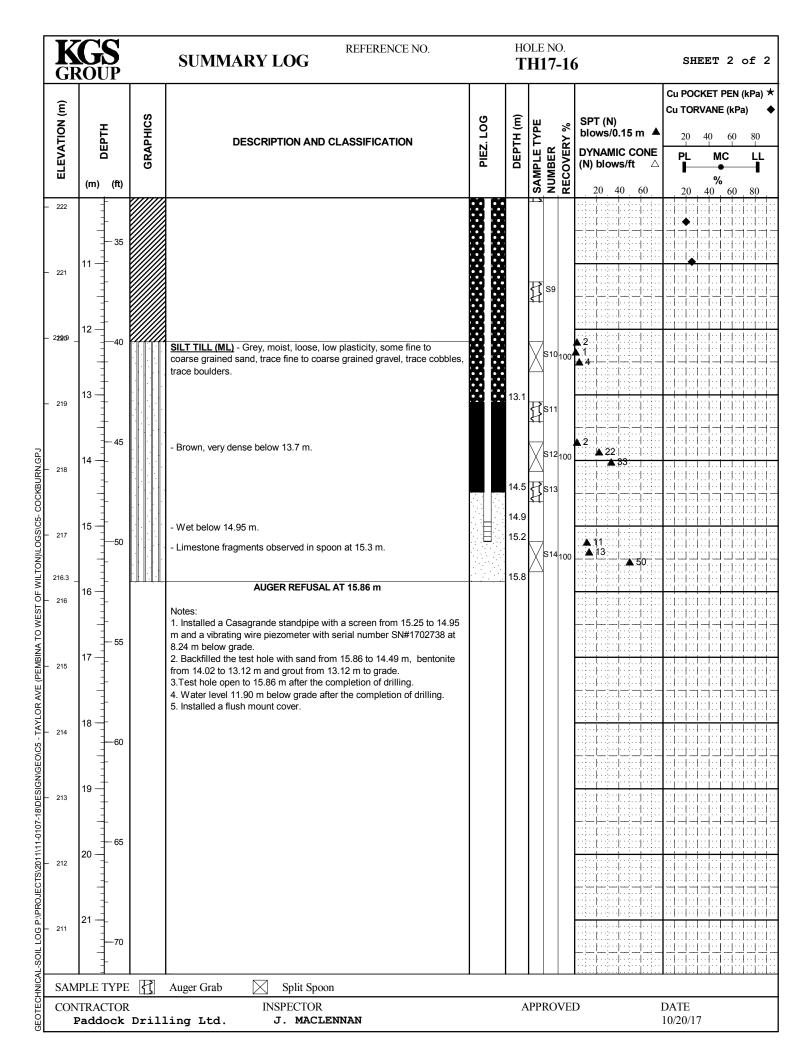
	K	GROU	S JP			HOLE TH1		4	SH	EET 1	of 2
	CLIE	JEC	т	Contra	OF WINNIPEG - WATER AND WASTE DEPARTMENT act 5 - Cockburn and Calrossie Sewer Relief			JOB NO. GROUND ELEV. TOP OF PVC ELE	23	-0107- 2.09	18
	SITE			aylor <i>A</i> Approxi	Ave mately 85 m East of Stafford St.			WATER ELEV. DATE DRILLED	4/2	25/201	7
	DRII MET	LLIN	G 1		ø Solid Stem Auger, B40X Truck Mounted Drill Rig			UTM (m)		5,524,5 632,80	
ŀ	ELEVATION (m)		<u> </u>	GRAPHICS	DESCRIPTION AND CLASSIFICATION	гуре	% X8	SPT (N) blows/0.15 m 🔺		CKET PERVANE (F	
	ELEVA	2	5	GRA		MPLE.	NUMBER RECOVERY %	DYNAMIC CONE (N) blows/ft △	PL.	MC	LL I
		(m)	(ft)	SVIKOVA VIS	CONCRETE	SAI	N N	20 40 60	20	<b>%</b> 40 6	0 80
ľ	- 231.9 _ 231.8 -	-	-		CONCRETE GRANULAR BASE (GW)						
	231.3	-	-		CLAY (CH) - Black, damp, stiff, high plasticity, some organics, trace fine to coarse grained sand.						
		1 -	-		SILT (ML) - Tan, moist, soft, low plasticity.		S1				
	- 231 230.9 _	-	-		CLAY (CH) - Brown. damp, stiff, high plasticity.						    <mark> </mark>
		-	<del>-</del> 5		- Trace silt inclusions below 1.5 m.						
.FJ	- 230	2 -									
JRN.G		-	-		- Mottled brown to grey below 2.3 m.	<b>}</b>	S2				
CKBI		-	-							    -≸	
C5- C	- 229	3 —	-10								· ·   · ·   · ·   · ·
.0GS\		-	-								
TON)/L		-	-		- Firm below 3.7 m.	<u> </u>	S3				:: :: :: ::  
F WIL	- 228	4 -	-			Z.T.					
EST 0		-	15							::  <mark>*</mark>  ::    -	:: :: :: ::  
TO W		=	"							11   11   11    11 <b>  ∳</b> 1   11	
/BINA	- 227	5 —	-			IP.	24				
E (PEN		-	}			<b>1</b>	54				
R AVE		-	-								
FAYLO	- 226	6 —	20								  ::: :: :: :: ::
50\c		-							44:		
N/GEC		7 –			- Grey, moist below 6.7 m.	<u>}</u>	S5			<b> </b>	
ESIG	- 225	-	-							   <b>♦</b>	::: :: :: ::  
)7-18∖Ľ		=	<u> </u>		- Soft to firm below 7.6 m.				- - -  :: :: ::	—  —  	- - -   :: :: :: ::
11-010	- 224	8 —	-								
\2011\		-	-			<u> </u>	S6				
JECTS		-	-			2.1					
:\PRO	- 223	9 —	30								· ·   · ·   · ·   · ·
-0G P		-	- 55								
SOIL		=	-			₹.	57				
GEOTECHNICAL-SOIL LOG PRPOJECTS\2011\11-0107-18\DESIGN\GEO\C5 - TAYLOR AVE (PEMBINA TO WEST OF WILTON)\LOGS\C5- COCKBURN.GPJ	SAM	PLE	l ГҮРБ		Auger Grab Split Spoon	\_\				<u> </u>	1111
TECHI	CON	TRAG	CTOR		INSPECTOR	APPR	OVE		DATE		
GEO	M	ſapl	e Le	eaf Er	nterprises J. MACLENNAN	DAA			10/20/1	7	

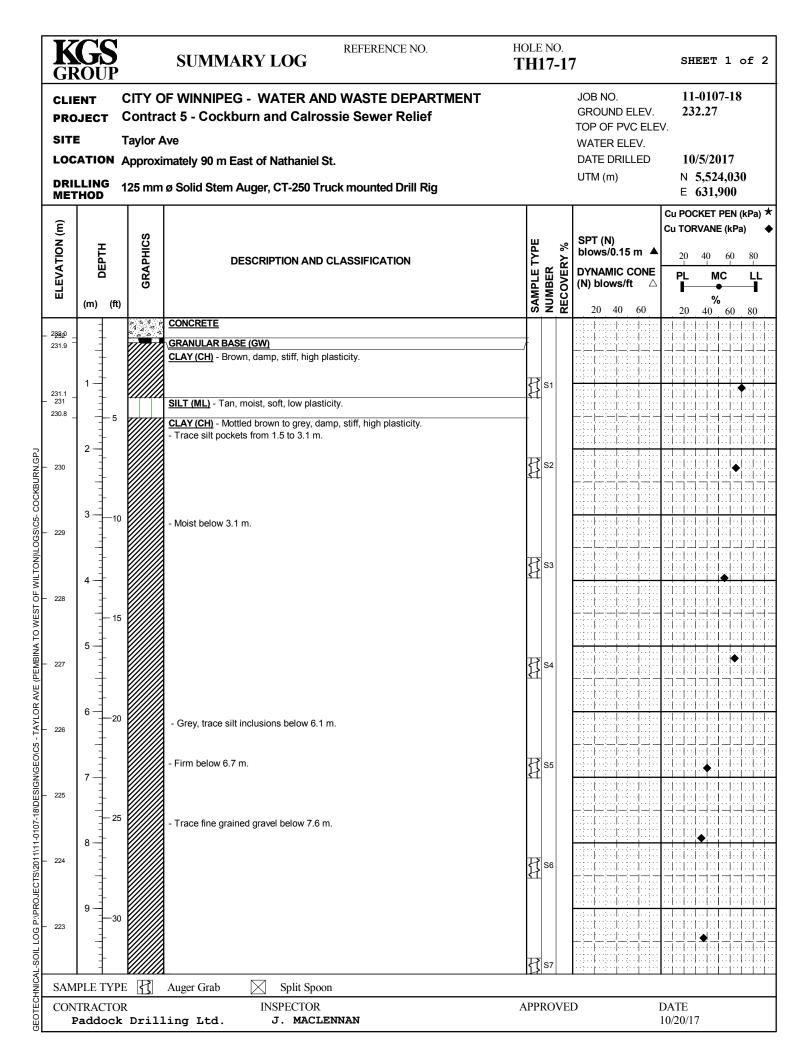


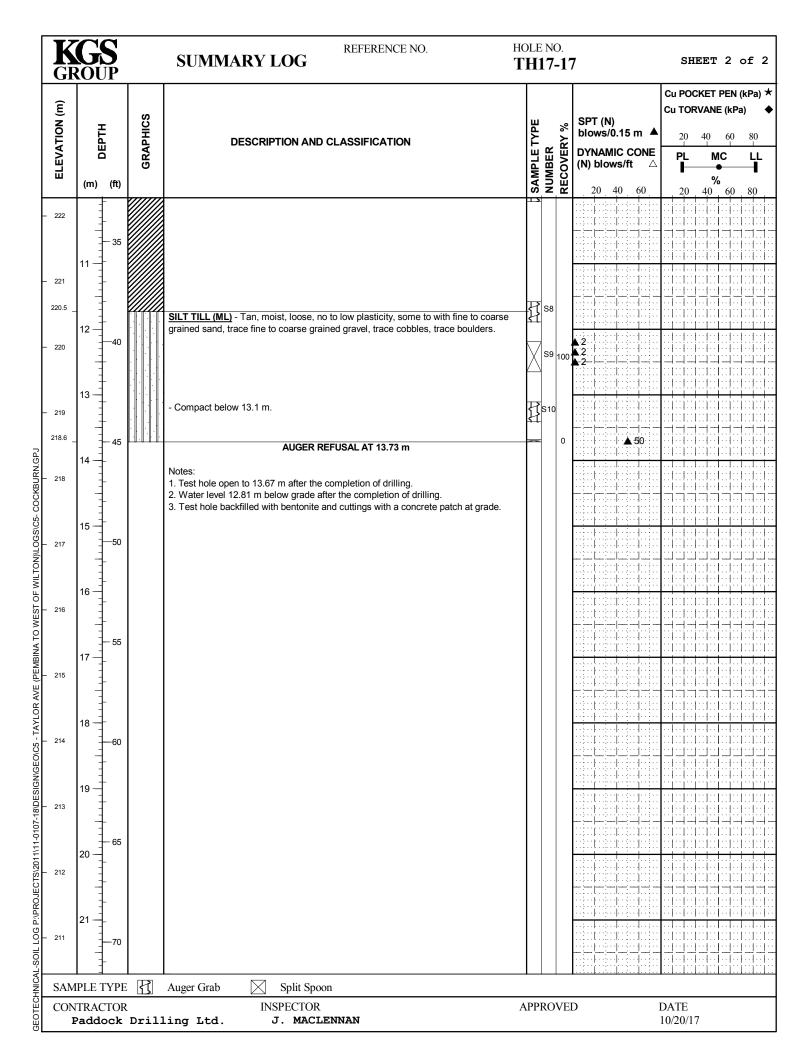
K GR	G	S JP		SUMMARY LOG REFERENCE NO.			)LE NO <b>H17</b> -		5	i	SHEE	т 1	. of	. 2
PRO	JEC.	т (	Contra	F WINNIPEG - WATER AND WASTE DEPARTME ct 5 - Cockburn and Calrossie Sewer Relief	NT				JOB NO. GROUND ELEV. TOP OF PVC ELE		11-01 231.7		18	
LOC. DRIL	ATIC	ON V	Taylor <i>A</i> Ventwo 25 mm		Drill Ri	9			WATER ELEV. DATE DRILLED UTM (m)	!	4/24/ N 5,5 E 63	524,5	580	
ELEVATION (m)	חבסים		GRAPHICS	DESCRIPTION AND CLASSIFICATION	PIEZ. LOG	<b>DEPTH</b> (m)	TYPE	RY %	SPT (N) blows/0.15 m	Cu F	POCKE	ET PE	N (kF (Pa)	Pa) ★
ELEV	(m)	(ft)	GRA		PIE	DEP	SAMPLE TYPE NUMBER	RECOVE	DYNAMIC CONE (N) blows/ft △ 20 40 60	ו   י	PL ■ 20 4	MC <b>%</b> 0 6		LL - <b>1</b> 30
231.6 _ 231.5 =	-	-		CONCRETE  GRANULAR FILL (GW)  CLAY FILL (CH) - Black, damp, stiff, high plasticity, some organics.	88 88 88 88 88									
- 233.b -	1 —	- -		NOOD CLAY (CH) - Brown, damp, stiff, high plasticity, trace silt inclusions.			<b>∏</b> S1							· ·   ·   · ·   ·   · ·   ·   · ·   ·
- 230 5	2 —	— 5 - -		- Mottled brown to grey below 1.5 m 75 mm silt lens at 2.1 m.	388888 3888888888888888888888888888888		Þ.						•	:    :    :    :
20 0 – 229	3 —	_		- Firm to stiff below 2.5 m.	333333 333333		\$ S2					*		-     -     -     -
20 – 228	-	—10 - -			388888 388888 3888888		Ps.							· ·   ·   · ·   ·   · ·   ·   · ·   ·
220	4 —	-			888888		S3					<b>*</b>		1::1:
0 – 227	5 —	_ 13		<ul> <li>- Unconfined Compressive Strength was measured to be 88 kPa at 4.9 m.</li> <li>- Grey, moist, firm below 5.2 m.</li> </ul>			S4 S5	100						· ·   c
2 2 3 4 5 7 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	6	- 20					<u></u> ₹1					*		1::1:
2 2 3 4 – 225	- - - - -	_		- Unconfined Compressive Strength was measured to be 82 kPa at 6.4 m.	38388 38388 38388		S6	100			] <u>                                     </u>	•		
	7 —	- - - 25		- Trace fine to coarse grained sand below 7.6 m.		7.6	ξ1.							
2 – 224	8 —	_ _ _		- Trace fine to coarse grained saild below 7.0 III.	88888	7.8	\$3 S8							
2 223	9 —	-30									1. <b>.</b>			1
2 222	- - - - -	_			33333 33333 33333		S9							
SAM	TRAC	CTOR		Auger Grab Shelby Tube Split Spoon INSPECTOR Atterprises J. MACLENNAN			Core PPRO AA			DAT: 10/20				

