

APPENDIX 'A'

GEOTECHNICAL INVESTIGATION REPORT



Stantec Consulting Ltd.
199 Henlow Bay
Winnipeg MB R3Y 1G4

February 26, 2024

Project/File: 123316895

Ali Campbell

Dillon Consulting Ltd.
1558 Willson Place
Winnipeg, MB R3T 0Y4

Good day Ali,

Reference: 24-R-02 Geotechnical Investigation

Stantec Consulting Ltd. (Stantec) was retained to undertake a factual geotechnical investigation for the Local Streets Package 24-R-02 in Winnipeg, Manitoba. Use of this report is subject to the Statement of General Conditions provided in **Appendix A**.

The subsurface coring and drilling sampling program was conducted from January 10, 2024, to January 25, 2024. Pavement coring was performed by our geotechnical field personnel, and drilling services were provided by Maple Leaf Drilling under the supervision of our personnel. The borehole locations are shown on the attached Borehole Location Plan provided in **Appendix B**. When subsurface drilling was required, the pavement cores were sampled with a 150 mm bit and boreholes were drilled with 125 mm solid stem augers. Geotechnical drilling boreholes were terminated at a depth of 2.0 m below the pavement, which resulted in borehole depths ranging from 2.14 m to 2.25 m below the surface. Soil samples were obtained directly from the auger flights at depths of 0.6 m, 0.9 m, 1.2 m, 1.6 m, and 2.0 m from the bottom of the existing pavement. Upon completion of drilling, the testholes were examined for evidence of sloughing and groundwater seepage. The borehole records are provided in **Appendix C**. The soil classification used in the borehole records is as per ASTM D2487 – *Standard Practice for Classification of Soils for Engineering Purposes (Unified Soil Classification System)*. Core photographs are provided in **Appendix D**.

Reference: 24-R-02 Geotechnical Investigation

EXISTING PAVEMENT THICKNESS

The existing pavement thickness is provided in the following table:

Table 1 – Existing Pavement Thickness

Street	Core ID	Asphalt Thickness (mm)	Concrete Thickness (mm)	Total Pavement Thickness (mm)
Carruthers Ave	BH-40	0	165	165
Carruthers Ave	BH-41	0	175	175
Carruthers Ave	BH-42	0	140	140
McAdam Ave	BH-43	0	175	175
McAdam Ave	BH-44	40	130	170
McAdam Ave	BH-45	20	170	190
Gordon Ave	BH-46	95	160	255
Gordon Ave	BH-47	30	140	170
Gordon Ave	BH-48	90	100	190
Rudolph Bay	BH-49	0	145	145
Rudolph Bay	BH-50	0	150	150
Rudolph Bay	BH-51	0	175	175
Rudolph Bay	BH-52	0	140	140
Dahlia Alley	BH-53	0	160	160
Dahlia Alley	BH-54	0	165	165
Hood Ave	BH-55	0	145	145
Hood Ave	BH-56	0	165	165
Fortier Ave	BH-57	0	165	165
Fortier Ave	BH-58	0	150	150
Summerfield Way	BH-59	55	145	200
Summerfield Way	BH-60	0	155	155
Summerfield Way	BH-61	0	145	145
Summerfield Way	BH-62	0	150	150
Summerfield Way	BH-63	0	155	155
Summerfield Way	BH-64	0	150	150
Summerfield Way	BH-65	65	160	225
Tranquility Cove	BH-66	75	155	230
Tranquility Cove	BH-67	0	155	155

Reference: 24-R-02 Geotechnical Investigation

Street	Core ID	Asphalt Thickness (mm)	Concrete Thickness (mm)	Total Pavement Thickness (mm)
Tranquility Cove	BH-68	0	150	150
Snowdon Ave	BH-69	0	140	140
Snowdon Ave	BH-70	0	135	135
Snowdon Ave	BH-71	0	180	180
Snowdon Ave	BH-72	0	125	125
Snowdon Ave	BH-73	30	150	180
Dearborn Ave	BH-74	0	165	165
Dearborn Ave	BH-75	0	170	170
Lacy St	BH-76	0	165	165
Lacy St	BH-77	0	180	180
Norilyn Bay	BH-78	0	155	155
Norilyn Bay	BH-79	0	160	160
Norilyn Bay	BH-80	0	150	150
Norilyn Bay	BH-81	0	155	155
Kullman St	BH-82	0	150	150
Kullman St	BH-83	0	155	155

LABORATORY TESTING

The following laboratory tests were conducted on select soil samples:

- ASTM D2216 - *Laboratory Determination of Water (Moisture) Content of Soil by Mass*
- ASTM D4318 - *Liquid Limit, Plastic Limit, and Plasticity Index of Soils*
- ASTM D7928 - *Particle-Size Distribution of Fine-Grained Soils Using The Sedimentation Analysis*
- ASTM D698 - *Laboratory Compaction Characteristics of Soil Using Standard Effort*
- ASTM D1883 - *California Bearing Ratio (CBR) of Laboratory-Compacted Soils*
- CSA A23.2-14C – *Obtaining and testing drilled cores for compressive strength testing*

The CBR tests were performed at 95% maximum dry density under soaked conditions. Prior to testing the concrete core samples for compressive strength, the cores were conditioned in water at room temperature for 48 hours. The moisture content results are shown on the borehole records, and the laboratory test reports are provided in **Appendix E**.

Reference: 24-R-02 Geotechnical Investigation

CLOSURE

We appreciate the opportunity to assist you on this project. Please contact the undersigned if you have any questions regarding this report.

Regards,

STANTEC CONSULTING LTD.



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Attachment: Appendix A – Statement of General Conditions
Appendix B – Borehole Location Plan
Appendix C – Borehole Records
Appendix D – Core Photographs
Appendix E – Laboratory Test Reports

- Atterberg Limits Test Reports
- Particle-Size Analysis Reports
- Standard Proctor Test Reports
- CBR Test Reports
- Concrete Core Compressive Strength Test Results

APPENDIX A

Statement of General Conditions

STATEMENT OF GENERAL CONDITIONS

USE OF THIS REPORT: This report has been prepared for the sole benefit of the Client or its agent and may not be used by any third party without the express written consent of Stantec and the Client. Any use which a third party makes of this report is the responsibility of such third party.

BASIS OF THE REPORT: The information, opinions, and/or recommendations made in this report are in accordance with Stantec's present understanding of the site-specific project as described by the Client. The applicability of these is restricted to the site conditions encountered at the time of the investigation or study. If the proposed site-specific project differs or is modified from what is described in this report or if the site conditions are altered, this report is no longer valid unless Stantec is requested by the Client to review and revise the report to reflect the differing or modified project specifics and/or the altered site conditions.

STANDARD OF CARE: Preparation of this report, and all associated work, was carried out in accordance with the normally accepted standard of care in the state or province of execution for the specific professional service provided to the Client. No other warranty is made.