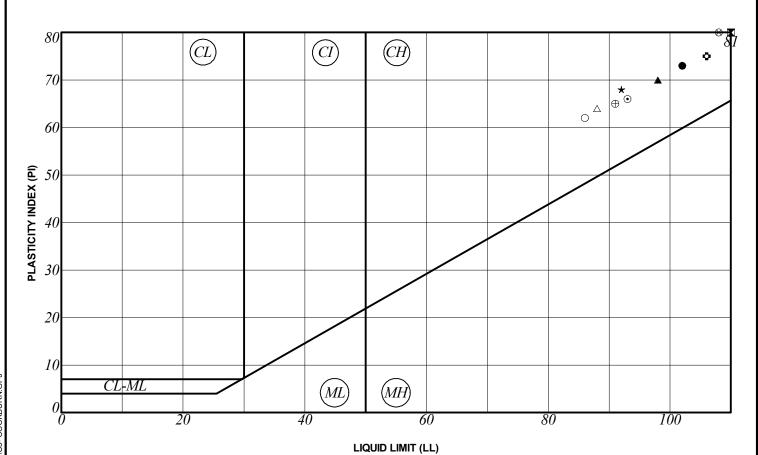


	K GR	G	S IP		SUMMARY LOG	NCE NO.		OLE NO. <b>H17-1</b>	6	SH	EET	1 o:	f 2
		JEC.			OF WINNIPEG - WATER AND WASTE act 5 - Cockburn and Calrossie Sewe				JOB NO. GROUND ELEV. TOP OF PVC ELEV	23	-0107 2.14	·-18	
	SITE			Taylor <i>I</i> ∆nnroxi	Ave mately 40 m West of Nathaniel St.				WATER ELEV. DATE DRILLED	10	/5/20	17	
	DRII	LLIN	G,		ø Solid Stem Auger, CT-250 Truck mounte	d Drill Ria			UTM (m)	Ν	5,523 631,7	,977	
ŀ		HOD	)	T						Cu PO			 Pa) ★
	ELEVATION (m)		_	ဗ္ဗ		ပ	Ê	ш ,	SPT (N)	Cu TOF	RVANE	(kPa)	•
	'ATIO	DEDTH	<u> </u>	GRAPHICS	DESCRIPTION AND CLASSIFICA	NOIT.	DEPTH (m)	R R ERY %	blows/0.15 m ▲ DYNAMIC CONE	20			80
	ELEV			g		=	DE	SAMPLE TYPE NUMBER RECOVERY %	(N) blows/ft △	PL I	M( • %	<u> </u>	LL ¶
ŀ	- 232	(m)	(π)	wwww	TOPSOIL - Black, damp, firm, trace roots, trace fine t	o coarse	66	\& \overline{\o	20 40 60	20	40	60 8	80
	- 232 231.8 _		-		grained sand.  SILT (ML) - Tan, moist, soft, low plasticity.	silt inclusions.		\$1					
	231.4 _	1 1	-		CLAY (CH) - Brown, damp, stiff, high plasticity, trace	silt inclusions.		FI so					
ŀ	- 231		_					\$2 \$2					
		-	<del></del> 5		- Mottled brown to grey, moist, trace silt inclusions be	elow 1.5 m.							
.GPJ	- 230	2-	-					F 53					.11.
KBURN			_					\$3 \$3					
2- COC		3 —	- 10									<u> </u>	::::::::::::::::::::::::::::::::::::::
OGS/C	- 229		-										
WILTON)\L			_		- Firm below 3.7 m.			\$4     S4					
JF WIL	- 228	4-	_					2.1					
WEST		-	— 15										.     . -  -  - :     .
NA TO	- 227	5 —	_							::i::i:: ::i::i::	i∷i≨i: <del>1ii</del>	::i::i:: <del>::i::i:</del>	:i::i: <del>:1::1:</del>
(PEMBINA	_ 221		_		- Grey below 5.2 m.			S5					
R AVE			-				8.2.8.8.8.8.8.8.8.8.8.8.8.8.8.8.8.8.8.8						
TAYLOR	- 226	6 —	—20										
O/C5 -		-	_					12					
SIGN/GEO/C5	- 225	7-	_					\$6 S6			<b>\Delta</b>   .		
18/DES			-							-1-1-	•     -   -		-  - -  -
1-0107-		8 —	— 25 -		- Silt till pocket, approximately 100 mm thick at 7.6 m - Trace fine grained gravel below 7.6 m.			E or					
2011/1	- 224		-			25. 10	184	\$7 			<b> </b>		
JECTS			_								<b>₩</b> 1.1:		
P:\PRO	- 223	9 -	-30		- Trace silt till pockets below 9.1 m.		8888888888				-     		-11- -11- -11-
L LOG I		-	-		- Trace siit tiii pockets below 9.1 Tii.								
AL-SOIL		-	_		- Soft below 9.8 m.			₹ S8		:: :: ::  -: -: •		.:j:::j:: - <u></u>	
CHNIC		PLE T			Auger Grab Split Spoon			nnnove	D.	ATT			
HOTE		TRAC <b>add</b>			INSPECTOR Ling Ltd. J. MACLENNAN		F	APPROVE		DATE 10/20/1	7		









SYMBOL	HOLE	DEPTH (m)	SAMPLE#	LL	PL	PI	% SAND	% SILT %	6 CLAY	% MC	CLASSIFICATION
•	TH17-01	3.8	S3	102	29	73				53.1	CH
	TH17-01	4.9	S4	110	29	81				55.4	CH
<b>A</b>	TH17-06	3.8	S3	98	28	70				48.7	CH
*	TH17-06	6.4	S6	92	24	68				50.0	CH
•	TH17-06	9.0	S9	93	27	66				48.4	CH
•	TH17-10	3.8	S2	106	31	75				54.2	CH
$\circ$	TH17-10	6.4	S6	86	24	62				47.8	CH
Δ	TH17-10	11.4	S11	88	24	64				48.5	CH
$\otimes$	TH17-15	4.9	S4	108	28	80				51.8	CH
$\oplus$	TH17-15	6.4	S6	91	26	65				50.4	CH

Notes:

**ML - Low Plasticity Silt** MH - High Plasticity Silt
CL-ML - Silty Clay
CL - Low Plasticity Clay
CI - Intermediate Plasticity Clay
CH - High Plasticity Clay

LL - Liquid Limit

PL - Plastic Limit PI - Plasticity Index

MC - Moisture Content

NP - Non-Plastic



# CITY OF WINNIPEG -WATER AND WASTE DEPARTMENT

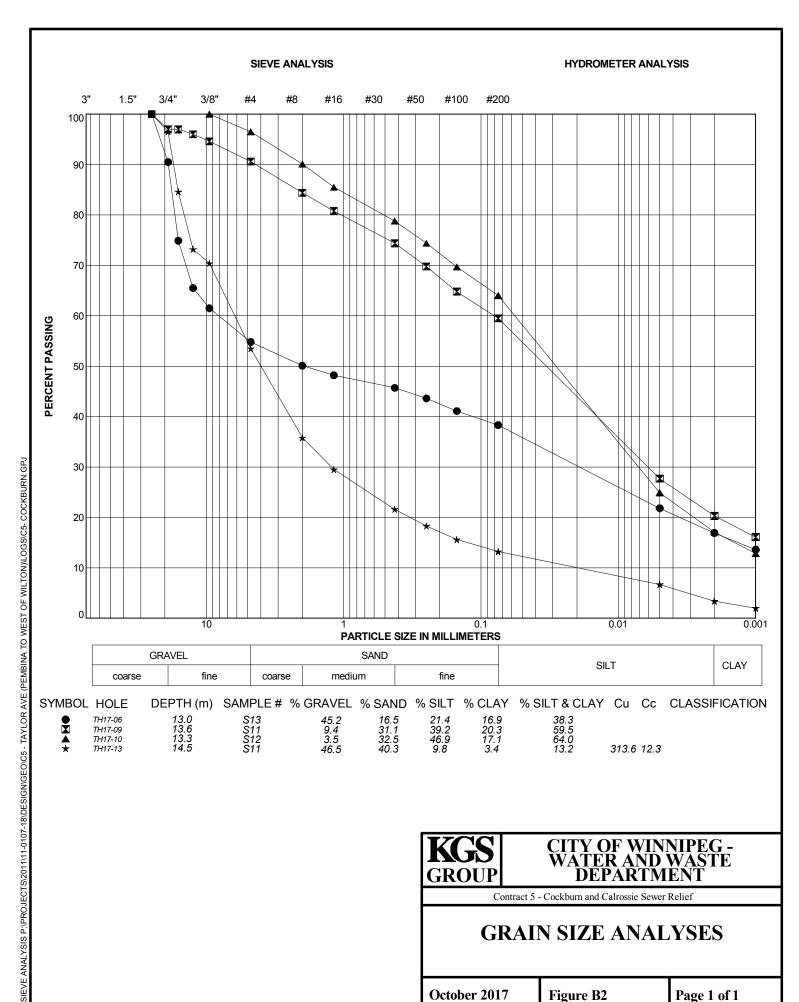
Contract 5 - Cockburn and Calrossie Sewer Relief

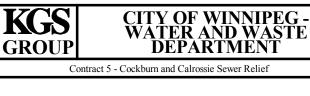
### **A-LINE PLOT**

October 2017

Figure B01

Page 1 of 1

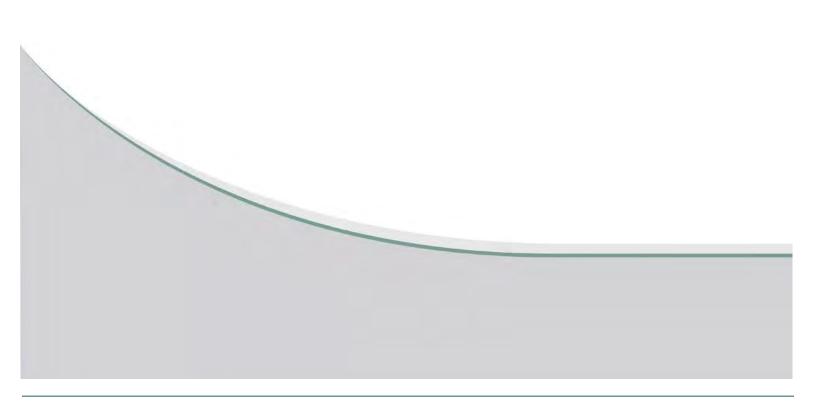




**GRAIN SIZE ANALYSES** 

October 2017 Figure B2 Page 1 of 1

# APPENDIX C 2018 TEST HOLE LOGS





## KGS GROUP

### SOIL DESCRIPTION CRITERIA

#### PRINCIPAL AND MINOR SOIL COMPONENTS

And 35-50% With 20-35% Some 10-20% Trace 0-10%

Occasional Trace of very local concentration

#### FIELD MOISTURE CONTENT

Dry No moisture visible or to touch when fresh exposure is examined

Damp Slightly wet to touch Moist Fresh exposure wet to touch

Wet A film of water is readily visible around particles of granular soils, cohesive soils can readily be smeared or remolded; water can be squeezed

out

Saturated Water can easily be squeezed out

Free Water Water completely separated from the soil particles

#### DEPOSITIONAL STRUCTURE

Massive Structureless soil

Stratified (Layered) Different soils or visible variations in soil constituents arranged in layers, generally but not necessarily parallel to one another,

and not necessarily in horizontal position, at least 6 mm thick

Varved Glaciolacustrine deposits with annual pairs of fine and coarser laminae (thin laminae of alternately deposited inorganic silt and

clay)

Laminated Closely spaced, regularly alternating layers of differing soils and/or colours, or shades of similar gradation, relatively consistent in

thickness and consisting of sand, silt, or clay

Lens Inclusions of a different soil within surrounding soils, which thins out horizontally and may not be continuous over any

significant distance

Pocket A different soil type of very limited thickness or lateral extent (a small lens)

Inclusions Small pockets

Nuggety A different soil type in the form of small lumps Parting Paper thin separation of one type by another

#### POST DEPOSITIONAL STRUCTURE

Fissured A soil breaks along definite, pre-existing planes or fracture with little resistance to fracturing

Slickensided Polished or glossy, sometimes striated surfaces resulting from movement of a material block relative to the adjacent blocks
Blocky/Friable/Platy Cohesive soil that can be broken down into angular larger fragments (blocky), small fragments (friable), or thin plate-like

fragments (platy) which resist further breakdown

Cemented Soil particles or fragments held together by cemented materials, often chemical precipitants, or deposits within overall soil mass

#### GRAIN SIZE DISTRIBUTION IN COARSE GRAINED SOIL

 $\begin{array}{lll} \mbox{Boulders} & >& 200 \mbox{ mm } \mbox{\o} \\ \mbox{Cobbles} & 75-200 \mbox{ mm } \mbox{\o} \\ \mbox{Coarse Grained Gravel} & 19-75 \mbox{ mm } \mbox{\o} \\ \mbox{Fine Grained Sand} & 4.75-19 \mbox{ mm } \mbox{\o} \\ \mbox{Coarse Grained Sand} & 2-4.75 \mbox{ mm } \mbox{\o} \\ \mbox{Medium Grained Sand} & 0.425-2 \mbox{ mm } \mbox{\o} \\ \mbox{Fine Grained Sand} & 0.075-0.425 \mbox{ mm } \mbox{\o} \\ \mbox{\o} \end{array}$ 

#### DENSITY OF GRANULAR SOIL

Description	Standard Penetration Test	Relative Density
Very Loose	0-4 Blows Per $0.3$ m	<15%
Loose	4 – 10 Blows Per 0.3 m	15 - 35%
Compact	10 - 30 Blows Per 0.3 m	35 - 65%
Dense	30 - 50 Blows Per 0.3 m	65 - 85%
Very Dense	>50 Blows Per 0.3 m	>85%

#### CONSISITENCY OF COHESIVE SOILS

Description	Torvane	Standard Penetration Test
Very Soft	<12 kPa	<2
Soft	12 – 25 kPa	2 - 4
Firm	25 - 50  kPa	4 - 8
Stiff	50 - 100  kPa	8 - 15
Very Stiff	100 - 200  kPa	15 - 30
Hard	>200 kPa	>30

	K	G	S JP		SUMMARY LOG REFERENCE NO.	HOLE NO. <b>TH18-</b> (	)1	SHEET 1 of 1
	CLI				OF WINNIPEG - WATER AND WASTE DEPARTMENT urn and Calrossie Sewer Relief		JOB NO. GROUND ELEV. TOP OF PVC ELE	11-0107-18 233.00 V.
	SITE				on Bay - East Lane		WATER ELEV.	
	LOC	ATIC	ON A	Approxi	mately 25 m North of Taylor Avenue		DATE DRILLED	5/2/2018
	DRII MET	HOE	G 1	25 mm	ø Solid Stem Auger B54X Mobile Track Mounted Drill Rig	1	UTM (m)	N 5,524,056 E 631,200
	ELEVATION (m)	     	DEP IN	GRAPHICS	DESCRIPTION AND CLASSIFICATION	SAMPLE TYPE NUMBER	SPT (N) blows/0.15 m  DYNAMIC CONE	Cu POCKET PEN (kPa) ★ Cu TORVANE (kPa) ◆  20 40 60 80
	ELEV,		그 (ft)	GR.		AMPLE	(N) blows/ft	PL MC LL
ŀ	222.0	(,	1,	PAFA	\ASPHALT	Ø Z i	20 40 60	20 40 60 80
	232.9 _ 232.8 -		1	WWW.W	CONCRETE	S1		
	232.6		}		GRANULAR FILL - Tan, moist compact to dense.	S1 S2		
ŀ	232.1 – 232	1 –	†	//////	TOPSOIL - Black, frozen, trace fine to coarse grained gravel, trace oxidation.	_/ -		
		:	1		<u>CLAY</u> - Mottled brown to grey, frozen, high plasticity, trace silt inclusions, trace oxidation.	S3		
		=	-5		oxidation.			
	- 231	2 -	1		- Moist, stiff below 1.8 m.			·····
			Ī			12 54		
		-	Ī			S4 S4		
	- 230	3 -	1					
	- 230	3 -	10					
		-	1					
			1			13 05		
GPJ	- 229	4 –	1			S5 S5		
-18		:	1					
107		=	15					
7	- 228	5 -	}					······································
Ë.		]	}					
OSS		-	}			₹ S6		
ALR	00070	=	†					
D C	- 2 <b>26</b> 79 _	6 –	20		END OF HOLE AT 6.10 m			
AAN		-	1					
J.		-	-		Notes:			
S	- 226	7 –	}		Test hole open to 6.10 m below existing grade.     Test hole dry immediately after drilling.			
O)		-	-		Test hole backfilled with cuttings and bentonite chips with concrete patch.			
368		:	25					
13/L(	- 225	8 –	-					
Ċ		:	+					
3\C		-	-					
GE	- 224	9 —	1					
<u>I</u>		ਁ	-30					
DES		-	1					
-18	000	10 =	1					
0107	- 223	10 —	1					
/11-		-	1					
2011			35					
TS	- 222	11 –	•					
JEC		-	1					
PRC			1					
3 P.	- 221	12 —						
ΓO		:	40					
β		:	1					
AL-S			<u>†                                    </u>					
GEOTECHNICAL-SOIL LOG P.\PROJECTS\2011/11-0107-18\DESIGN\GEO\C6 - C13\LOGS\COCKBURN AND CALROSSIE - 11-0107-18.GPJ	SAM	PLE	TYPE		Auger Grab			
넖			CTOR		INSPECTOR	APPROV	ED	DATE
ÉOJ					rilling Ltd. M. ALFARO	1		8/7/18
O					<del>-</del>			

K	G	S		CTT 53 5 1 DTT 5 C C	HOLE TH	E NO. <b>18-0</b>	2		SI	HEET	1	of 1
CL	IENT OJEC		_	OF WINNIPEG - WATER AND WASTE DEPARTMENT urn and Calrossie Sewer Relief			JOB NO. GROUND TOP OF F		23	1-010 <sup>6</sup> 32.42		3
SIT	Έ		Poseido	on Bay - East Lane			WATER E					
LO	CATI	ON .	Approxi	mately 250 m North of Taylor Avenue			DATE DR	ILLED		/3/201		_
	ILLIN THOI		125 mm	ø Solid Stem Auger B54X Mobile Track Mounted Drill Rig			UTM (m)			5,52, 631,		16
ELEVATION (m)	(m)	(ft)	GRAPHICS	DESCRIPTION AND CLASSIFICATION	AMPLE TYPE	NUMBER RECOVERY %	SPT (N) blows/0. DYNAMIC (N) blows	CONE s/ft △	Cu TO	40 M	60 IC	80 LL
222.2	+ ,	1		ASPHALT	8	<b>~</b> ~	20 40	60	20	40	60	80
232.2 - 2 <b>32</b> 21	= 3	1		CONCRETE	1							
232.1		}		GRANULAR FILL - Tan, moist, compact to dense.	11	S1						1::1::1::
231.7	1 –	†	ИИ	CLAY FILL - Grey, frozen, high plasticity, trace silt inclusions.	<u> </u>	S2						1
231.0 - 231	4			CLAYEY SILT - Light brown, frozen, low to intermediate plasticity, trace oxidation.		l I						1::1::1::
	7	5		CLAY - Mottled brown to grey, frozen, high plasticity, trace silt inclusions, trace oxidation.	13	S3						1
	2 -	Ī		- Moist, stiff below 1.8 m.						1		<u> </u>
- 230		1			L.	S4						1:1:1:
230	-				比	S4					ı <b>♥</b> !  :: ::	
	3 –	<u> </u>									<u> </u>	1::1::1::
		10									lada	Tadada
- 229	-	}							1			101010
_		1										
D CALROSSIE - 11-0107-18.GPJ	4 -	1			13	S5					<del>                                     </del>	1
<u>∞</u> – 228		}		- Firm below 4.3 m.						.   : :   <b>\ </b>		
107	7	15									i II I	1333
7	5 –	}								◆	تثث	1:::::::::
<u></u>		}										
SSO 227	-	}		- Grey, trace fine grained gravel below 5.5 m.								1333
ALR		}			R	S6					rii iii	1:1:1:1:
0	6-	20		- No oxidation below 6.1 m.		1						T
¥ - 226	_	}							1-1-1-			1::1::1:: 1::1::1::
N.		}			L							1:4:4:
8	7 –	}		- Increased trace silt inclusions below 7.0 m.	灯	S7				++++		1
O 225		+										
Ses		25								100		
13/L(	8 –	+								<u> </u>	1	1
ပ် မ – 224		-								. 1 1 1 : 1 : : 1 : : 1	1::1::	1::1::1::
900	-	}			11	S8				<b>†</b>	ıda	1818
GEG GEG	9 –	1									<u>rata</u>	1::1::1::
223.3		30		END OF HOLE AT 9.14 m	$\dashv$							
SHO 223	-	}								444	133	1444
-18/		1		Notes:  1. Test hole open to 8.84 m below existing grade.								1::1::1::
2107	10 -	}		Test hole open to 6.64 in below existing grade.      Test hole dry immediately after drilling.						inini	(aja	inini:
= 222	_	1		3. Water seeping from silt layer.						لالال	عقا	
201		35		4. Test hole backfilled with cuttings and bentonite chips with concrete patch.							(11111) 11111	100100100
XZT3X	11 -	}										1::1::1::
S - 221	1 3	ł						iddii:			<u>lata</u>	lididi
PRO		İ									  :: ::	1
<u>G</u>	12 —	İ	1							<del>                                      </del>	<del>-  -</del>	<del>                                      </del>
0 220		40	1									
팅	-	1	1								H	1-1-1-
AL-S		<u>†</u>										<u>   </u>
SAI	MPLE	TYP	E <b>[</b> ]	Auger Grab								
5	NTRA			INSPECTOR	APP	ROVE	D		DATE			
				rilling Ltd. M. ALFARO		-512			8/7/18			
ڻ ا				-								

K	GROU	S JP		SUMMARY LOG REFERENCE NO.	HOLE TH	E NO. <b>18-0</b> .	3	SHEET 1 of 1			
CLIENT PROJECT			_	OF WINNIPEG - WATER AND WASTE DEPARTMENT urn and Calrossie Sewer Relief			JOB NO. GROUND ELEV. TOP OF PVC ELEV	11-0107-18 232.35			
SIT	E	7	Taylor A	Avenue - North Curb Lane			WATER ELEV.	•			
LOC	ATIC	) N	Approxi	mately 230 m East of Poseidon Bay			DATE DRILLED	5/3/2018			
	LLIN		125 mm	ø Solid Stem Auger B54X Mobile Track Mounted Drill Rig			UTM (m)	N 5,523,809 E 631,450			
ELEVATION (m)	(m)		GRAPHICS	DESCRIPTION AND CLASSIFICATION	SAMPLE TYPE	NUMBER RECOVERY %	SPT (N) blows/0.15 m  DYNAMIC CONE (N) blows/ft   20 40 60	Cu POCKET PEN (kPa) * Cu TORVANE (kPa)   20 40 60 80  PL MC LL  % 20 40 60 80			
232.3 -			D 4 4 B	ASPHALT	1			:: :: :: :: :: :: :: :: :: :: :: :: ::			
- 232 232.1	1 -	-		CONCRETE   SILT - Light brown, moist, firm, low to intermediate plasticity, with clay, trace oxidation.	_/ ∏	S1		•			
- 2 <u>3</u> 3,0 -	1 =	_		- Frozen below 1.2 m.		S2					
		— 5 -		<u>CLAY</u> - Mottled brown to grey, frozen, high plasticity, trace silt inclusions, trace oxidation.	μ						
- 230	2 —	-		- Trace fine grained gravel below 1.5 m. - Moist, stiff below 1.8 m.	II	S3					
- 229	3 -	—10 - -									
D CALROSSIE - 11-0107-18.GPJ	4	- - 15 -		- Trace gypsum nodules, no fine grained gravel below 4.0 m.	<u> </u>	S4					
- 227 - 227 - 227	5	-			1	S5					
WBURN AND 226 – 226	7	20 - - -		- Grey, firm below 6.1 m.	₹?	S6					
13/LOGS/CO0	8 -	- 25 -		- Trace to some silt inclusions below 7.2 m.							
O - 90\OEON	9 -	- - - 30			1	S7					
107-18/DESIG	10	- - -		- Trace to some fine to coarse grained gravel below 9.8 m.	<u> </u>	S8					
222	] =	_ 25			_  }	S9					
5\201	11 -	— 35 -		END OF HOLE AT 10.67 m							
226   226	12 —	-		Notes: 1. Test hole open to 10.36 m below existing grade. 2. Test hole dry immediately after drilling. 3. Water seeping from silt layer.							
AL-SOIL LOG		40 - -		Test hole backfilled with cuttings and bentonite chips with concrete patch.							
SAM	IPLE T	ГҮРЕ		Auger Grab							
CON	NTRA(			INSPECTOR rilling Ltd. M. ALFARO	APP	ROVE		DATE 8/7/18			

	K	GS	S P		SUMMARY LOG REFERENCE NO.	HOLE TH1		1	SHEET 1 of 1	1
ļ	CLIE	ENT JECT	_		F WINNIPEG - WATER AND WASTE DEPARTMENT urn and Calrossie Sewer Relief			JOB NO. GROUND ELEV. TOP OF PVC ELEV	11-0107-18 232.28	
	SITE				venue - North Service Road			WATER ELEV.		
	LOC	ATIOI	ΝД	pproxi	mately 115 m East of Cambridge Street			DATE DRILLED UTM (m)	5/3/2018 N 5,524,380	
	DRII MET	LLING HOD	1:	25 mm	ø Solid Stem Auger B54X Mobile Track Mounted Drill Rig			O TWI (III)	E 631,430	
	ELEVATION (m)	ОЕРТН		GRAPHICS	DESCRIPTION AND CLASSIFICATION	TYPE	NUMBER RECOVERY %	SPT (N) blows/0.15 m  DYNAMIC CONE	Cu POCKET PEN (kPa) Cu TORVANE (kPa)  20 40 60 80	<b>★</b>
	ELEV,	٥		GR.		MPLE	MBEF	(N) blows/ft $\triangle$	PL MC LL	
		(m)	(ft)			SAI	N N	20 40 60	<b>%</b> 20 40 60 80	
-	232.2 - 232.2 232.1 - 232.1	1-1	- 5		CONCRETE  CLAY - Mottled brown to grey, frozen, high plasticity, trace silt inclusions.  - Trace fine grained gravel between 0.6 m and 0.9 m.		S1		•	
-	- 230	2 - 1	-10		- Moist, stiff below 1.4 m Trace oxidation below 1.7 m.	母	S2			
GPJ	- 229	4	10			<u> </u>	S3			: :   : :   : :   : :
GEOTECHNICAL-SOIL LOG P.\PROJECTS\2011\11-0107-18\DES\GN\GEO\C6 - C13\LOGS\COCKBURN AND CALROSSIE - 11-0107-18.GPJ	- 228 - 227	5 6	- 15 20						•	
S/COCKBURN AND	- 226 - 225 224.7	7-1			- Grey, firm, no oxidation below 7.0 m.	<u> </u>				
GEO\C6 - C13\LOG	- 224	8 9	- 25		Notes:  1. Test hole open to 4.57 m below existing grade.  2. Test hole dry immediately after drilling.  3. Test hole backfilled with cuttings and bentonite chips with concrete patch.					
1-0107-18\DESIGN	- 223 - 222	10 -	-30							
P:\PROJECTS\2011\1	- 221	11	- 35							
JICAL-SOIL LOG	- 220 SAM	PLE T	-40 VPF		Auger Grab					
TECHI	CON	TRAC	ΓOR		INSPECTOR	APPR	ROVE		DATE	_
GEO	M	Maple	Le	af Dr	rilling Ltd. M. ALFARO				8/7/18	

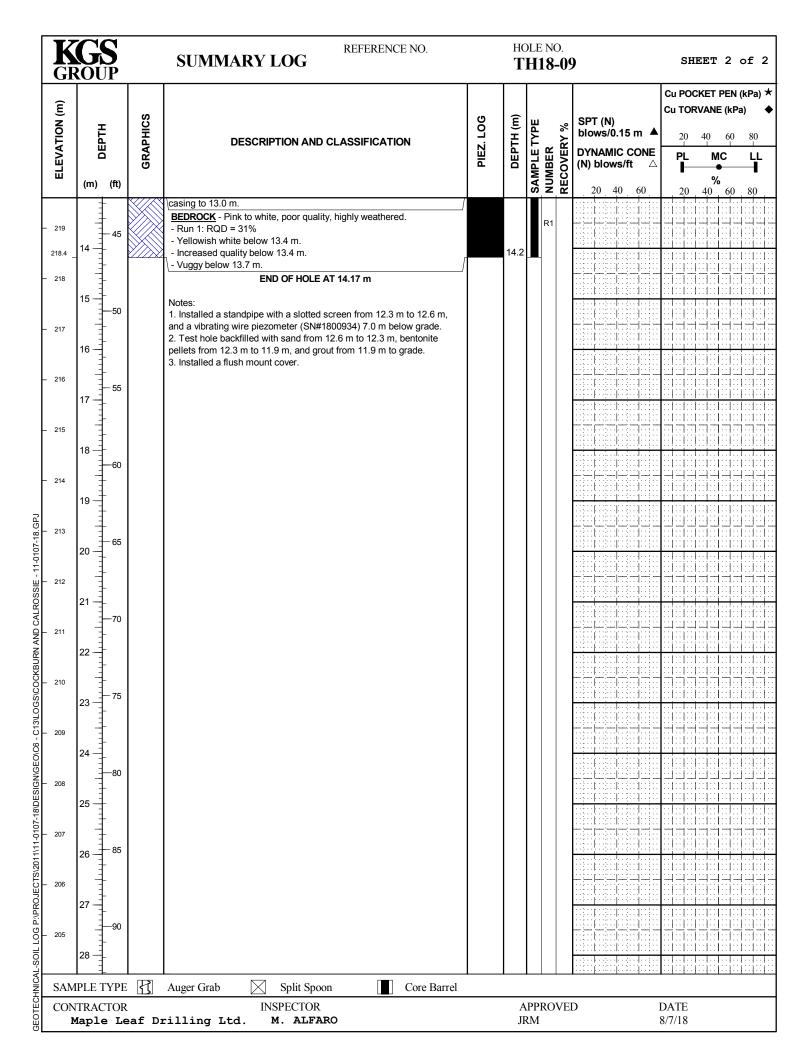
	K GF	G	S JP		SUMMARY LOG  REFERENCE NO.	HOLE TH1		5					SHE	ET :	1 0	f 1
•	CLII PRO SITI	JEC	т (	TO TO									11-0107-18 232.03			
					mately 50 m South of Grant Avenue				TER TED				5/7/	/2018	3	
	DRII MET	HOL	G 1	25 mm	ø Solid Stem Auger B40 Truck Mounted Drill Rig			UT	M (m	)			E 6	,524, 31,50	69	
	ELEVATION (m)		E E	GRAPHICS	DESCRIPTION AND CLASSIFICATION	MPLE TYPE	NUMBER RECOVERY %	SP blo DY (N)	T (N) ows/C NAM blov	).15 r IC C(		Cu ·	TORV	/ANE (	( <b>kPa)</b>	(Pa) ★  80  LL
		(m)	(ft)		DACDUAL T	S	3 2		20	40	60		20		60	80
	232.0 _ 231.7		-	P & d P	<u>\asphalt</u> \ <u>concrete</u>	─/			11:12:		1::::::					
	231.1		-		SILT - Light brown, frozen, low to intermediate plasticity, trace fine to coarse grained sand, trace oxidation.		S1									
	- 284.10 -	1 –			SANDY SILT - Tan, moist, trace clay, trace oxidation.	/1	- 1		1	1	1		. <del>    .</del>	<del>.    </del>	1	<del> </del>
		-	- 5		SILT - Light brown, moist, firm, low to intermediate plasticity, trace oxidation.  - Moist to wet below 1.4 m.		S3				-		445	-1-1	-	
	- 230	2 —	-		Work to Wel below 1.4 III.	<i>₹</i> ₹	64A		1	1	1		1::1:	1	1	
	229.6						64B	;								
			-		CLAY - Mottled brown to grey, moist, firm to stiff, high plasticity, trace silt inclusions, trace oxidation.	<u> </u>	S5									
ł	- 229	3 —	-10			13			tiiti	li ii	<u>luiu</u>	:::::::	1:1:		1::1:	
		-			- Grey below 3.4 m.						1		-1::1: -1::1:			
2	- 228	4 -	-			<u> </u>	S6				1000					
-18.G			-													
0107			15					;								
+	- 227	5 –							1::3:	<u> </u>	1		1:1:	<u>-11</u> :1::1::	<u>1::1:</u>	
SSIE		-	-													
ND CALROSSIE - 11-0107-18.GPJ	295-0	=	-					;			1::::::	::1::	1:1:	11:11:	1::1:	::1::1::
	_ 2 <u>25</u> @ _	6 –	20		END OF HOLE AT 6.10 m											
RNA		-			Notes:						1		Н.Н.		1.1:	
ЖВ	- 225	7 -	-		Test hole open to 6.10 m below existing grade.     Test hole dry immediately after drilling.			;	1	<u> </u>	1		<del>                                      </del>			
3/00			-		Test hole dry immediately after drilling.     Test hole backfilled with cuttings and bentonite chips with concrete patch.								.1::1: 1111:	: :: :: 		
LOGS			25													
.C13	- 224	8 –							1::2:	1:3:	<u>laia</u>	:::::::	1:1:		1::1:	
9)(6		-	-													
N/GE(	- 223	9 —							:t:::::		J::::::  ::::	::1::	.1::1: .11.	11:11:	:1::1: :1::1:	.:::::::::::::::::::::::::::::::::::::
SSIG			<del>-</del> 30					::}::								
-18\D			-								İ. i.					
0107	- 222	10 —	-								1	::::::				
1111		-	35												1	
\$\20	- 221	11 –	- "						1::5:	1		:::::::	1:1:	11:11:	<u> </u>	<u> </u>
JEC			-													
:\PRC																
OG P	- 220	12 —	40						<del>. t</del>	<del>1</del>	<del> </del> 		<del>:  -</del> : :: :	<del>                                      </del>	<del>    .    </del>	<del>.   .   .</del> :   :   :   :
OIL L		-	-								-			44		
SAL-S			<u> </u>	<u> </u>						ļ	<u> </u>		1:11			
CHNIC		PLE '			Auger Grab											
GEOTECHNICAL-SOIL LOG P.\PROJECTS\2011\11-0107-18\DESIGN\GEO\C6 - C13\LOGS\COCKBURN A		TRA(			INSPECTOR rilling Ltd. M. ALFARO	APPR JRM	ROVE	D				DAT 8/7/1				