INTERPRETATION OF SITE CONDITIONS: Soil, rock, or other material descriptions, and statements regarding their condition, made in this report are based on site conditions encountered by Stantec at the time of the work and at the specific testing and/or sampling locations. Classifications and statements of condition have been made in accordance with normally accepted practices which are judgmental in nature; no specific description should be considered exact, but rather reflective of the anticipated material behavior. Extrapolation of in situ conditions can only be made to some limited extent beyond the sampling or test points. The extent depends on variability of the soil, rock, and groundwater conditions as influenced by geological processes, construction activity, and site use.

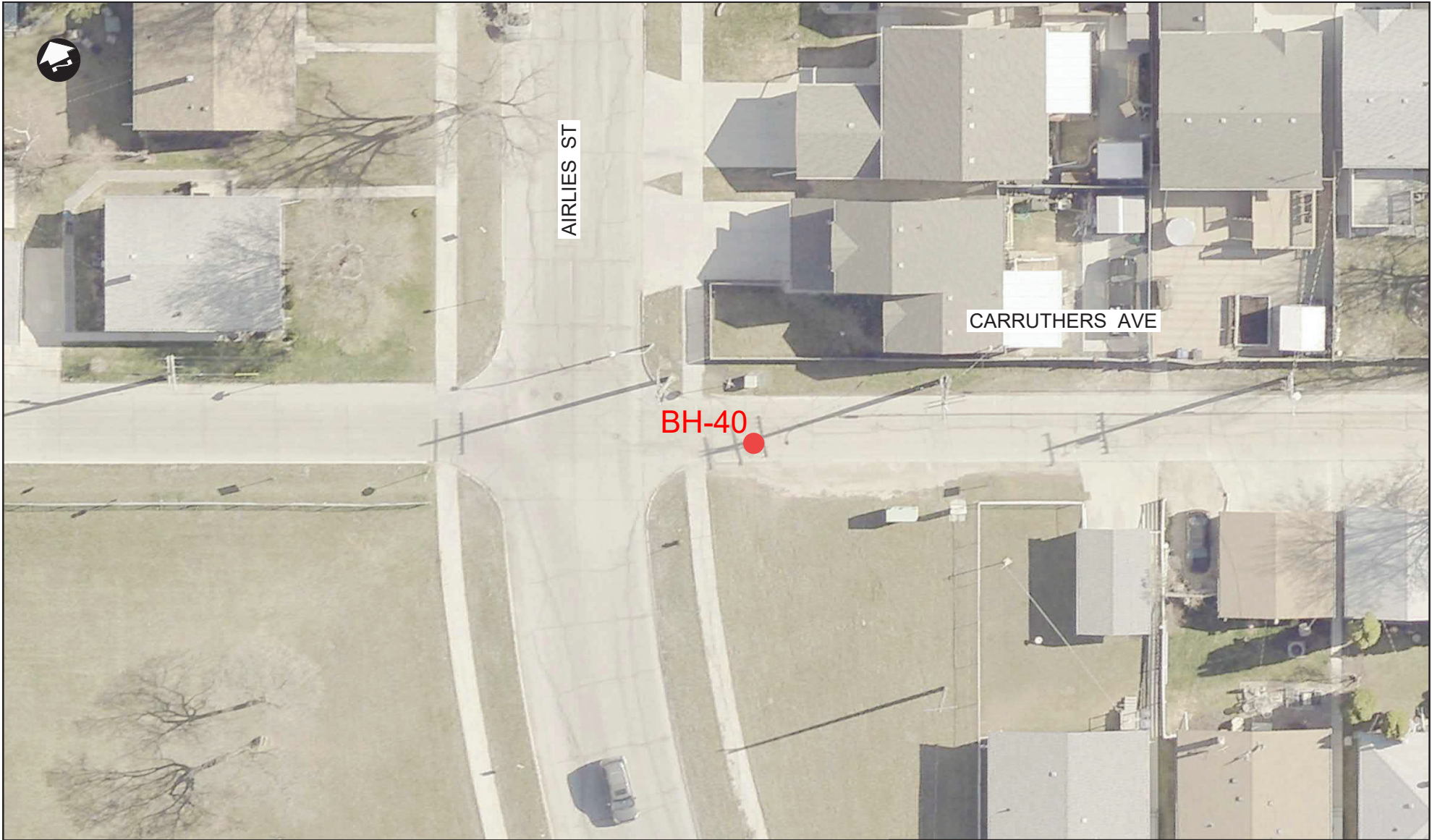
VARYING OR UNEXPECTED CONDITIONS: Should any site or subsurface conditions be encountered that are different from those described in this report or encountered at the test locations, Stantec must be notified immediately to assess if the varying or unexpected conditions are substantial and if reassessments of the report conclusions or recommendations are required. Stantec will not be responsible to any party for damages incurred as a result of failing to notify Stantec that differing site or sub-surface conditions are present upon becoming aware of such conditions.

PLANNING, DESIGN, OR CONSTRUCTION: Development or design plans and specifications should be reviewed by Stantec, sufficiently ahead of initiating the next project stage (property acquisition, tender, construction, etc.), to confirm that this report completely addresses the elaborated project specifics and that the contents of this report have been properly interpreted. Specialty quality assurance services (field observations and testing) during construction are a necessary part of the evaluation of sub-subsurface conditions and site preparation works. Site work relating to the recommendations included in this report should only be carried out in the presence of a qualified geotechnical engineer; Stantec cannot be responsible for site work carried out without being present.