	K	GROU	S JP		SUMMARY LOG REFERENCE NO.	HOLE TH1		5	SH	EET	1 (	of 1	
	CLII	ENT DJEC			OF WINNIPEG - WATER AND WASTE DEPARTMENT urn and Calrossie Sewer Relief			JOB NO. GROUND ELEV. TOP OF PVC ELE	23	11-0107-18 231.76			
	SITI				Avenue - North Lane			WATER ELEV.	<b>=</b> 10	2/201	0		
			_		mately 25 m East of Nathaniel Street			DATE DRILLED UTM (m)		3/2018 5,524		l	
	ME1	LLIN THOD	1	25 mm	ø Solid Stem Auger B54X Mobile Track Mounted Drill Rig					631,7			
	ELEVATION (m) DEPTH			GRAPHICS	DESCRIPTION AND CLASSIFICATION	E TYPE	NUMBER RECOVERY %	SPT (N) blows/0.15 m   DYNAMIC CONE	Cu POC Cu TOR	RVANE	(kPa	-	
	ELE			5		MPL		(N) blows/ft △	Ē	**************************************		Ť	
ļ	_	(m)	(ft)		√ASPHALT	S	<u> </u>	20 40 60	20		60	80	
	231.7 _ 231.5		-		CONCRETE	<b>7</b>							
ŀ	- <sup>231.0</sup> -	1 -	-		CLAY FILL - Black, frozen, intermediate plasticity, trace fine to coarse grained gravel, trace organics, trace silt inclusions.		S1						
			_		<u>CLAY</u> - Mottled brown to grey, frozen, high plasticity, trace silt inclusions.	_ 	S2						
ŀ	- 230		- 5 -		- Moist, stiff, trace oxidation below 1.5 m.							<b>→</b>   -	
		2 -	-			13/	20						
	- 229					<u> </u>	53						
	220	3 —	-10										
		=	-										
ιĐ	- 228	4 -	-		- Firm below 3.7 m.	<u> </u>	S4						
7-18.G			-										
1-0107	- 227		— 15 -										
iE - 1		5 -	-		- Trace fine to coarse grained gravel below 5.2 m.								
ROSS	- 226				- Grey below 5.5 m.	<u> </u>	S5						
CAL		6 -	-20								1		
N AN		-	-										
KBUF	- 225	7 -			- Soft, increasing trace silt inclusions below 7.0 m.	١٦	26		:: :. <b>Y</b> ::		<del>                                      </del>		
SICOC		]	-				50			?!::!:: : ك ك	:::: !::!		
\LOG	- 224	8 -	— 25 -		Tour to the Control of the Control o								
- C13		0	-		- Trace to some fine to coarse grained gravel below 8.0 m.				::1::1::1	:::::::::::::::::::::::::::::::::::::::	11:11		
EO/C6	- 223	=				<b>₹</b>	57						
GN/G	222.6	9 —	-30		END OF HOLE AT 9.14 m					. <del></del>			
NDESI	- 222	-	-		Notes:								
107-18	_ 222	10 -	-		1. Test hole open to 5.18 m below existing grade.     2. Test hole dry immediately after drilling.						<del></del>		
1/11-0		-			Test hole dry infinediately after driffing.     Test hole backfilled with cuttings and bentonite chips with concrete patch.				داداتا				
S\201	- 221	11 -	— 35 -								1111		
JECT			-										
:\PRC	- 220												
-0G P		12 —	<del>4</del> 0							<del>.   .   .</del>  :: :: :			
SOIL L	- 219		-										
GEOTECHNICAL-SOIL LOG PAPROJECTS/2011/11-0107-18/DES/GN/GEO/C6 - C13/LOGS/COCKBURN AND CALROSS/E - 11-0107-18.GPJ		I <u> </u>	ГУРБ		Auger Grab			<u> </u>		···	<u> </u>		
TECHI		TRAC			INSPECTOR	APPR	OVE	D 1	DATE				
Maple Leaf Drilling Ltd. M. ALFARO JRM 8/7/18													

	K	G	S IP		0 T T T T T T T T T T T T T T T T T T T		E NO. <b>18-0</b> ′	7	SHEE	T 1	of 1	
	CLII	ENT JEC1		_	F WINNIPEG - WATER AND WASTE DEPARTMENT urn and Calrossie Sewer Relief			JOB NO. GROUND ELEV. TOP OF PVC ELEV	11-0107-18 232.13			
	SITI				venue - North Service Road			WATER ELEV.	<i>5 12 1</i> 2	010		
			_		mately 650 m East of Cambridge Street			DATE DRILLED UTM (m)	5/3/2 N 5,5	018 524,59	4	
		HOD		25 mm	ø Solid Stem Auger B54X Mobile Track Mounted Drill Rig			. ,	E 63			
	ELEVATION (m)	(B) DEPTH	i i (ft)	GRAPHICS	DESCRIPTION AND CLASSIFICATION	AMPLE TYPE	NUMBER RECOVERY %	SPT (N)	Cu POCKE Cu TORVA  20 40 PL	NE (kPa		
	- 2 <del>33</del> 21 -	(''') 	(11)	D 4 9 D	∖ASPHALT	<u>  3</u>	Z Z	20 40 60	20 40	0 60	80	
	231.9 231.4 231.4 _	1-1	- - - - - 5		CONCRETE  CLAY FILL - Grey, frozen, high plasticity, trace fine to coarse grained sand, trace fine to coarse grained gravel.  SILT - Light brown, frozen, with clayey silt, trace oxidation, trace fine to coarse grained gravel.	/1	S1 S2					
	230.1 _ - 230	2-	-		<u>CLAY</u> - Mottled brown to grey, moist, stiff, high plasticity, trace silt inclusions, trace oxidation.		S3					
-18.GPJ	<ul><li>229</li><li>228</li></ul>	4-1	—10 - - -		- Firm below 4.3 m.	<u> </u>	S4					
D CALROSSIE - 11-0107-18.GPJ	- 227	5-1	— 15 - - -			<u> </u>	S5					
COCKBURN AND C	<ul><li>226</li><li>225</li></ul>	7	20 - - -		- Grey below 6.1 m Trace to some silt inclusions below 7.0 m.	<u>₹</u>	S6					
368/0	224.5	-	- 25		END OF HOLE AT 7.62 m	-						
GEO/C6 - C13/LC	- 224	8 7 7 1	- - -		Notes:  1. Test hole open to 7.16 m below existing ground surface immediately after drilling.  2. Test hole dry immediately after drilling.  3. Test hole backfilled with cuttings and bentonite chips with concrete patch.							
107-18\DESIGN	<ul><li>223</li><li>222</li></ul>	10 —	<del></del> 30 - -									
JECTS\2011\11-0	- 221	11 -	- 35 - -									
GEOTECHNICAL-SOIL LOG P./PROJECTS/2011/11-0107-18/DESIGN/GEO/C6 - C13/LOGS/COCKBURN AN	- 220	12 —	- 40 -									
INICAL	SAM	PLE T	YPE		Auger Grab			1 : 1 : [13:11:3:1]	1 111	1 11.	1 1 1 1 1 1 1 1	
GEOTECH		TRAC			INSPECTOR rilling Ltd. M. ALFARO	APP JRM	ROVE		OATE /7/18			

	K	G	S IP		SUMMARY LOG  REFERENCE NO.	HOLE I		3	SHEET 1 o	f 1	
	CLIENT PROJECT			Cockb	OF WINNIPEG - WATER AND WASTE DEPARTMENT urn and Calrossie Sewer Relief	JOB NO. GROUND ELEV. TOP OF PVC ELE	11-0107-18 231.70				
	SITE				Avenue - North Lane mately 230 m West of Wilton Street			WATER ELEV. DATE DRILLED	5/7/2018		
	DRII	LLING	<b>3</b> 1		ø Solid Stem Auger B40 Truck Mounted Drill Rig			UTM (m)	N 5,524,353 E 631,974		
	ELEVATION (m)	(B)		GRAPHICS	DESCRIPTION AND CLASSIFICATION	SAMPLE TYPE	NUMBER RECOVERY %	SPT (N) blows/0.15 m   DYNAMIC CONE (N) blows/ft   20 40 60	PL MC	-	
İ	231.5 -	=	_	p s q p Www.	CONCRETE  CLAY FILL - Black, frozen, intermediate plasticity, trace silt inclusions, trace fine	_				:1::1::	
-	- 231		-		grained gravel.  - Trace organics from 0.2 m to 1.1 m.	13	24				
	230.3	1 -	-		- Brown below 1.1 m.						
	- 2 <del>2</del> 399	1	- 5		<u>SILT</u> - Light brown, frozen, intermediate plasticity, trace oxidation.	138	32				
	_	2-1	-		<u>CLAY</u> - Mottled brown to grey, moist, stiff, high plasticity, trace rootlets, trace silt inclusions, trace oxidation.		63				
107-18.GPJ	- 229 - 228 - 227	3 — 1 — 1 — 1 — 1 — 1 — 1 — 1 — 1 — 1 —	- 10 - - - - - -				3	64			
GEOTECHNICAL-SOIL LOG PAPROJECTS/2011/11-0107-18/DES/GN/GEO/C6 - C13/LOGS/COCKBURN AND CALROSSIE - 11-0107-18.GPJ	- 226	5 - 1	- - - - 20		- Grey below 4.9 m.	13	55		• • • • • • • • • • • • • • • • • • •		
SS/COCKBUR	- 225 224.1 _	7-	- - - 25				S6				
26 - C13/LOG	- 224	8-1	-		Notes:  1. Test hole open to 7.62 m below existing grade.						
DESIGN/GEO	- 223	9   1	- 30 -		Test hole dry immediately after drilling.     Test hole backfilled with cuttings and bentonite chips with concrete patch.						
\11-0107-18\	- 222	10 -	-								
JECTS\2011	- 221	11 -	35 - -								
OG P:\PRO	- 220	12 —	- - 40								
SOILL	- 219		-						4444444		
NICAL-	SAM	L 3 PLE 1	үрг		Auger Grab		1		<u></u>		
GEOTECH	CON	TRAC	TOR		INSPECTOR rilling Ltd. M. ALFARO	APPR JRM	.OVEI		DATE 8/7/18		

K	G	SP		SUMMARY LOG REFERENCE NO.			LE NO. <b>H18-(</b>	9				SHE	EET	1 (	of	2
CLIE PRO	ENT JECT		_	OF WINNIPEG - WATER AND WASTE DEPARTMI urn and Calrossie Sewer Relief	ENT			C	OB NO. GROUND E OP OF PVO				-0107 2.60	7-18		
SITE	E	,	Wilton S	Street - West Lane					VATER ELE		.V.					
LOC	ATIO	N	Approxi	mately 20 m South of Grant Avenue					ATE DRIL	_ED		5/4	/201	8		
	LLING		125 mm <u>Drill Rig</u>	ø Solid Stem Auger, and Triple Tube Coring, B54X Mobil	le Track I	Mour	nted	, L	JTM (m)			E 6	5,524 632,0	70		
(m) NOIL	DEPTH		GRAPHICS	DESCRIPTION AND CLASSIFICATION	PIEZ. LOG	DEPTH (m)	TYPE	<b>ΣΙ</b>	SPT (N) blows/0.15		Cu '	TOR	VANE	-		* •
ELEVATION			GRA		PIEZ	DEP.	SAMPLE TYPE NUMBER	i (1	YNAMIC C N) blows/ft		F	PL 	M		LL -	
	(m)	(ft)					SAI	ايُ	20 40	60	<u>L</u> .	20	<b>%</b>	60	80	
232.4 -	=			CONCRETE  CLAY FILL - Black, frozen, intermediate plasticity, trace fine to	- 23 23						::1:				::1::	1::
- <sup>232,0</sup> -				coarse grained gravel, trace organics, trace silt inclusions.	<b>√88 8</b> 8		S1				1 -					1
	1 = 1			<u>CLAY</u> - Mottled brown to grey, frozen, high plasticity, trace silt inclusions, trace oxidation.	<b>B B</b>				1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -		1:::					1
- 231	=	-5		- Moist, stiff below 1.4 m.	8 8		\$2 S2			4==			•			 
	2 -	-								1		: :: : <del>  </del>		<u> </u> ◆	:: ::	1::
				- Trace gypsum nodules below 2.1 m.			<b>∃</b> S3									::
- 230	=	-			<b>88</b> 88		13			Ţ						1
	3 =	-10								<u> </u>						1::
229	=										::: :  ::: :					1:: 1::
	4-	-					<b>S</b> 4							<u> </u>		: : 
	]													<b>♦</b>  ::		
228		– 15								j						
	5 =				88 88					1						$\Box$
227	🛉						S5 S5				1:1:					 
	6-	- 20			88					1	1::1:	:1::1:			:: ::	1::
	=							::								1::
226		-		- Firm, no gypsum nodules below 6.7 m.		7.0	₽ s6			4			•			
	' ]				N.W.		₹ S6						•			
225	=	- 25			<b>88</b> 88					444						124
	8 =	-		- Grey, trace to some silt inclusions below 7.9 m.						11:11:	1:1:		 	<u>-   -   -  </u>	::1::	1::
224							} S7			4	-   -	: :: :    •::				1::
	<del>[</del>				<b>8</b> 8									<u>:: :: </u>		i::
	Ĭ Į	-30			88 88											
223	1			Tour Such assessment and blood Suc	<b>88</b> 88		13 00				1-1-	 				  ::
222.4	10 =			- Trace fine to coarse grained gravel below 9.8 m.	88 88		₹ S8			1		<u> </u>	<del>-</del>		:: ::	1::
- 222	=			SILT TILL - Grey, moist, loose, some fine to coarse grained gravel.			{} s9									ļ:: 
	111=	35 -					S10 <sub>10</sub>	٥	Ž	4						1::
- 221				- 3.8% gravel, 32.9% sand, 49.8% silt, 13.5% clay at 11.2 m With fine to coarse grained gravel below 11.4 m.	888888888888888888888888888888888888888	11.9	S11					P  :   :				::  :: 
	12	—4∩				12.2			6		+	++		+		<del> </del>
220	=	<b>-</b> -∪ -		- Compact below 12.2 m.		12.3 12.6	S12 <sub>10</sub>	2	8	-   -   -   -   -   -		1 1	44		4-	ļ::-
219.6		-		- SPT sampler bouncing on suspected granite boulder at 12.6 m. - Power auger refusal at 12.7 m. Switched to coring and advanced			S13	::		4						1::
SAM	PLE T	ΥPΙ	E 🔢	Auger Grab Split Spoon Core Barrel												
	TRAC Maple			INSPECTOR rilling Ltd. M. ALFARO			PPROV LM	ED			DAT 8/7/1					



	K	G	S IP		SUMMARY LOG REFERENCE NO.	HOLE I		)				SH	EET	1	of 1
	CLIE	ENT DJECT			F WINNIPEG - WATER AND WASTE DEPARTMENT urn and Calrossie Sewer Relief				JND	ELEV. /C ELE	=V.		-010 <sup>6</sup> 2.29	7-18	}
	SITE				rdon Avenue -			WATE	R EL	EV.					
				Approxi	mately 80 m East of Wilton Street			DATE UTM		LLED			3/201 5,52		2
	DRII MET	LLING THOD	<b>3</b> 1	25 mm	ø Solid Stem Auger B40 Truck Mounted Drill Rig			01111	()				632,		-
	ELEVATION (m)	DEPTH	i	GRAPHICS	DESCRIPTION AND CLASSIFICATION	TYPE	NUMBER RECOVERY %		s/Ó.1	5 m .≜ CONE	Cu	<b>TOR</b>	VANE	60 60	80
	:LEV	-	)	GR,		MPLE	MBE	(N) bl				PL 		—	
	3	(m)	(ft)			SAI		20	40	60	<u> </u>	20	<b>4</b> 0	60	80
	- 232.1 - - 232 231.7		-		CONCRETE  CLAY FILL - Black, frozen, intermediate plasticity, trace fine to coarse grained										1::1::1:: 1::1::1::
	231.7		-		gravel, trace organics, trace silt inclusions.  CLAY - Mottled brown and grey, frozen, high plasticity, trace silt inclusions, trace	_R\$	51								
	- 2 <b>20</b> .19 _	1	-		oxidation.		S2								
	230.8 —		- 5 -		CLAYEY SILT - Light brown, moist, firm, low to intermediate plasticity, trace oxidation, trace silt inclusions.		53						<b>♦</b>   :: ::		1:-1:-1:- <b>.</b> :1::1::
	- 230	2 –	-		<u>CLAY</u> - Mottled brown to grey, moist, firm to stiff, high plasticity, trace silt inclusions, trace oxidation.	13									
		1	-			₹\$	54								
	220	3 -	<del>-</del> 10									:: ::	:: ::		1::1::1::
	- 229	1	-												1::1::1:: 1::1::1::
GPJ		4 =	-		- Trace gypsum pocket (25 mm) at 4.0 m.	₹\$	S5								!::!::!:: <del>!  </del>
07-18.	- 228		- 15							——-				<b>*</b>	1::1::1:: 1::1::1::
11-01		5 -	-												
SSIE -	- 227		-			₹\$	S6								
ALRO	226.2	6 -	=			12						:: ::  :: ::			1::1::1:: 1::1::1::
AND C	- 226 - 226		—20 -	(//////	END OF HOLE AT 6.10 m										
BURN,			-		Notes:  1. Test hole open to 6.10 m below existing grade.										1::1::1:: 1::1::1::
OCKE	- 225	7 -	-		Test hole dry immediately after drilling.     Test hole backfilled with cuttings and bentonite chips with concrete patch.										
OGS/C			- 25		3. Test fole backlined with cuttings and bentonite drips with condete patch.										12121
C13/L	- 224	8 =	-									:: ::	:: ::  :: ::		1::1::1::
- 90\C	- 224		=												
N/GE		9 - ]	- 30									:: ::  :: ::	:::::::!		1::1::1:: 1::1::1::
DESIG	- 223	=	-								-	- -			<del>           </del>
07-18\		10 -	-												1::1::1:: <del>1::1::1::</del>
\11-01	- 222	=	-												التالا!
\$\2011		11 -	— 35 -						3 . II						1::1::1::
JECT	- 221		-												
:\PRC			-												
LOGF	- 220	12 -	<del></del> 40												
-SOIL		=	-												
NICAL	SAM	PLE T	YPE		Auger Grab				p		11	-11	11		111
GEOTECHNICAL-SOIL LOG P:/PROJECTS/2011/11-0107-18/DES/GN/GEO/C6 - C13/LOGS/COCKBURN AND CALROSSIE - 11-0107-18.GPJ	CON	TRAC	TOR		INSPECTOR	APPR	OVE	D			DA				
GEC	M	Maple	≥ Le	eaf Dr	rilling Ltd. M. ALFARO	JRM					8/7/	18			

	K	G	S JP		SUMMARY LOG REFERENCE NO.	HOLE NO. <b>TH18-1</b> 1	1	SHEET 1 of 1
	CLI	ENT JEC			F WINNIPEG - WATER AND WASTE DEPARTMENT urn and Calrossie Sewer Relief		JOB NO. GROUND ELEV. TOP OF PVC ELE	11-0107-18 232.31 V.
	SITE				venue - North Lane		WATER ELEV.	
				Approxi	mately 35 m East of Wilton Street		DATE DRILLED UTM (m)	5/7/2018 N 5,524,534
	DRII MET	HOD	G 1	25 mm	ø Solid Stem Auger B40 Truck Mounted Drill Rig		O TWI (III)	E 632,128
	ELEVATION (m)	i	ב ב	GRAPHICS	DESCRIPTION AND CLASSIFICATION	SAMPLE TYPE NUMBER RECOVERY %	SPT (N) blows/0.15 m  DYNAMIC CONE	Cu POCKET PEN (kPa) ★         Cu TORVANE (kPa) →         20 40 60 80
	:LEV	'	2	GR		APLE MBEF	(N) blows/ft $\triangle$	PL MC LL
	ш	(m)	(ft)			SAN	20 40 60	<b>%</b> 20 40 60 80
Ī	232.1 - - 232 - 232.0		-		CONCRETE   GRANULAR FILL - Tan, moist, compact to dense, trace fine to coarse grained	IF 81		
	232.0	-	-		sand.  CLAY - Mottled brown to grey, frozen, high plasticity, trace oxidation, trace silt	S1		
	- 231	1 –	-		inclusions.	\$2 S2		
	201	-	- 5		- Trace rootlets between 0.3 m and 0.9 m.			
		2 -			- Moist, stiff below 1.8 m.			
ŀ	- 230	-	-			₹ s3		
		3 —	- 10		0			
ŀ	- 229	-	-		- Gypsum pocket (10.2 cm - 15.2 cm diameter) at 3.0 m.			
2		4_				<b>S</b> 4		
-18.GF	- 228	4	-			175		
-0107		=	— 15 L					
IE - 11	- 227	5 -	-		- Trace fine grained gravel at 5.0 m.			
ROSS		-	-			\$5		
D CAL		6 -	-20					
N AN	- 226	-	-					
KBUF		7 —	-			₽ S6		
S/CO	- 225		- 05		- Grey, some silt inclusions below 7.5 m.	₹ S6		
3/LOG		8 —	— 25 -		- Trace fine to coarse grained gravel below 7.8 m.			
6 - C1	- 224		-					
3EO/C			-		- Firm below 8.5 m.	\$7		
SIGN(	223.2 _ - 223	9 —	-30		END OF HOLE AT 9.14 m			
18\DE			-		Notes:			
.0107-	- 222	10 —	-		Test hole open to 9.14 m below existing grade.     Test hole dry immediately after drilling.			
11/11	222	-	_ 35		Test hole backfilled with cuttings and bentonite chips with concrete patch.			
STS/20		11 —	-					
ROJE	- 221	-	-					
3 P:\P		12 —	-					
IL LO	- 220	-	<del>4</del> 0					
AL-SO			_					
CHNIC		PLE '			Auger Grab			
GEOTECHNICAL-SOIL LOG P.\PROJECTS\2011/11-0107-18\DES\GN\GEO\C6 - C13\LOGS\COCKBURN AND CALROSSIE - 11-0107-18.GPJ		TRA( [apl			INSPECTOR rilling Ltd. M. ALFARO	APPROVEI JRM		DATE 8/7/18

	K	GS ROUI	)			HOLE I		2	SH	EET	1 (	of 1
•	CLIE PRO SITE	JECT	C	ockbı	F WINNIPEG - WATER AND WASTE DEPARTMENT urn and Calrossie Sewer Relief			JOB NO. GROUND ELEV. TOP OF PVC ELE	23	-0107 2.21	7-18	
					Avenue - West Lane mately 80 m East of Wilton Street			WATER ELEV. DATE DRILLED	5/′	7/201	8	
	DRII	LLING HOD	_	-	ø Solid Stem Auger B40 Truck Mounted Drill Rig			UTM (m)	Ν	5,524 632,2	,532	2
	ELEVATION (m)	DEРТН		GRAPHICS	DESCRIPTION AND CLASSIFICATION	TYPE	۲۲ %	SPT (N) blows/0.15 m	Cu TOF			(kPa) ★ a) ◆
	ELEVA			GRA		MPLE	NUMBER RECOVERY %	DYNAMIC CONE (N) blows/ft		M• • %	C	LL I
ŀ		(m) (1	τ)	6 Ø p	CONCRETE	3	Z Z	20 40 60	20	40	60	80
ŀ	_ 2 <u>332</u> 0 — 231.7 —	1	X		GRANULAR FILL - Tan, dry to damp, compact to dense, with fine to coarse grained gravel.		51				•	
•	- 231	1-1			<u>CLAY</u> - Mottled brown to grey, moist, stiff, high plasticity, trace silt inclusions, trace oxidation.	₹\$	52				<b>+</b> _	
-	- 230	2-1				₹3°	53				<b>.</b>	
-	- 229	3 - 1	10								•	
0107-18.GPJ	- 228	4-1-	15			<b>₹</b>	54				<b>*</b>	
GEOTECHNICAL-SOIL LOG PAPROJECTS/2011/11-0107-18/DES/GN/GEO/C6 - C13/LOGS/COCKBURN AND CALROSSIE - 11-0107-18.GPJ	- 227	5 - 1				<b>₹</b>	S5				<b>*</b>	
3URN AND CA	- 226	6-1-2	20		- Grey, trace to some silt inclusions, trace fine to coarse grained gravel below 6.2 m.	13	26				<b>*</b>	
3S/COCK	- 225 224.6 _	7	25			<u>}</u>					•	
- C13/LOC	- 224	8-1			END OF HOLE AT 7.62 m  Notes:					 		
N/GEO/C6		9-1	30		Test hole open to 7.62 m below existing grade.     Test hole dry immediately after drilling.     Test hole backfilled with cuttings and bentonite chips with concrete patch.							
-18\DESIG	- 223	+										
11/11-0107	- 222	10	35									
OJECTS/20	- 221	11 - 1										
JG P:\PR	- 220	12 —	10									
IT-SOIL LC		1 1 1										
HNICA	SAM	PLE TY	PE	<u>}</u>	Auger Grab							
GEOTEC		TRACT(		af Dr		APPR JRM	OVE	D	DATE 8/7/18			

	K	GROU	S JP		SUMMARY LOG REFERENCE NO.	HOLE NO. <b>TH18-13</b>	3	SHEET 1 of 1
	CLIE PRO SITE	JEC	т	Cockb	OF WINNIPEG - WATER AND WASTE DEPARTMENT urn and Calrossie Sewer Relief		JOB NO. GROUND ELEV. TOP OF PVC ELE WATER ELEV.	11-0107-18 232.19 V.
	LOC	ATIC	ON A	Approxi	mately 20 m East of Wilton Street		DATE DRILLED	5/7/2018 N 5,524,370
	DRII MET	HOE	G 1	25 mm	ø Solid Stem Auger B40 Truck Mounted Drill Rig		UTM (m)	E 632,183
	ELEVATION (m)	i	ב ב	GRAPHICS	DESCRIPTION AND CLASSIFICATION	SAMPLE TYPE NUMBER RECOVERY %	SPT (N) blows/0.15 m  DYNAMIC CONE (N) blows/ft	Cu POCKET PEN (kPa) ★ Cu TORVANE (kPa) ◆  20 40 60 80  PL MC LL
	ᆸ	(m)	(ft)			SAMF	20 40 60	<b>%</b> 20 40 60 80
-	- 2 <b>222</b> 0 _ 231.8 -	1 —	_		CLAY - Brown, frozen, intermediate plasticity, trace fine to coarse grained gravel, trace organics, trace silt inclusions.  CLAY - Brown, frozen, intermediate to high plasticity, trace silt inclusions, trace rootlets, trace oxidation.  - Mottled brown to grey, moist, stiff, high plasticity below 1.4 m.	\$1 \$2 \$3 \$4		20 40 00 80
-	- 230	2-	- 5 - - -		- wouled brown to grey, moist, suit, high plasticity below 1.4 m.	\$ \$5		
107-18.GPJ	<ul><li>229</li><li>228</li></ul>	4-	- - - - -		- Trace gypsum nodules below 3.7 m.	₹ se		
D CALROSSIE - 11-01	- 227 - 226	5	- - - - - -20		- Firm, no gypsum nodules below 6.1 m.	<b>⅓</b> s7		
OGS/COCKBURN AN	- 225	7-	_ _ _ _ _ 25		- Grey below 6.4 m.	₹ s8		
SIGN/GEO/C6 - C13/L	- 224 - 223	9 —	- - - - 30			₹ S9		
111/11-0107-18\DES	– 222 221.5 _	10	- - - - - 35		END OF HOLE AT 40 67 w			
GEOTECHNICAL-SOIL LOG P./PROJECTS/2011/11-0107-18/DESIGN/GEO/CE - C13/LOGS/COCKBURN AND CALROSSIE - 11-0107-18 GPJ	- 221 - 220	11 —	-40		END OF HOLE AT 10.67 m  Notes:  1. Test hole open to 10.67 m below existing grade.  2. Test hole dry immediately after drilling.  3. Test hole backfilled with cuttings and bentonite chips with concrete patch.			
CHNICA			ГҮРЕ		Auger Grab			
GEOTE			CTOR e Le		INSPECTOR rilling Ltd. M. ALFARO	APPROVEI JRM		DATE 8/7/18