APPENDIX B

Borehole Location Plan



AIRLIES ST

CARRUTHERS AVE

BH-40



TITLE	CARRUTHERS AVENUE 1 OF 5
-------	-----------------------------

PROJECT NO.	-
DRAWING NO.	-



CARRUTHERS AVE



TITLE
CARRUTHERS AVENUE
2 OF 5

PROJECT NO.
-
DRAWING NO.
-



CARRUTHERS AVE

BH-41 ●



SCALE: 1:250

TITLE

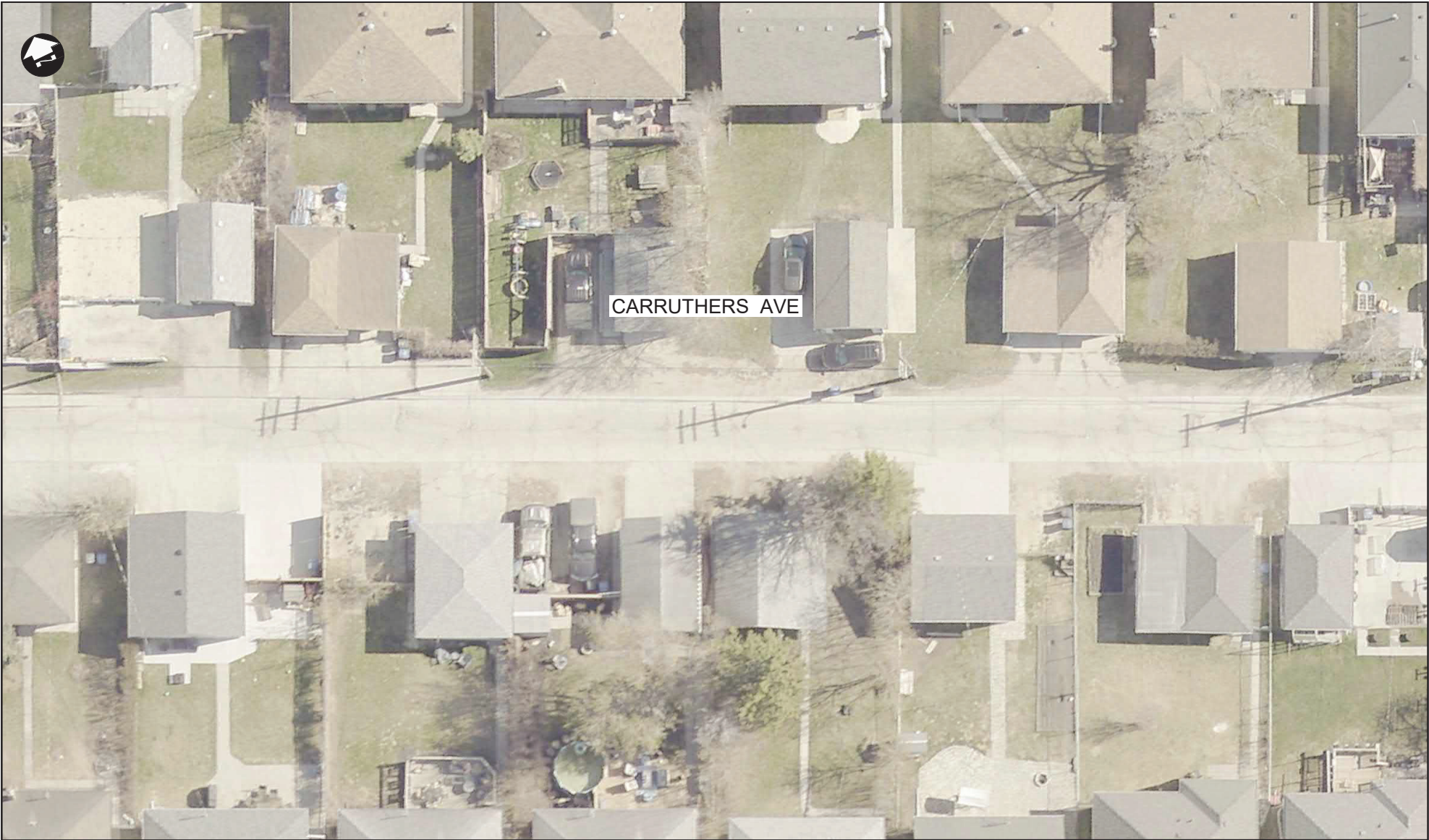
CARRUTHERS AVENUE
3 OF 5

PROJECT NO.

-

DRAWING NO.

-



CARRUTHERS AVE



SCALE: 1:250

TITLE

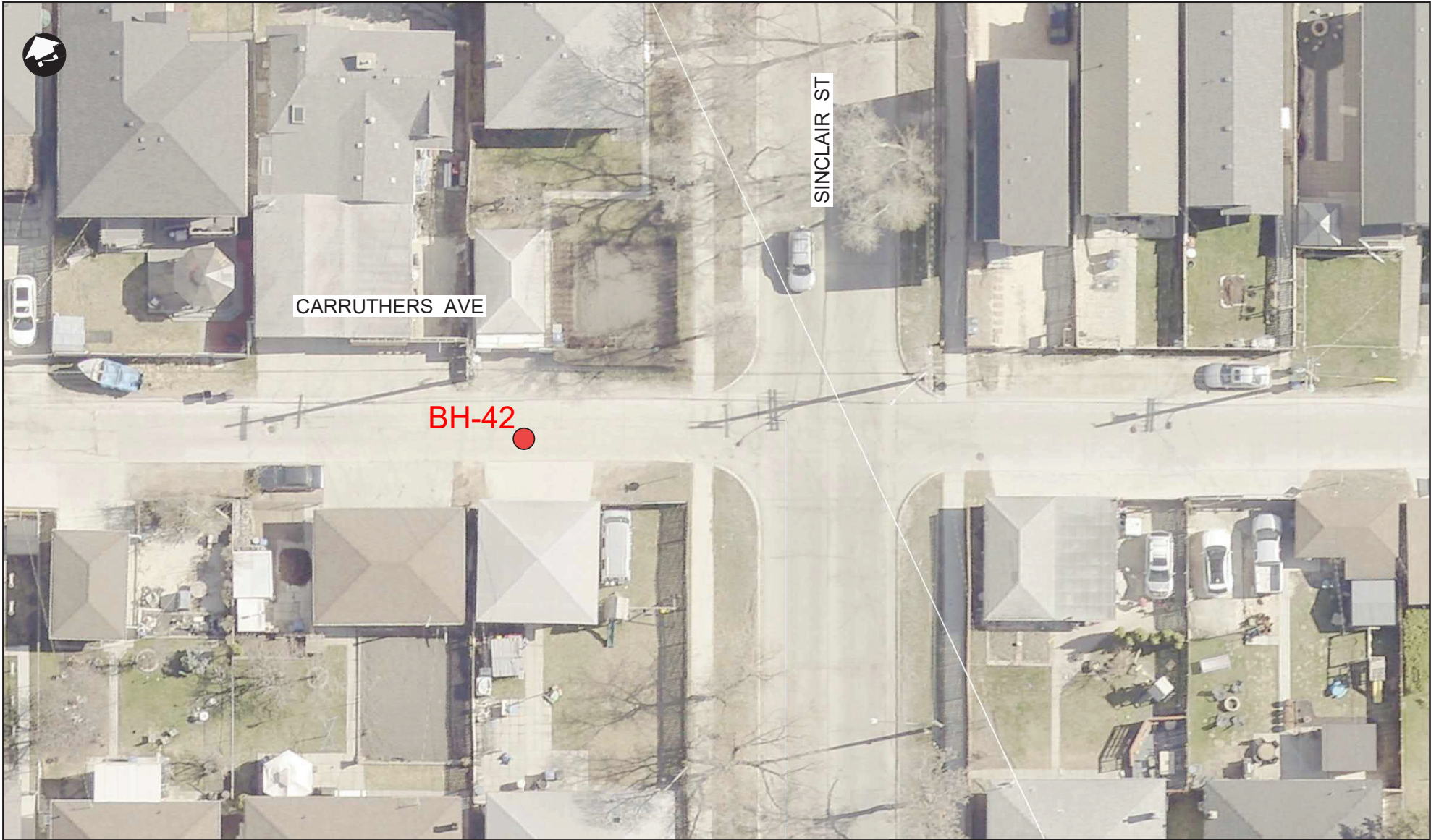
CARRUTHERS AVENUE
4 OF 5

PROJECT NO.

-

DRAWING NO.