SITE LOCATION DRILLING		urn and Calrossie Sewer Relief			GROUND ELEV. TOP OF PVC ELE		2.65		
		Avenue - South Back Lane			WATER ELEV.				
DRILLING	Approxi	imately 25 m South of Grant Avenue			DATE DRILLED		8/2018 5 524		c
METHOD	125 mm	ø Solid Stem Auger B40 Truck Mounted Drill Rig			UTM (m)	E	5,524 632,3	42	
ELEVATION (m)	GRAPHICS	DESCRIPTION AND CLASSIFICATION	SAMPLE TYPE	NUMBER RECOVERY %	SPT (N) blows/0.15 m A  DYNAMIC CONE (N) blows/ft \( \triangle \)  20 40 60	Cu POC Cu TOF	40 MC %	(kPa	•
232.5		CONCRETE	_			:: :: ::	<u> </u>	:1::1	:: ::
28320		TOPSOIL - Black, frozen, trace fine to coarse grained gravel, trace rootlets, trace oxidation.	1	S1					
1 1		CLAY - Mottled brown to grey, frozen, intermediate to high plasticity, trace organics,		S2			1::1::1:	11:11	11111
231.3		trace rootlets, trace to some silt inclusions.  SILT - Light brown, moist, low to intermediate plasticity, trace oxidation.	_ 12						
231		SILI - Light brown, moist, low to intermediate plasticity, trace oxidation.	3	S3					
230.5		CLAY - Mottled brown to grey, moist, stiff, high plasticity, trace silt inclusions, trace	$\dashv$						
22909		oxidation.	7	S4					
229.6	10	SILT - Light brown, moist, low to intermediate plasticity, trace oxidation.	-73				<u>  : :   : :   :</u>	<u> </u>	•
		<u>CLAY</u> - Mottled brown to grey, moist, stiff, high plasticity, trace silt inclusions.	1	S6			:: :: :  :: :: :	11:11	
229		-						•	
4 = 1		- Trace gypsum nodules between 3.8 m and 5.0 m.					<del>                                     </del>	1	
228	15	- Firm to stiff below 4.3 m.	3	S7			→•		
5							•		
			13	00					
227			13	50				ĦĦ	
6-1-2	20 /////						•		::::::
226							1::1::1:		
7			I	S9			:: :: :		
		- Trace fine to coarse grained gravel below 7.0 m. - Grey below 7.3 m.	<u>₩</u>  }}				 		
225.0	25	END OF HOLE AT 7.62 m							
8 = 1		Notes:					1::1::1:		
224		1. Test hole open to 7.62 m below existing grade.							
9 =		Test hole dry immediately after drilling.     Test hole backfilled with cuttings and bentonite with concrete patch.					<u> :: :: :</u>		
	30								
223							! — — : ! : : ! : : ! :		
10 =						::1::1::	<u> </u>	3133	::::::
=							jiji:	اتات	
222   3	35						<u>                                     </u>		
'' }									
221							1		
12 -	40							+++	
1 4	<del>10</del>							44	
220									
SAMPLE TY	РЕ 🔀	Auger Grab							
CONTRACTO		INSPECTOR rilling Ltd. M. ALFARO	APP	ROVE	D	DATE			

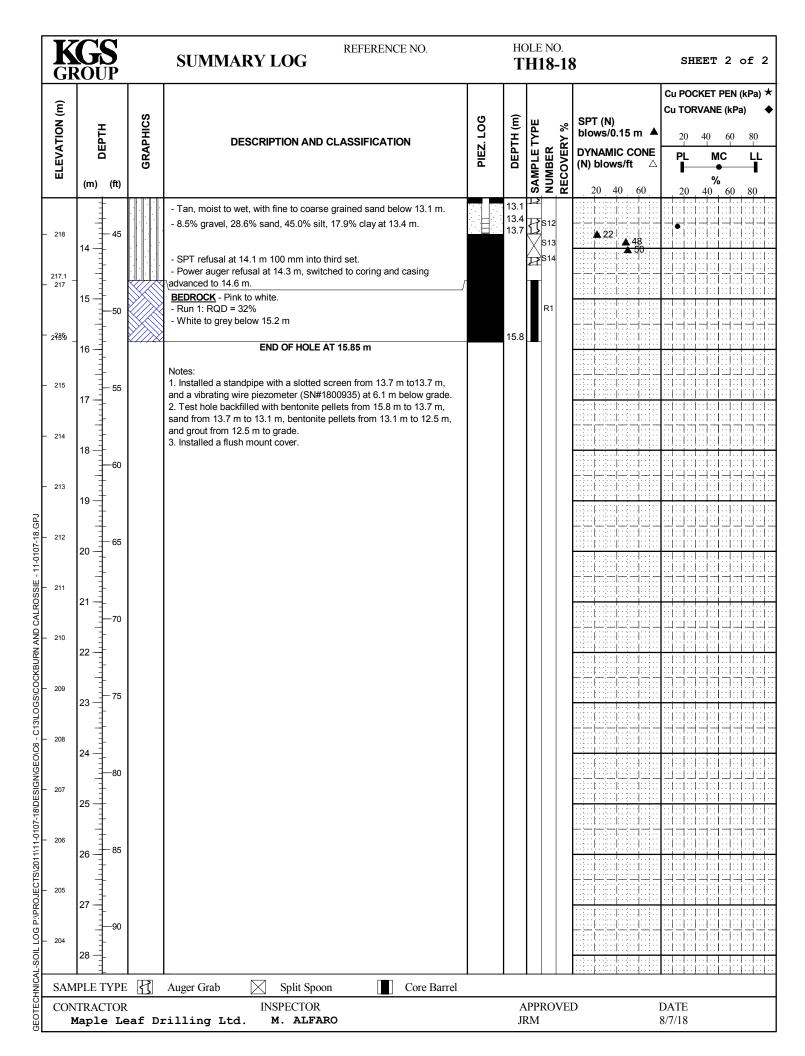
	KG RO			SUMMARY LOG REFERENCE NO.	HOLE TH	E NO. <b>18-1</b> :	5	SHEET 1 of 1
CL	IENT		_	OF WINNIPEG - WATER AND WASTE DEPARTMENT urn and Calrossie Sewer Relief			JOB NO. GROUND ELEV. TOP OF PVC ELE	11-0107-18 232.55 V.
SI.				Avenue - East Lane			WATER ELEV.	
LO	CAT	ON	Approxi	imately 40 m West of Harrow Street			DATE DRILLED	5/8/2018
	ETHO		125 mm	ø Solid Stem Auger B40 Truck Mounted Drill Rig			UTM (m)	N 5,524,681 E 632,397
ELEVATION (m)	(m	) (ft)	GRAPHICS	DESCRIPTION AND CLASSIFICATION	AMPLE TYPE	NUMBER RECOVERY %	SPT (N) blows/0.15 m   DYNAMIC CONE (N) blows/ft	Cu POCKET PEN (kPa)   Cu TORVANE (kPa)  20 40 60 80  PL MC LL  %
222.4	+	<del>/ (</del>	e 4 4 e	CONCRETE	၂ဖ	<b>Z</b> &	20 40 60	20 40 60 80
232.4 232.3		<u>}</u>		ASPHALT				
- 232.3 - 232 231.8	-	‡		CLAY FILL - Black, moist, soft, trace fine to coarse grained gravel.				
	1 -	1	$\mathcal{U}\mathcal{U}$	<u>CLAYEY SILT</u> - Light brown, frozen, low to intermediate plasticity, trace oxidation.	<u>}</u>	S2		
231.0 - 231	-	1 5		- Moist below 1.2 m.	_			
		}		<u>CLAY</u> - Mottled brown to grey, moist, firm to stiff, high plasticity, trace silt inclusions, trace oxidation.				
	2 -	‡		- 50 mm silt pocket at 2.0 m.				
- 230		}			$\square$	S3		
		‡						
	3 -	<del>]</del> —10						
- 229		-						
2	1,	1			F	S4		
CALROSSIE - 11-0107-18.GPJ 	4 -	1			17	-		
228		1,	. <i>//////</i>					
1-01	_	‡ ``						
Т. -	5 -	7						
ISS _ 227		}			<b>P</b>	S5		
ALR		‡						
	6-	-20		- Grey, firm below 6.1 m.				
Z - 226		}						
BUR	_	‡				86		
Š	7 -	]		- Stiff below 7.0 m.	11	S6		
O/S - 225		<u></u>	. //////					
JLO0	8-	1 ~		Fire two for to reason wind and below 70 as				
C13	0 -	]		- Firm, trace fine to coarse grained gravel below 7.9 m.				
9 – 224		‡			<b>3</b>	S7		
GEC	9-	}						
223.4	1	= 30		END OF HOLE AT 9.14 m	$\dashv$			
223		}		Notes:				
7-18	10 -	₫		1. Test hole open to 9.14 m below existing grade.				
1-010		1		2. Test hole dry immediately after drilling.				
= 222			5	Test hole backfilled with cuttings and bentonite chips with concrete patch.				
S/20.	11 -	‡ ``						
ECT		}						
Q - 221		‡						
P.'F	12 -	}						
LOG		1-40	)					
- 220 OS		Ī						
GEOTECHNICAL-SOIL LOG P:\PROJECTS\2011\1-0107-18\DESIGN\GEO\CO\CKBURN AN		Ŧ						
Ĭ SA	MPLE	TYP	E 🔢	Auger Grab				
E CO	NTRA			INSPECTOR		ROVE		DATE
GEC	Map.	le I	Leaf D	rilling Ltd. M. ALFARO	JRM			8/7/18

SITE	JECT E ATION	Cockb Sparling Approxi	SUMMARY LOG  PF WINNIPEG - WATER AND WASTE DEPARTMI urn and Calrossie Sewer Relief g Avenue - East Lane mately 25 m West of Harrow Street			[18-1	JOB NO. GROUND ELEV. TOP OF PVC ELE WATER ELEV. DATE DRILLED UTM (m)	11-0107-18 231.98 V. 4/30/2018 N 5,524,172
ELEVATION (m) TAN	HLLANG (m) (ff	Rig GRAPHICS	ø Solid Stem Auger, and Triple Tube Coring B54X Mobile  DESCRIPTION AND CLASSIFICATION	FEZ LOG		SAMPLE LYPE NUMBER RECOVERY %		E 632,682  Cu POCKET PEN (kPa) *  Cu TORVANE (kPa) *  20 40 60 80  PL MC LL  % 20 40 60 80
231.8 -	1 - 1 - 5		CONCRETE CLAY - Grey, frozen, high plasticity, trace silt inclusions.  - Mottled brown to grey, moist, stiff, trace oxidation below 1.5 m.		<u> </u>	<b>3</b> S1		
230	2 - 1 - 1 - 1 3 - 1 - 1	0			1	<b>3</b> S2		
228	4 1 1 1 5 1	5			1	<b>3</b> S3		
226	6-1-2	0	- Grey below 5.2 m Firm below 6.4 m.			<b>3</b> S4		
225	7	5	- FIITH DELOW 0.4 III.	8888888	7.6 7.8	<b>3</b> S5		
223	9-1-3	0			1	<b>3</b> S6		
	10	5	- Soft below 9.8 m.		}	<b>3</b> S7		
220.2 _	11	0	SILT TILL - Grey, moist, loose, non to low plasticity.	88888888888888888888888888888888888888	<u>}</u>	\$8 \$9 \$10	<b>1</b> 510	
219	1		- SPT refusal at 12.4 m, on suspected cobble.					
CON	PLE TYI TRACTO	OR OR	Auger Grab Split Spoon Core Barrel INSPECTOR cilling Ltd. M. ALFARO		AP JRN	PROVI		DATE 8/7/18

(E) Z	SS		)G	(m)	»E	SPT (N)	Cu TOR	KET PEN VANE (kPa	
ELEVATION (m)	GRAPHICS	DESCRIPTION AND CLASSIFICATION	PIEZ. LOG	DEPTH (m)	SAMPLE TYPE NUMBER RECOVERY %	blows/0.15 m ▲ DYNAMIC CONE (N) blows/ft △	20 PL	## 60 ## MC	LI
217	5 0 0 5 5 0 0 0 5 5	- Boulders and cobbles between 12.5 and 13.4 m Tan below 13.0 m 12.6% gravel, 28.0% sand, 42.9% silt, 16.5% clay at 13.1 m Power auger refusal at 13.4 m, switched to coring.  BEDROCK - Pink to white, highly fractured Run 1: Boulder and 50 mm of bedrock, RQD = 0% Run 2: RQD = 0%, 150 mm of bedrock Rubble at 15.1 m Run 3: RQD = 12%  END OF HOLE AT 16.15 m  Notes: 1. Installed a standpipe with a slotted screen from 16.2 m to 15.8 m, and a vibrating wire piezometer (SN#1800937) 7.6 m below grade. 2. Test hole backfilled with sand from 15.8 m to 15.5 m, bentonite pellets from 15.5 m to 14.9 m, and grout from 14.9 m to grade. 3. Installed a flush mount cover.		14.9 15.5 15.8 16.2	R1 R2 R3			40 60	80

	K	G	S JP		SUMMARY LOG REFERENCE NO.	HOLE TH1		7	SH	EET	1 o	of 1
•	CLIE	JEC	т (	Cockb	OF WINNIPEG - WATER AND WASTE DEPARTMENT urn and Calrossie Sewer Relief			JOB NO. GROUND ELEV. TOP OF PVC ELE	23	-0107 1.96	-18	
	SITE			-	venue - West Lane			WATER ELEV.	<i>= 1</i> 2	3/2011	0	
				Approxi	mately 50 m East of Stafford Street			DATE DRILLED UTM (m)		2/2018 5,524		)
	DRII MET	HOE	G 1	25 mm	ø Solid Stem Auger B54X Mobile Track Mounted Drill Rig			· · · · · · · · · · · · · · · · · · ·		632,6		
	ELEVATION (m)		ב ב	GRAPHICS	DESCRIPTION AND CLASSIFICATION	E TYPE	NUMBER RECOVERY %	SPT (N) blows/0.15 m  DYNAMIC CONE	Cu POC Cu TOF	RVANE	(kPa)	
	ELE		- (ft)	9		SAMPL	NUMBE RECOV	(N) blows/ft △ 20 40 60	20	%		80
ľ	231.9			9 4 9	ASPHALT		T		::[::[::			
	231.7 231.3	-			CONCRETE CLAY FILL - Grey to brown, moist, firm to stiff, high plasticity.	<b>—Д</b>	24					
	- 2 <del>8</del> 8.19	1 _	-		SILT - Tan, moist, soft, low plasticity, trace to some clay, trace fine grained gravel.	<b>-</b> ∕[ <u>[</u> ]	51			<u> </u>		::1::1::
		' :	-		CLAY - Mottled brown to grey, frozen, high plasticity, trace silt inclusions, trace	<b>一</b>	S2			-		
		-	-5		organics, trace oxidation Increased silt inclusions between 1.4m and 1.5 m.		S3	HHHHHH		ıHH:		445
ŀ	- 230	2 —	-		- Moist, stiff, no organics below 1.5 m.							
			-			D.	84					
		-	Ĺ				34					
ŀ	- 229	3 —									111	
			"							(111111) 		
		-	-								•	
Ğ.	- 228	4 -	-			<u>}</u>	S5			100   100   10 	::::::::::::::::::::::::::::::::::::::	::::::::::::::::::::::::::::::::::::::
-18.6			-		- Firm to stiff below 14.3 m.					:: ::	4:4:	
0107		-	<del>-</del> 15									
-11-	- 227	5 -	-							• •	11:11:	
SSIE		-				<u>}</u>	S6					
LROS		-				12				:: :: <b>T</b> :		
CA	- 226	6 –	-20							<del>-   -   -   -   -   -   -   -   -   -  </del>	1	
AN		_	-									
3UR			-			<u>}</u>	S7					
ÖKE	- 225	7 —	-		- Grey, firm, no oxidation below 7.0 m.						++	
S/C	224.3	-				<u> </u>	S8			<b>₩</b> 1.		444
LOG	- 224	]	25		END OF HOLE AT 7.62 m					-		
.C13	227	8 –	-		Notes:							
9)(0		-	-		Test hole open to 7.32 m below existing grade.     Test hole dry immediately after drilling.							333
GEC	- 223	9 —	-		Test hole dry infinediately after drilling.     Test hole backfilled with cuttings and bentonite chip with concrete patch.							
NBIGN			-30									
\DES		-	-							- - -		
7-18	- 222	10 —								<u> </u>	44	
1-010			-									
11/1		-	— 35							idd:		HH:
rs\20	- 221	11 –	-									
JEC.			-									
PRO		-	-									
G P:	- 220	12 —	_10							<del>         </del>		<del>-   -   -</del>
LLO		]	40							,::::::   4	11111 1111	:::::: 
SO!		:	-									
ICAL	- 219 SAM	DIE'	LADE	<u></u>	Auger Grab			1 - 1 - 5 - 1	<u> </u>	11.		
NH.					-	A DDD		<u> </u>	DATE	—	—	
GEOTECHNICAL-SOIL LOG P.NPROJECTS/2011/11-0107-18/DES/GN/GEO/C6 - C13/LOGS/COCKBURN AND CALROSSIE - 11-0107-18.GPJ	CON M				INSPECTOR rilling Ltd. M. ALFARO	APPR JRM	OVE		DATE 8/7/18			

SITI LOC DRII	JEC1	T ( ) ON / G 1	Cockb Weather	OF WINNIPEG - WATER AND WASTE DEPARTM orn and Calrossie Sewer Relief rdon Avenue - West Lane mately 25 m East of Wentworth Street Ø Solid Stem Auger, and Triple Tube Coring B54X Mob		Mour	nted Drill	JOB NO. GROUND ELEV TOP OF PVC EL WATER ELEV. DATE DRILLED UTM (m)	5/1/2018 N 5,524,94 E 632,705	15
ELEVATION (m)	Э	i i (ft)	GRAPHICS	DESCRIPTION AND CLASSIFICATION	PIEZ. LOG	DEPTH (m)	SAMPLE TYPE NUMBER RECOVERY %	SPT (N) blows/0.15 m A DYNAMIC CONE (N) blows/ft A	PL MC	
231.7 _ 231.5 _ 231 _ 230.2	1-	- - -		CONCRETE  GRANULAR FILL - Moist to wet, fine to coarse grained gravel, some sand.  CLAY FILL - Grey, frozen, high plasticity, trace silt inclusions.			\$1 } \$2			
230	2-1	5   		\ - Mottled brown to grey, moist, stiff, trace organics below 1.5 m.  CLAY - Mottled brown to grey, moist, stiff, high plasticity, trace silt inclusions.			<b>∏</b> s₃			
228	4	—10 - - -		- Grey below 4.0 m. - Firm below 4.3 m.	\$3333333 \$3333333 \$3333333		<b></b>			
227	5	- 15 - - -			88888888	6.1	\$55			
225	7	20 - - - -			N.W.	162	<b>₹</b> 36			
224	8 - 1	25 - - - -				12.5	<b></b>			
222	10 —	30 - - - -		- Soft below 10.4 m.	53333333 533333333 533333333		<b>₹</b> 58			
221	11 -	- 35 - - -			8888888		<b>₹</b> 59			1::1::1: 1::1::1: 1::1::1: 1::1::1: 1::1::1:
219.7 _	12 -	40 - -		SILT TILL - Grey, moist, loose, some to with fine to coarse grained sand, trace to some fine to coarse grained gravel SPT sampler sunk under SPT rod's weight at 12.2 m.		12.5	S10	<b>2</b> 0		<del>1  .</del>  :  .  :  .



	K	G	S JP		SUMMARY LOG REFERENCE NO.	HOLE NO. <b>TH18-1</b> 9	)	SHEET 1 of 1
	CLIE	JEC	т (	Cockb	OF WINNIPEG - WATER AND WASTE DEPARTMENT urn and Calrossie Sewer Relief		JOB NO. GROUND ELEV. TOP OF PVC ELE	11-0107-18 231.93
	SITE				rdon Avenue - West Lane		WATER ELEV.	5/2/2019
			_		mately 25 m East of Lilac Street		DATE DRILLED UTM (m)	5/2/2018 N 5,525,048
	DRII MET			25 mm	ø Solid Stem Auger B54X Mobile Track Mounted Drill Rig		. ,	E 632,891
	ELEVATION (m)		UEV II	GRAPHICS	DESCRIPTION AND CLASSIFICATION	YPE	SPT (N) blows/0.15 m	Cu POCKET PEN (kPa) ★ Cu TORVANE (kPa) ◆  20 40 60 80
	LEVA.		2	GRAF	DECOME HOWARD GEAGGII IOATION	SAMPLE TYPE NUMBER RECOVERY %	$\begin{array}{ll} \textbf{DYNAMIC CONE} \\ \textbf{(N) blows/ft} & \triangle \end{array}$	PL MC LL
	ш	(m)	(ft)			SAN	20 40 60	<b>%</b> 20 40 60 80
	231.8		-	D & 4 D	CONCRETE SILT - Light brown, frozen, low plasticity, trace to some clay, trace oxidation.			
	231.3	-	-		CLAY - Mottled brown and grey, frozen, high plasticity, trace silt inclusions, trace	1)		
	231	1 -	_ 5		oxidation.	\$2 S2		
ŀ	230	2 -	-		- Moist, stiff below 1.8 m.			
		-	-			<b>₹</b> 3		
F	229	3 —				S4		
		-	-					
교-	228	4 -			- Firm below 3.7 m.	S5		
7-18.G			1					
11-010	227	5 –	15					
SIE - 1		5 -	-			₽ s6		
ALROS	226					₹ S6		
ND C	220	6-	20					
URN		-			- Grey, no oxidation below 6.7 m.			
OCKB	225	7 –						
068/0	224.3 _		25		END OF HOLE AT 7.62 m	\$7 S7		
C13/L	224	8 –	-		Notes:			
0\C6		-	-		Test hole open to 7.46 m below existing grade.     Test hole dry immediately after drilling.			
3N/GE	223	9 -	- -30		Test hole backfilled with cuttings and bentonite chip with concrete patch.			
NDESIG			-					
107-18	222	10 —						
1/11-0		-	- 35					
TS\201	221	11 —	- 33					
OJEC		-	-					
P:\PR	220	12 —						
IL LOG			<del>-</del> 40					
AL-SO	219							
CHNIC,			ГҮРЕ		Auger Grab			
GEOTECHNICAL-SOIL LOG P./PROJECTS/2011/11-0107-18/DES/GN/GEO/C6 - C13/LOGS/COCKBURN AND CALROSSIE - 11-0107-18.GPJ			CTOR e Le		INSPECTOR rilling Ltd. M. ALFARO	APPROVE JRM		DATE 8/7/18

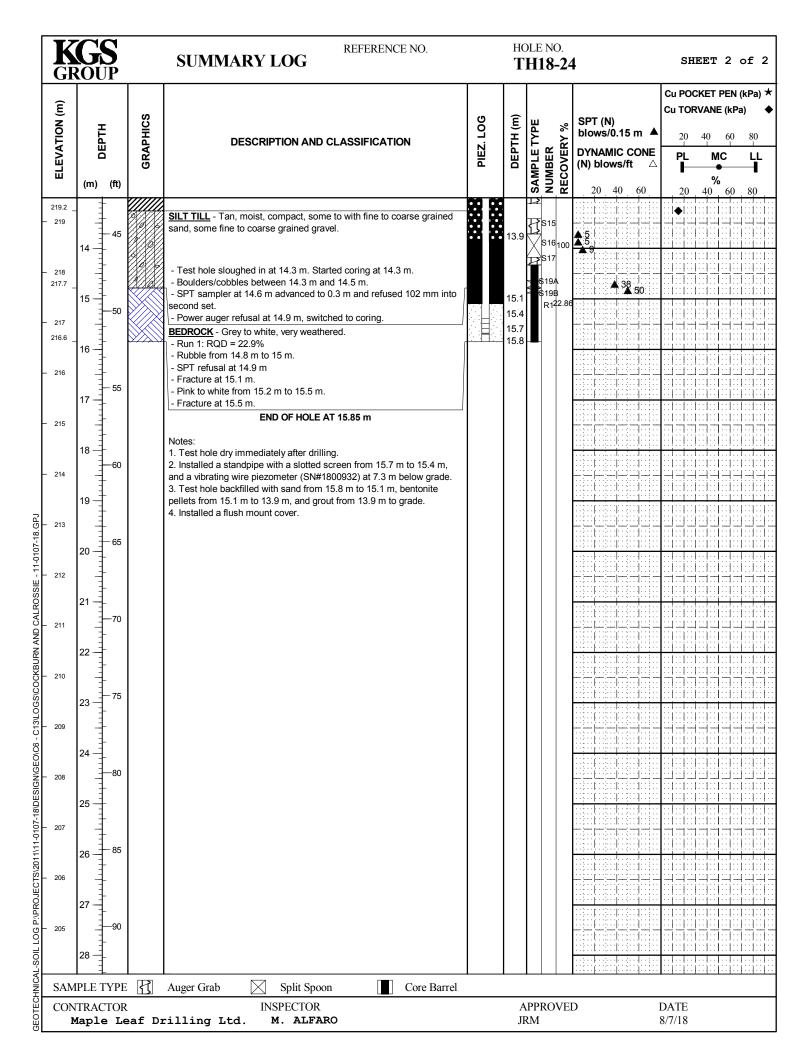
	K	G	S JP		~	HOLE TH1		)	SH	EET	1 (	of 1
	CLII	ENT JEC			OF WINNIPEG - WATER AND WASTE DEPARTMENT urn and Calrossie Sewer Relief			JOB NO. GROUND ELEV. TOP OF PVC ELE	23	-0107 1.63	<b>7-18</b>	
	SITI	=	H	lector A	Avenue - West Lane			WATER ELEV.	٧.			
	LOC	ATIC	ON A	Approxi	mately 25 m East of Wentworth Street			DATE DRILLED		2/201		•
	DRII MET	HOE	G 1	25 mm	ø Solid Stem Auger B54X Mobile Track Mounted Drill Rig			UTM (m)	E	5,524 632,7	48	
	ELEVATION (m)	ļ	<u> </u>	HICS	DESCRIPTION AND OF A COLETO ATTION	YPE	%,	SPT (N) blows/0.15 m 🔺	Cu POC Cu TOF		-	
	LEVAT	ן נ <u>י</u>	ב ב	GRAPHICS	DESCRIPTION AND CLASSIFICATION	APLE T	NUMBER RECOVERY %	DYNAMIC CONE (N) blows/ft	PL	MC		LL I
	ш	(m)	(ft)			SAN	NEG NEG	20 40 60	20	<b>%</b>	60	80
-	231.4 _	-	_		CONCRETE  CLAY - Mottled grey to brown, frozen, high plasticity, trace silt inclusions, trace oxidation.							
	. 2 <u>3</u> 9 <sub>0</sub> 0	1 -	- 5		- Moist, firm below 1.2 m. - Brown below 1.5 m.	12						
	229.8	2 —	-		CLAYEY SILT - Light brown, moist, firm, trace oxidation.		52			· •	.:1::1 <del>-   • </del>	
	- 229		-		CLAY - Mottled brown to grey, moist, stiff, high plasticity, trace silt inclusions, trace oxidation below 1.8 m.	<b>₽</b> °	33					
		3 —	—10 -						::1::1::	-   : :   : :   :   : :   : :		   : :   : :   : :   : :   : :   : :
2	- 228	4 -	-			<u></u>	S4				•	
77-18.G	- 227		- 15								<b>*</b>	:: :: ::    -
≣ - 11-01(	- 221	5	-		- Firm below 4.9 m.	<b>₹</b>	65					
ALROSSII	- 226		-		- No oxidation below 5.5 m.	<b>₽</b> °	86					
N AND C	005	6 -	-20									
CKBUR	- 225	7 -	-			<u>₹</u>	S7			•		
LOGS/C	- 224		25									
C6 - C13	- 223	8 –	-				58					
3N/GEO	223	9 –	_ 30									
-18\DESI	- 222		-								 	
11-0107		10 —	-			<b>!</b>	59		•			
3/2011/	. 2 <u>321</u> 40 _	11 —	35	<i>///////</i>	END OF HOLE AT 10.67 m	$\dashv$						
OJECTS	220	''			Notes:  1. Test hole open to 2.44 m below existing grade.							
G P:\PR	- 220	12 —			Test hole dry immediately after drilling.     Test hole backfilled with cuttings and bentonite chips with concrete patch.							
-SOIL LO	- 219	-	40 									
INICAL	SAM	PLE	і ГҮРЕ		Auger Grab			1	1	1		
GEOTECHNICAL-SOIL LOG P.;PROJECTS/2011/11-0107-18/DES/GN/GEO/C6 - C13/LOGS/COCKBURN AND CALROSSIE - 11-0107-18.GPJ	CON	TRA	CTOR		INSPECTOR cilling Ltd. M. ALFARO	APPR JRM	OVE		DATE 8/7/18			

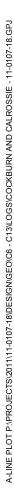
	K	GROU	S JP			HOLE TH1		1				SHI	EET	1	of	1
	CLII	ENT JEC		_	OF WINNIPEG - WATER AND WASTE DEPARTMENT urn and Calrossie Sewer Relief				UND I	ELEV. /C ELE	V.		-010′ 1.75			
	SITI				reet - South Lane				ER EL			<i>5 1</i> 0	. /2.0.1	0		
			_		mately 25 m East of Ebby Avenue			UTM	E DRIL I (m)	LED			2/201 5,52		8	
		HOD		25 mm	ø Solid Stem Auger B54X Mobile Track Mounted Drill Rig							Ε (	632,9	946		
	ELEVATION (m)		<u> </u>	HICS		YPE	%	SPT blow		5 m ▲			KET I			*
	EVAT	ן נ	7	GRAPHICS	DESCRIPTION AND CLASSIFICATION	LE T	NUMBER RECOVERY %	DYN.	AMIC			PL	M		Ļ	_
		(m)	(ft)			AMP	IUME ECO	(14) 5				20	%			
ŀ	231.7				ASPHALT	<b>1</b> 22		20	) 40	60	::1:	20	40	60	80	1::
	231.5 - - 231.2	-			\GRANULAR FILL - Tan, moist, compact to dense. \SILT - Grey, frozen, low plasticity, trace oxidation.	-\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\								•		
	201	1 -	-		<u>CLAY</u> - Mottled brown to grey, frozen, high plasticity, trace silt inclusions, trace fine to coarse grained gravel.						::1:	11:11		::1::		1::
		-	_ _ 5		- Brown, moist, stiff, trace oxidation below 1.5 m.	3	S3								) 	1:4
ŀ	- 2 <b>29</b> 09 _	2 —	-		SILT - Light brown, moist, soft, trace oxidation.		84				::: :	<u> </u>	:: :: <u> </u>	:: :: 		1::
			-		CLAY - Mottled brown and grey, moist, stiff, high plasticity, trace silt inclusions, trace oxidation.											
-	- 229	3 —	_ 10			3	33				::1:					1::
		-	-													i:: 1::
J. J.	- 228	4 —	-			<u>}</u>	S6					11:1		***		1::
D CALROSSIE - 11-0107-18.GPJ					- Firm to stiff below 4.3 m.									)		
1-010	- 227		— 15 -													ļ::
SIE - 1		5 —	-			13	67									1::
LROS	- 226	-			- No oxidation below 5.5 m.	1	37									ļ::
ND CA		6 -	-20		- Grey below 5.8 m.											Ī::
JRN A	- 225											## !!!!				<del>1</del>
OCKBL		7 –				<u> </u>	S8									1::
GS/CC	224.1	-	- 25		END OF HOLE AT TOO	4				444						
13/LO	- 224	8 -	-		END OF HOLE AT 7.62 m							11				1::
C6 - C		-			Notes:  1. Test hole open to 7.32 m below existing grade.											ļ:: 1::
/GEO/	- 223	9 —	-		Test hole dry immediately after drilling.     Test hole backfilled with cuttings and bentonite chips with concrete patch.						::: :					<u> ::</u>
SIGN			—30 –													
-18\DE	- 222	100	-													ļ::  :::
1-0107		10 —														
2011/1	- 221	=	35													1::
:CTS/		11 -	-													Ti
PROJE	- 220	-	-													1::
JG P:\		12 -	40											::::::		1::
OIL LC	- 219	=	-							4-1-						1::
GEOTECHNICAL-SOIL LOG P.\PROJECTS\2011\11-0107-18\DESIGN\GEO\C6 - C13\LOGS\COCKBURN AN		DI 5	EVE		Avenu Crob						<u> :: :</u>	<u>::::</u>	<u>:: :: </u>	<u>:: ::</u>		<u> </u> :::
ECHN		TRAC			Auger Grab  INSPECTOR	АРРІ	ROVE	D			DA	ΓE				
GEOT					rilling Ltd. M. ALFARO	JRM	-5 12	-			8/7/					