-



CARRUTHERS AVE

SINCLAIR ST

BH-42



TITLE	CARRUTHERS AVENUE 5 OF 5
-------	-----------------------------

PROJECT NO.	-
DRAWING NO.	-



TITLE
McADAM AVENUE
1 OF 2

PROJECT NO. -
DRAWING NO. -



McADAM AVE

BH-45

ARLINGTON ST



TITLE
McADAM AVENUE
2 OF 2

PROJECT NO. -
DRAWING NO. -

SCALE: 1:250



BRAZIER ST

GORDON AVE

BH-46 ●

LACY ST



SCALE: 1:250

TITLE

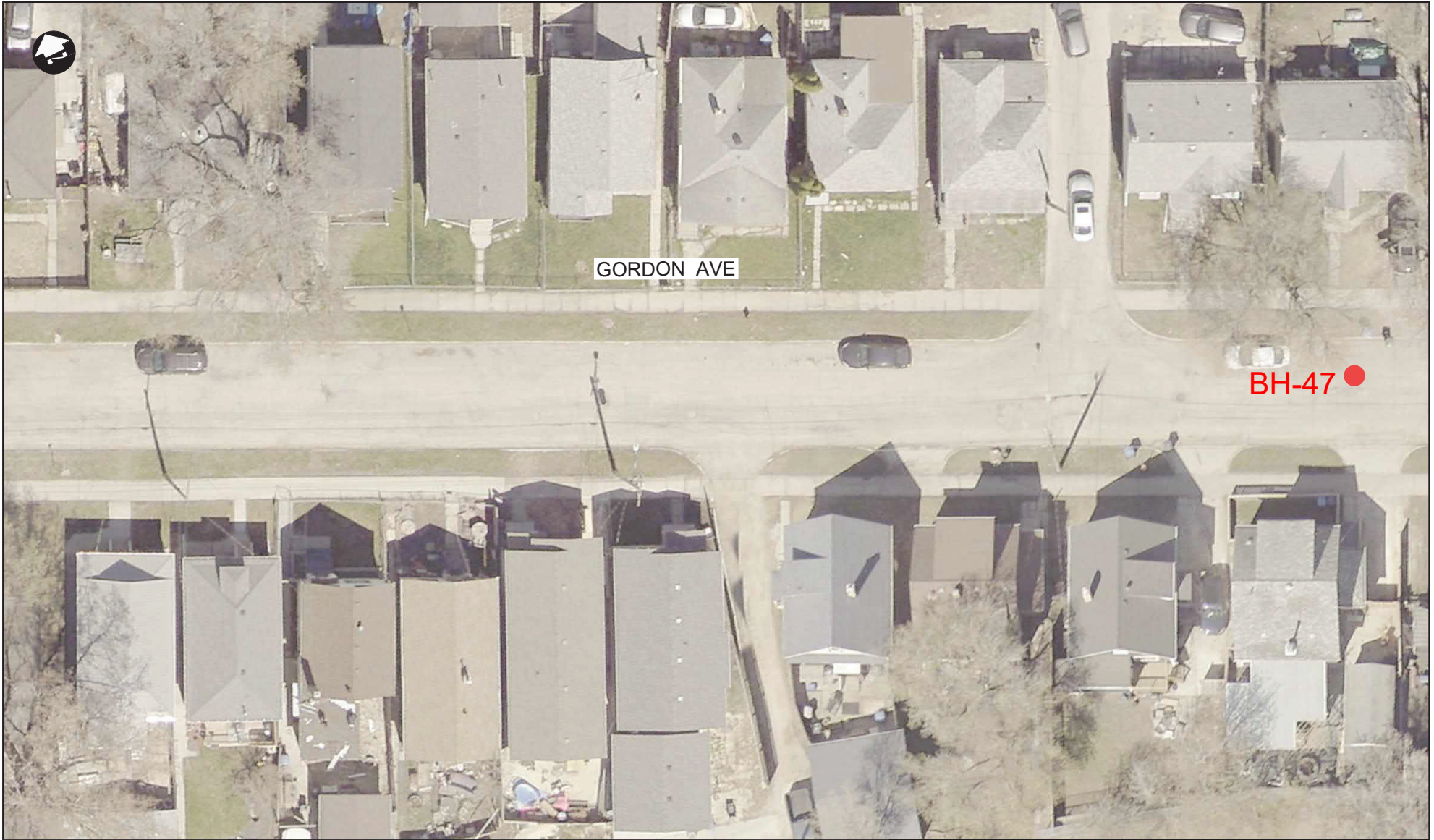
GORDON AVENUE
1 OF 4

PROJECT NO.

-

DRAWING NO.

-



GORDON AVE

BH-47 ●



TITLE	GORDON AVENUE 2 OF 4
-------	-------------------------

PROJECT NO.	-
DRAWING NO.	-



GORDON AVE



SCALE: 1:250

TITLE

GORDON AVENUE
3 OF 4

PROJECT NO.

-

DRAWING NO.

-



TITLE	GORDON AVENUE 4 OF 4
-------	-------------------------

PROJECT NO.	-
DRAWING NO.	-



RUDOLPH BAY

BH-49 ●

SNOWDON AVE



TITLE	RUDOLPH BAY 1 OF 3
PROJECT NO.	-
DRAWING NO.	-



RUDOLPH BAY

BH-50 ●

BH-51 ●



SCALE: 1:250

TITLE

RUDOLPH BAY
2 OF 3

PROJECT NO.

-

DRAWING NO.

-



SNOWDON AVE

BH-52

RUDOLPH BAY



SCALE: 1:250

TITLE

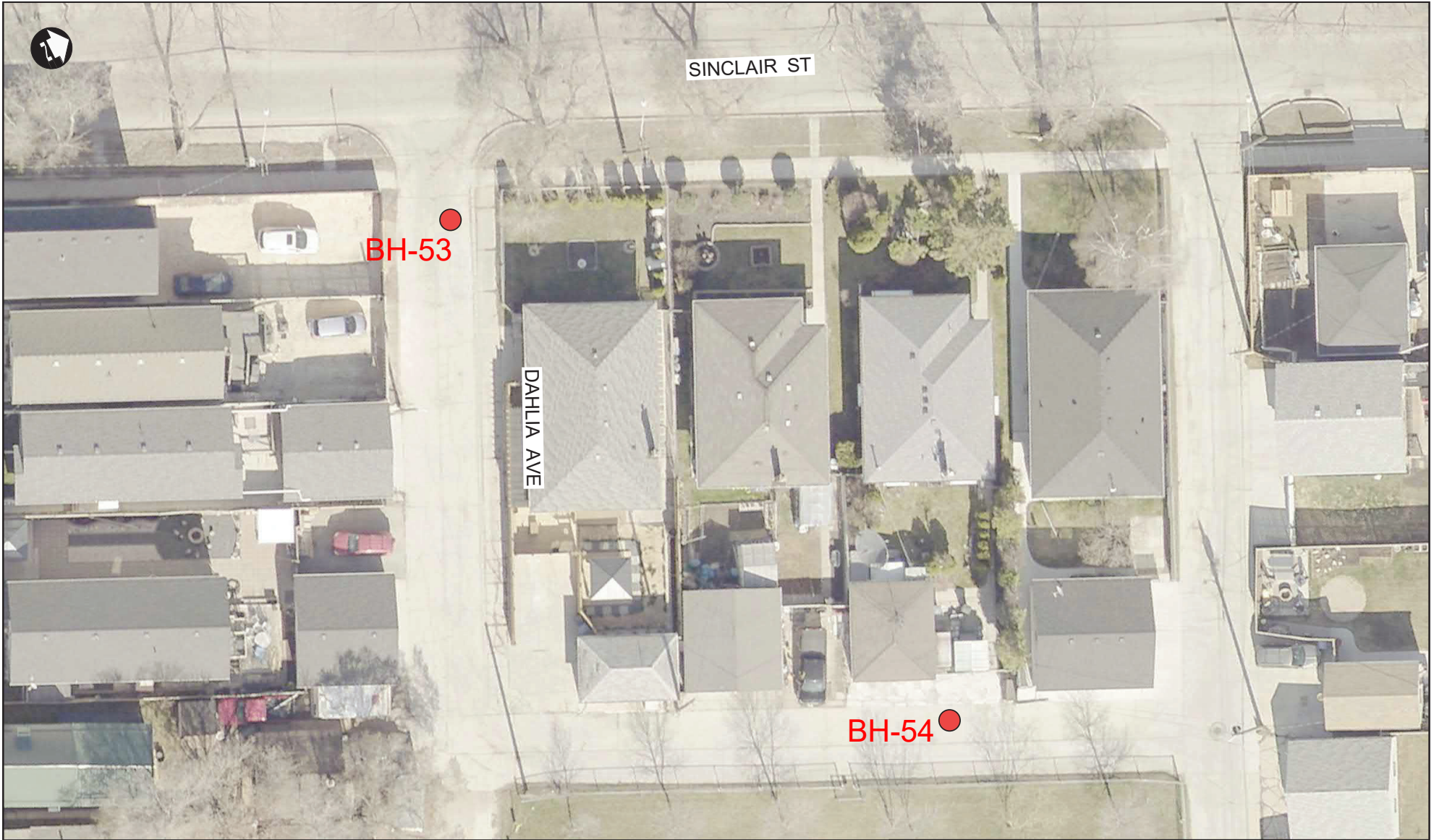
RUDOLPH BAY
3 OF 3

PROJECT NO.

-

DRAWING NO.

-



TITLE
DAHLIA AVENUE
1 OF 1

PROJECT NO.	-
DRAWING NO.	-



TITLE	HOOD AVENUE 1 OF 2
PROJECT NO.	-
DRAWING NO.	-



SCARFE ST

HOOD AVE

BH-56



TITLE	HOOD AVENUE 2 OF 2
-------	-----------------------

PROJECT NO.	-
DRAWING NO.	-



PENTLAND ST

FORTIER AVE

BH-57



SCALE: 1:250

TITLE

FORTIER AVENUE
1 OF 2

PROJECT NO.

-

DRAWING NO.

-



FORTIER AVE

BH-58

SUMMERFIELD WAY



SCALE: 1:250

TITLE

FORTIER AVENUE
2 OF 2

PROJECT NO.

DRAWING NO.



GILMORE AVE

SUMMERFIELD WAY

BH-59



SCALE: 1:250

TITLE

SUMMERFIELD WAY
1 OF 8

PROJECT NO.

-

DRAWING NO.

-



FORTIER AVE

SUMMERFIELD WAY

BH-60



SCALE: 1:250

TITLE

SUMMERFIELD WAY
2 OF 8

PROJECT NO.

-

DRAWING NO.

-



SUMMERFIELD WAY

BH-61



TITLE	PROJECT NO.
SUMMERFIELD WAY	-
3 OF 8	DRAWING NO.
	-



SUMMERFIELD WAY



TITLE

SUMMERFIELD WAY
4 OF 8

SCALE: 1:250

PROJECT NO.

-

DRAWING NO.

-



SUMMERFIELD WAY

BH-62



TITLE

SUMMERFIELD WAY
5 OF 8

PROJECT NO.

-

DRAWING NO.

-



SUMMERFIELD WAY

BH-63

TRANQUILITY COVE



TITLE	PROJECT NO.
SUMMERFIELD WAY	-
6 OF 8	DRAWING NO.
	-



SUMMERFIELD WAY

● BH-64



SCALE: 1:250

TITLE

SUMMERFIELD WAY
7 OF 8

PROJECT NO.

-

DRAWING NO.