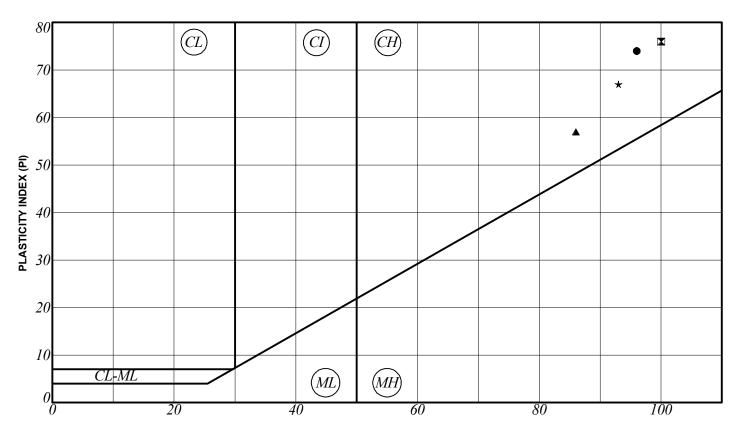
	K	G	S JP			HOLE <b>TH</b>	E NO. 1 <b>8-2</b> 2	2					SHE	ΈT	1 (	of 1	
	CLII PRO	ENT JEC			F WINNIPEG - WATER AND WASTE DEPARTMENT urn and Calrossie Sewer Relief			GRO	NO. DUNE OF F				11-( 231	0107 .97	7-18		
	SITE				Street - West Lane				TER E								
	LOC	ATIC	) N	Approxi	mately 40 m East of Stafford Street				ΓE DR /I (m)	RILLE	D			/201 5,524		5	
	DRII MET	HOD	G 1	125 mm	ø Solid Stem Auger B54X Mobile Track Mounted Drill Rig				// (III)			E	E 6	32,5	87		
	ELEVATION (m)	111111111111111111111111111111111111111		GRAPHICS	DESCRIPTION AND CLASSIFICATION	E TYPE	NUMBER RECOVERY %	SPT blow	「(N) ws/0.′	со		Cu T	20 20	KET F VANE  40 M	60 60		
		(m)	(ft)	ច		AMPL	IUMBI ECOV	(N) I	blows		Δ			<b>%</b>		<b>—I</b>	
<u> </u>	231.8	` ′		p 4 4 p	<u>CONCRETE</u>	\sqrt{s}	<b>~</b> ~	2	0 40	) 6	0	2	20 	40	60	80	
	231.4	]	_		GRANULAR FILL - Tan, moist, compact to dense, with clay.	_ 	S1							44			
-	231	1 —			<u>SILT</u> - Light brown, frozen, low to intermediate plasticity, trace oxidation.		S2						: :   :   : :   :   : -   :				
2	230.6 _	-	- 5		CLAY - Mottled brown to grey, frozen, high plasticity, trace silt inclusions, trace	- 13	S3										
-	230	2 —			oxidation.								1::1: 1::1:				
		-	_		- Moist, stiff below 2.1 m.	1	S4						:: :  :: :				
-	229	3 -	10 														
77-18.GPJ	228	4-	- - 15		- Firm below 4.3 m.	1	S5						-   -   -   -		<b>Y</b> ◆		
D CALROSSIE - 11-0107-18.GPJ	227	5 -	-			33	S6										
AND CALRO	226	6	- 20 -		Overhalm 2.4 m	1	S7						:: :  :: :  -: :  :: :				
SOCKBURN	225	7-	-		- Grey below 6.4 m.	<u> </u>	S8							•			
\S90	224.4	=	<b>— 25</b>		END OF HOLE AT 7.62 m	+			: -  ::: - -				-   -				
GEOTECHNICAL-SOIL LOG P./PROJECTS/2011/11-0107-18/DESIGN/GEO/C8 - C13/LOGS/COCKBURN AN	224	8 -	-		Notes: 1. Test hole open to 7.46 m below existing grade. 2. Test hole dry immediately after drilling.								-   -   -   -				
8\DESIGN\G	223	9 -	<del></del> 30 - -		Test hole backfilled with cuttings and bentonite chips with concrete patch.												
11/11-0107-1	222	10 -	- - 35														
ROJECTS/20	221	11 -	_ - -														
IL LOG P:\P	220	12 —	- 40 -														
AL-SO	210					$\perp$											
TNICA	SAM	PLE T	ГҮРЕ		Auger Grab												
GEOTEC!		TRA(			INSPECTOR rilling Ltd. M. ALFARO	APP JRM	ROVE	D				DAT1 8/7/1					

	K R	G			SUMMARY LOG		HOLE <b>TH</b> 1	E NO. <b>18-2</b>	3					SH	EET	1	of	1
CI	LIE RO.	NT JEC	r (	Cockb	F WINNIPEG - WATER AND WASTE urn and Calrossie Sewer Relief	DEPARTMENT			G T(	OP OI	ND E F PV	ELEV.			-010 1.80		8	
	ITE OC				reet - West Lane mately 15 m West of Pembina Highway					/ATEI ATE I				5/2	8/20	18		
DI	RIL	LING	G 1		ø Solid Stem Auger B40 Truck Mounted Dr	III Rig				TM (r				Ν	5,52 633,	5,03		
ELEVATION (m)		Ę	<u> </u>	нісѕ			YPE	%	S	PT (N lows/	l) (0.15	sm ⊿	Cı		CKET RVAN 40		(kPa) Pa)	•
ELEVAT		(m)		GRAPHICS	DESCRIPTION AND CLASSIFICA	HON	AMPLET	NUMBER RECOVERY %	D (N	l) blo	ws/f			PL 	N 9	IC	LL I	
231.	6	· ,	.,	P 4 9 P	CONCRETE		s □		::}	20	40	60	: :::	20	40	60	80	:1::
231.	з 🗌	4	-		CLAY FILL - Black, frozen, intermediate plasticity, tracking avel, trace organics, trace silt inclusions.	ce fine to coarse grained	R											
231. - 231	ĭd	1 -	-		CLAYEY SILT - Tan to light brown, frozen, low to inte	mediate plasticity, trace to		S3								liili		
		=	-		some clay.  CLAY - Mottled brown to grey, frozen, high plasticity.													
- 230		3	5 -		- Moist, stiff, trace silt inclusions, trace oxidation belo	w 1.5 m.												
		2 —	-										: ::		:   : :	•		1
		=	-				3	54										
- 229 228.		3 -	<del></del> 10		END OF HOLE AT 3.04	m	4					: :  : : <u>:</u>			:: :: <u> </u>  :: ::		11:11:	11:
		4	-						1							 		
_ 228	в	4	-		Notes: 1. Drilling hit an abandoned water line at approximate								: ::					
-18.G		. 1	-		<ol> <li>Water observed to be flowing out of the test hole do</li> <li>Test hole was abandoned for pipe repair.</li> </ol>	ie to the damaged water line.												
610 - 227	,	1	— 15 -						1.1									1:
H- 1		5	-										: ::		1::1::	1::1:		
SOSSI		=	-						- 3									
226	5	6	- 20										: :::	:: :: 	:: :: 	1::1:   -	11111	: 1 : : - 1 - :
AND		4	-												:: ::   -			:   : : -  : :
AND - 225	5	7	-															
Š O O		´ ‡	-															
\(\sigma \) = 224	4	1	- 25															
C13/I		8-	-												1::1::	1::1:		
-9)Ce		=	-						1									
N/GE/	3	9-	<del>-</del> 30							iitiis iiliis					:: :: 	:: :   .		:1::
ESIG		4	-						1						:: ::   -	:: :   -	-   -   -   -   -   -	
18 - 222		10	-															
1-010		" ‡	-															
E 221	,	1	<del>- 35</del>															<u> </u>
CTS		11 -	-												<u>                                     </u>			Ė
PROJE		-	-									4==						##
4 – 220 6 9		12 -	- 40													: :   :     .		1
		=	<del>-1</del> 0												   -   -		 	4:
OS- 219	9	-	-															::::
SA		PLE T			Auger Grab													
GEOTECHNICAL-SOIL LOG P:/PROJECTS/2011/11-0107-18/DES/GN/GEO/C6 - C13/LOGS/COCKBURN AND CALROSSIE - 11-0107-18.05 Page 252		TRAC <b>apl</b> e			INSPECTOR m. ALFARO		APP: JRM	ROVE	D				DA 8/7	TE 7/18				

	JECT	• (	Cockb	F WINNIPEG - WATER AND WASTE DEPARTME urn and Calrossie Sewer Relief	ENT			8-2	JOB GRO		ELEV. VC ELE	2	11-01 232.4	107-	18	2
SITE				venue and Pembina Highway						TER E		,	= 10.12	010		
			Southbo	ound Pembina to Grant Yield Island						E DRI (l (m)	LLED		5/9/2 N 5,5		257	
DRIL MET	LING HOD	r	Portable CME 75	Concrete Core Drill; 125 mm ø Solid Stem Auger, and Tr Truck Mounted Drill Rig	iple Tub	e Co	orin	g		()			63.			
ELEVATION (m)	DEPTH		GRAPHICS	DESCRIPTION AND CLASSIFICATION	PIEZ. LOG	DEPTH (m)	MPLE TYPE	NUMBER RECOVERY %	SPT blow DYN (N) I		5 m ▲ CONE /ft △	Cu T	<b>ORVA</b>	MC		· •
	(m)	(ft)					SA	N N	. 2	0 40	60	2	0 40	<b>%</b> 0 6	0 80	)
232.2 _ 232	1-1			<u>TOPSOIL</u> - Black, moist, firm, trace to some rootlets. <u>CLAYEY SILT</u> - Light brown, moist, firm, low to intermediate plasticity, trace rootlets, trace oxidation, trace fine to coarse grained gravel	888888		₹ ₹									
231	2-1	- 5		CLAY - Mottled brown to grey, frozen, high plasticity, trace rootlets, trace oxidation, trace silt inclusions.  - Moist, stiff below 1.8 m.  - Some to with silt between 1.8 m to 2.0 m.	888888		₹ ₹	S4						•		
230	3-1	-10		- Brown, no rootlets below 3.4 m.	88888		<u>}</u>	S5						•   •	<b>&gt;</b>	
228	4-1	- 15					蠺	S6							) 	
227	5			- Grey, firm, trace fine to coarse grained gravel, no oxidation below 5.6	28888		<u>}</u>									
226	6	-20		m Brown, trace oxidation, no gravel below 6.1 m.	888888	1	岱							—————————————————————————————————————		
225	8-	- 25		- Grey, trace fine to coarse grained gravel below 7.3 m Soft below 7.9 m.	_ \_M_	175	<u>{</u>						•	<b>X</b>		
224	9 -	-30			888888		蠺	S11					<b>*</b>			
	10 -				333333 333333		<u> </u>	512				•	) )			
222	11 -	- 35			838888											
	12 -	-40					丑									
SAMI	<del>T</del> PLE T	YPF	<b>///////</b> : [{]	Auger Grab Split Spoon Core Barrel	RR RJ	<u> </u>	R	514			<u> </u>		<u>  </u>	<u>  </u>	<u>  </u>	<u>i</u>
	TRAC			INSPECTOR			DDI	ROVE	D			DATE	7			_







## LIQUID LIMIT (LL)

SYMBOL	HOLE	DEPTH (m	) SAMPLE#	LL	PL	PΙ	% SAND	% SILT % CLAY	% MC	CLASSIFICATION
•	TH18-03	8.2	S7	96	22	74			49.7	CH
$\blacksquare$	TH18-09	5.2	S5	100	24	76			49.8	CH
<b>A</b>	TH18-16	8.2	S6	86	29	57			49.7	CH
*	TH18-18	5.2	S5	93	26	67			56.3	CH

Notes:

**ML - Low Plasticity Silt** MH - High Plasticity Silt
CL-ML - Silty Clay
CL - Low Plasticity Clay
CI - Intermediate Plasticity Clay
CH - High Plasticity Clay

LL - Liquid Limit

PL - Plastic Limit PI - Plasticity Index MC - Moisture Content

NP - Non-Plastic

CITY OF WINNIPEG -WATER AND WASTE DEPARTMENT

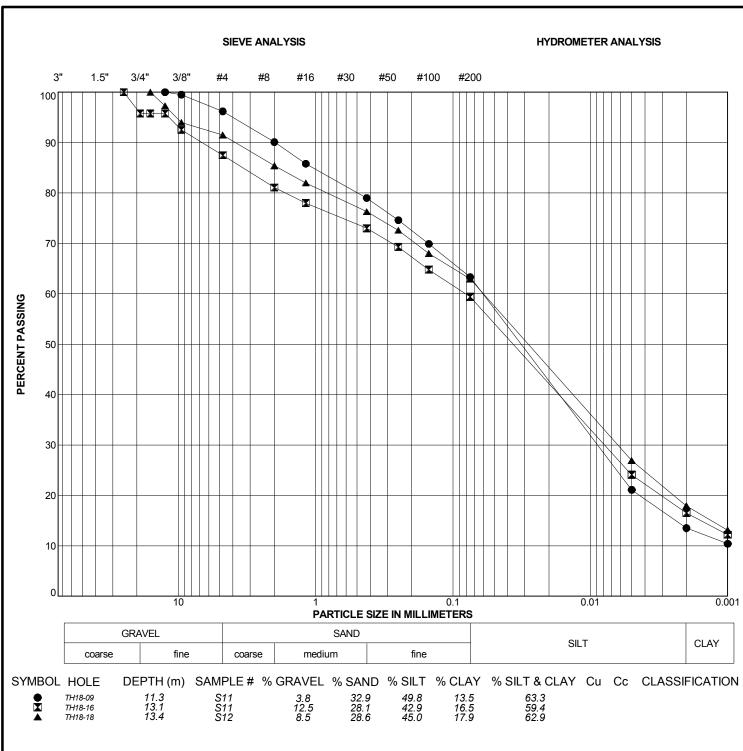
Cockburn and Calrossie Sewer Relief

**A-LINE PLOT** 

August 2018

Figure C1

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CITY OF WINNIPEG -WATER AND WASTE DEPARTMENT

Cockburn and Calrossie Sewer Relief

**GRAIN SIZE ANALYSES** 

August 2018

Figure C2

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