-



SUMMERFIELD WAY

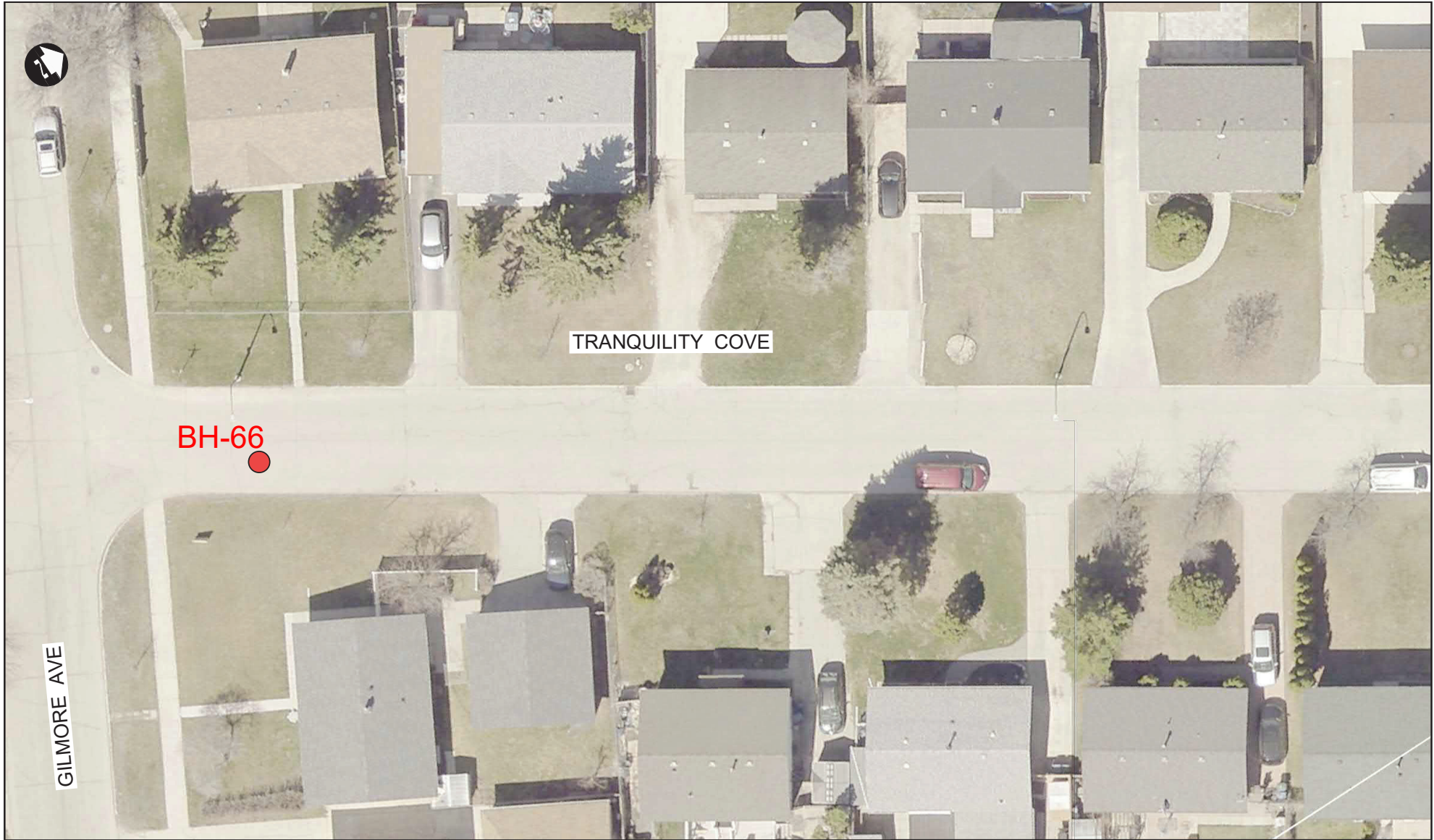
BH-65

GILMORE AVE



TITLE	SUMMERFIELD WAY 8 OF 8
-------	---------------------------

PROJECT NO.	-
DRAWING NO.	-



TRANQUILITY COVE

BH-66

GILMORE AVE



TITLE

TRANQUILITY COVE
1 OF 3

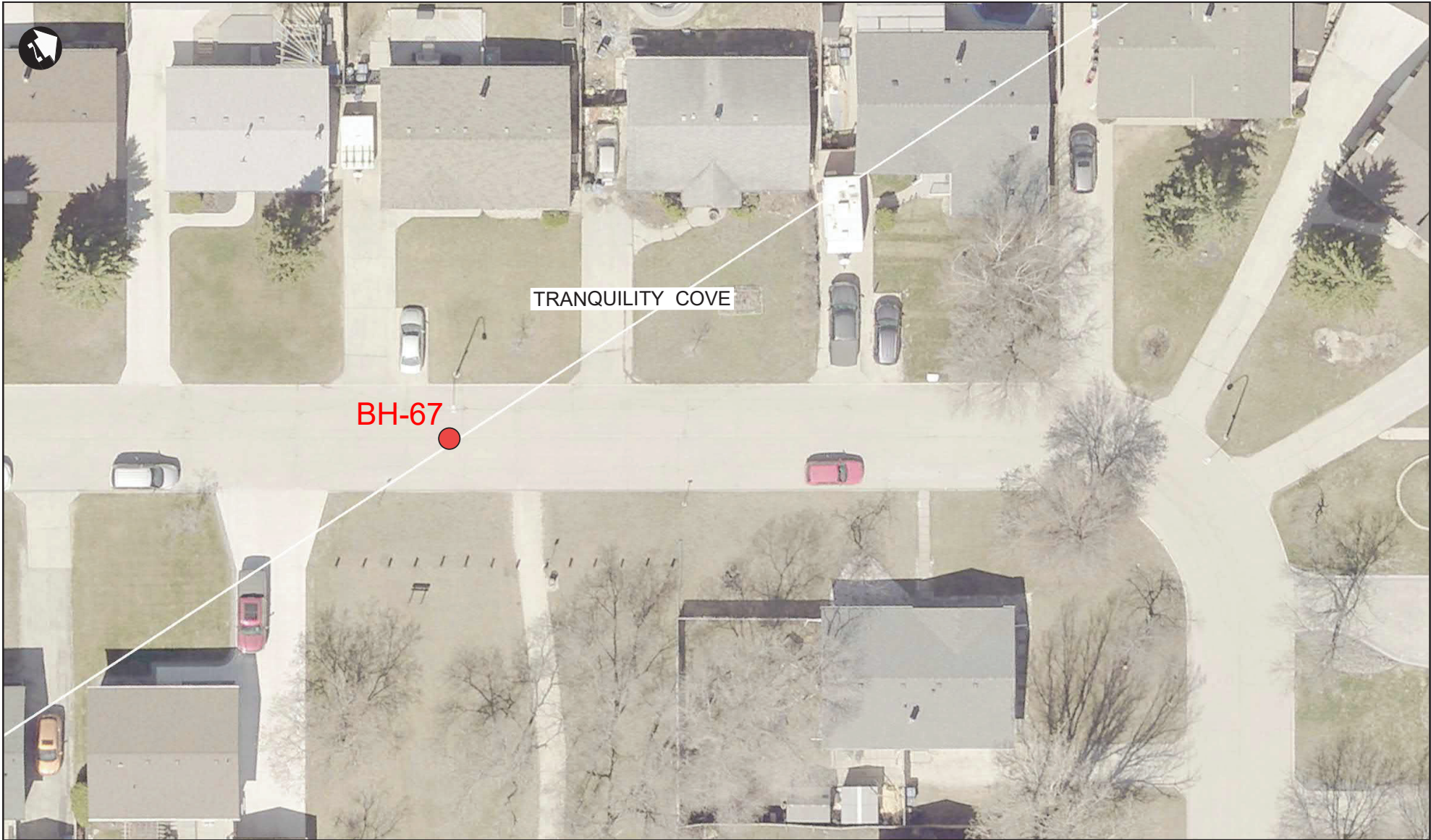
SCALE: 1:250

PROJECT NO.

-

DRAWING NO.

-



TRANQUILITY COVE

BH-67



TITLE
TRANQUILITY COVE
2 OF 3

PROJECT NO.
-
DRAWING NO.
-



TITLE
TRANQUILITY COVE
3 OF 3

PROJECT NO.	-
DRAWING NO.	-



SNOWDON AVE

BH-69

TREGER BAY



SCALE: 1:250

TITLE

SNOWDON AVENUE
1 OF 5

PROJECT NO.

-

DRAWING NO.

-



SNOWDON AVE

BH-70



TITLE

SNOWDON AVENUE
2 OF 5

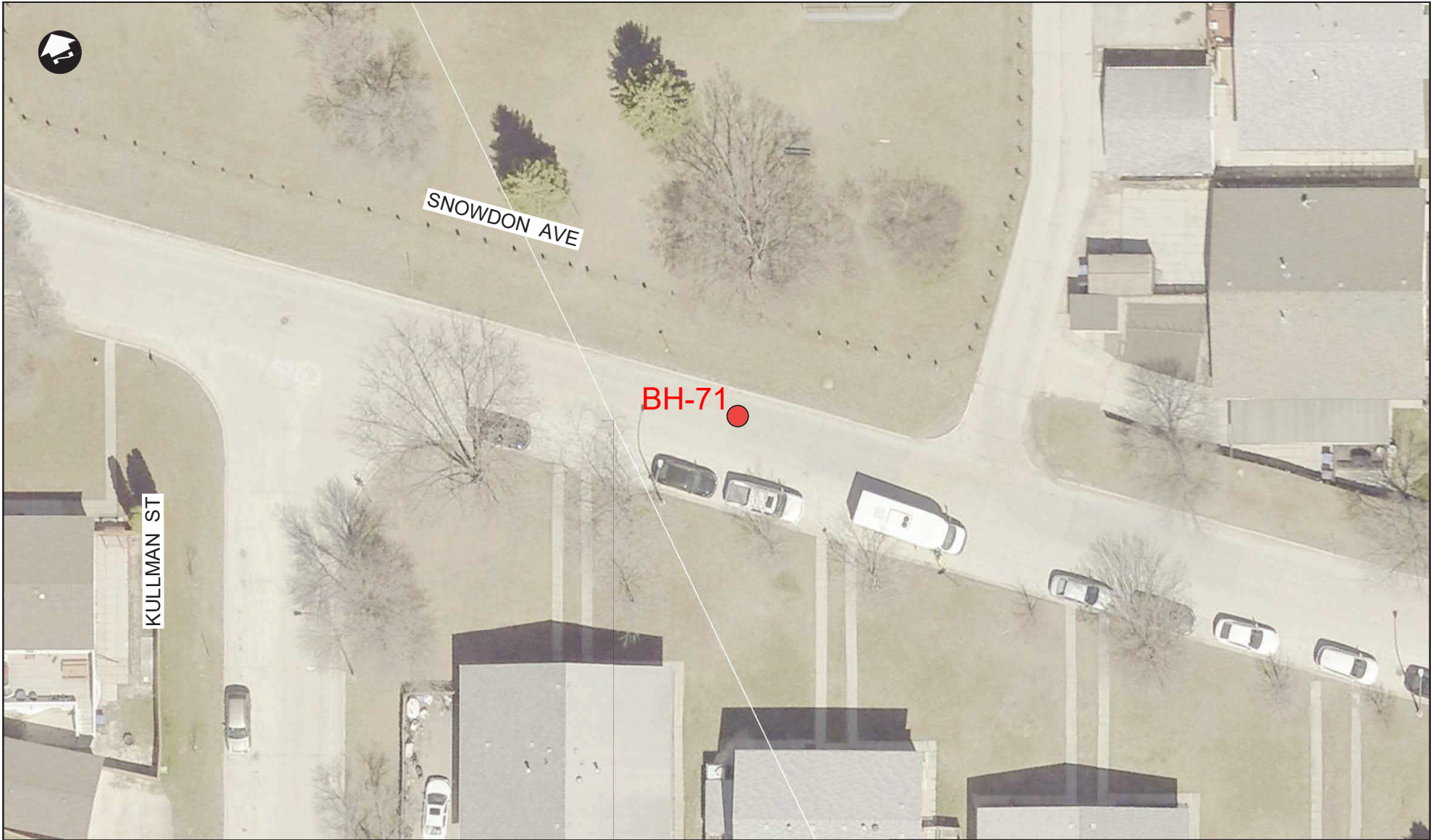
PROJECT NO.

-

DRAWING NO.

-

SCALE: 1:250



TITLE	PROJECT NO.
SNOWDON AVENUE	-
3 OF 5	DRAWING NO.
	-

SCALE: 1:250



RUDOLPH BAY

RUDOLPH BAY

SNOWDON AVE

BH-72



SCALE: 1:250

TITLE

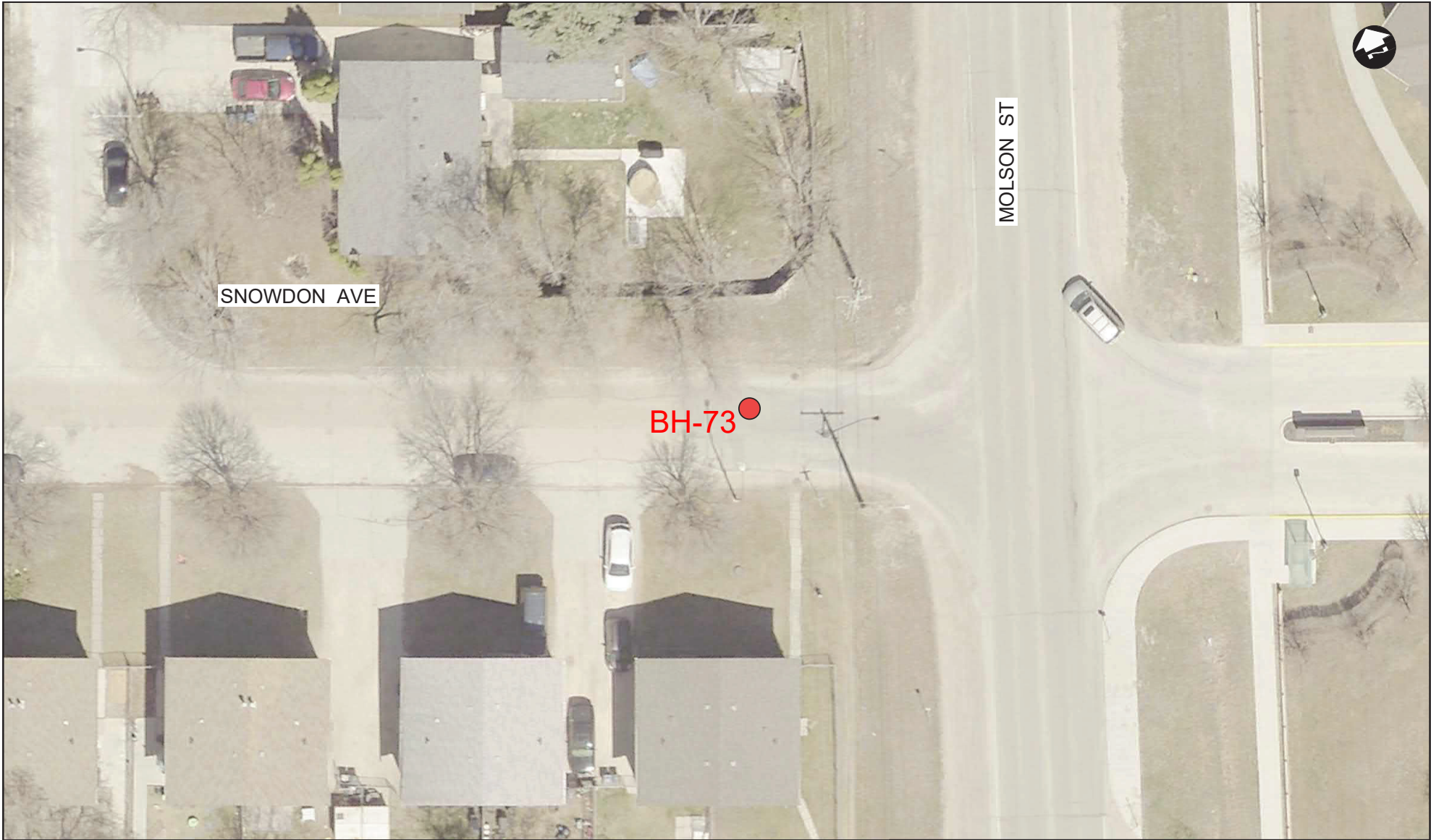
SNOWDON AVENUE
4 OF 5

PROJECT NO.

-

DRAWING NO.

-



SNOWDON AVE

MOLSON ST

BH-73



SCALE: 1:250

TITLE

SNOWDON AVENUE
5 OF 5

PROJECT NO.

-

DRAWING NO.

-



BRAZIER ST

DEARBORN AVE

BH-74 ●

BH-75 ●

LACY ST



SCALE: 1:250

TITLE

DEARBORN AVENUE
1 OF 1

PROJECT NO.

-

DRAWING NO.

-



BH-76

LACY ST

DEARBORN AVE



TITLE

LACY STREET
1 OF 2

SCALE: 1:250

PROJECT NO.

-

DRAWING NO.

-



LACY ST

GORDON AVE

BH-77



TITLE	LACY STREET 2 OF 2
-------	-----------------------

PROJECT NO.	-
DRAWING NO.	-



ROCKSPUR ST

ANTRIM RD

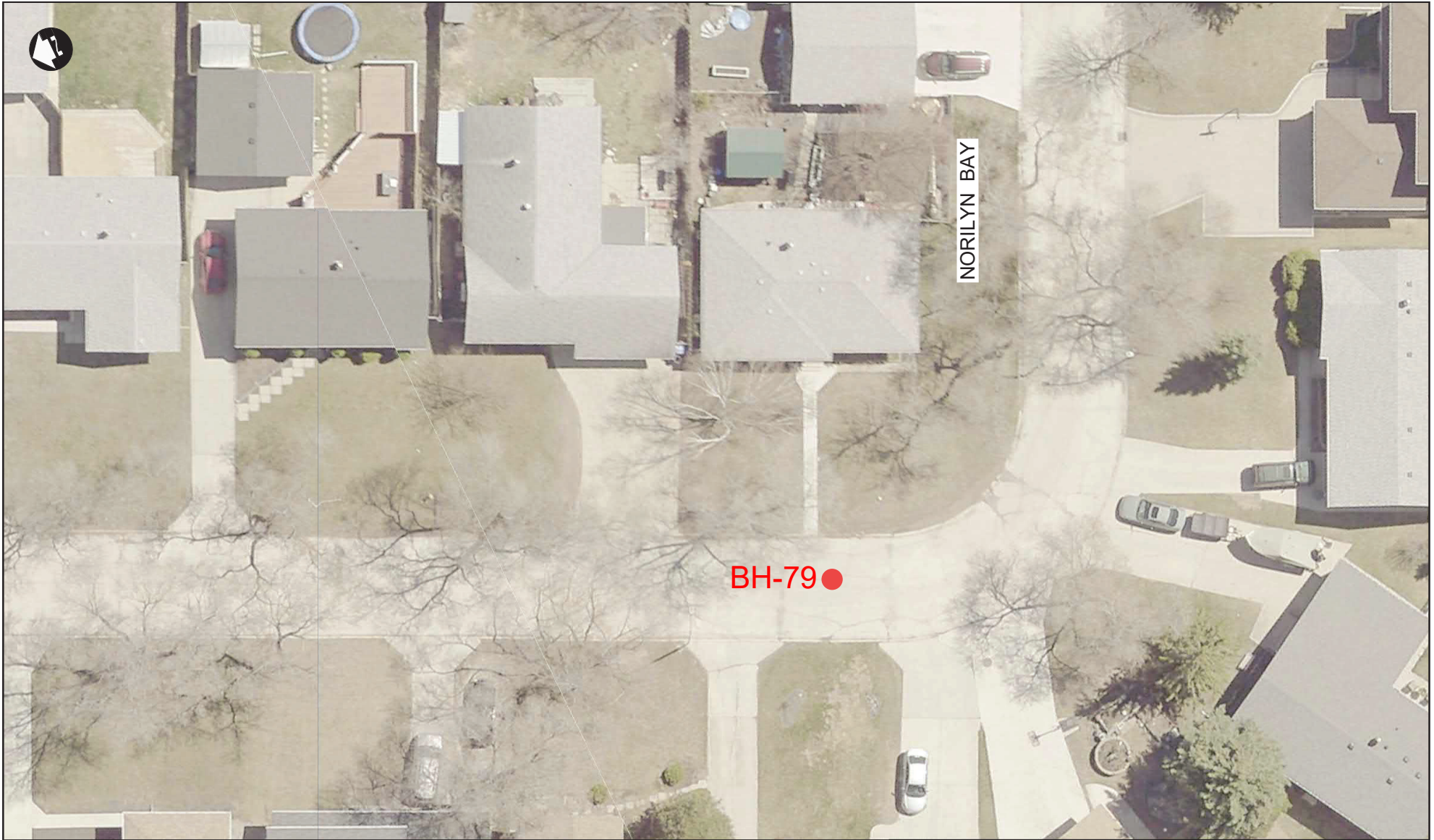
NORILYN BAY

BH-78



TITLE	NORILYN BAY 1 OF 4
-------	-----------------------

PROJECT NO.	-
DRAWING NO.	-



BH-79 ●

NORILYN BAY



TITLE

NORILYN BAY
2 OF 4

PROJECT NO.

-

DRAWING NO.

-



NORILYN BAY

BH-80



TITLE	NORILYN BAY 3 OF 4
PROJECT NO.	-
DRAWING NO.	-



NORILYN BAY

ANTRIM RD

DAMPSY CR

BH-81



TITLE
NORILYN BAY
4 OF 4

PROJECT NO. -
DRAWING NO. -



BH-82

KULLMAN ST

KIMBERLY AVE



TITLE
KULLMAN STREET
1 OF 2

PROJECT NO. -
DRAWING NO. -



TITLE	KULLMAN STREET 2 OF 2
-------	--------------------------

PROJECT NO.	-
DRAWING NO.	-

APPENDIX C

Borehole Records

SYMBOLS AND TERMS USED ON BOREHOLE AND TEST PIT RECORDS

SOIL DESCRIPTION

Terminology describing common soil genesis:

<i>Rootmat</i>	- vegetation, roots and moss with organic matter and topsoil typically forming a mattress at the ground surface
<i>Topsoil</i>	- mixture of soil and humus capable of supporting vegetative growth
<i>Peat</i>	- mixture of visible and invisible fragments of decayed organic matter
<i>Till</i>	- unstratified glacial deposit which may range from clay to boulders
<i>Fill</i>	- material below the surface identified as placed by humans (excluding buried services)

Terminology describing soil structure:

<i>Desiccated</i>	- having visible signs of weathering by oxidization of clay minerals, shrinkage cracks, etc.
<i>Fissured</i>	- having cracks, and hence a blocky structure
<i>Varved</i>	- composed of regular alternating layers of silt and clay
<i>Stratified</i>	- composed of alternating successions of different soil types, e.g. silt and sand
<i>Layer</i>	- > 75 mm in thickness
<i>Seam</i>	- 2 mm to 75 mm in thickness
<i>Parting</i>	- < 2 mm in thickness

Terminology describing soil types:

The classification of soil types are made on the basis of grain size and plasticity in accordance with the Unified Soil Classification System (USCS) (ASTM D 2487 or D 2488) which excludes particles larger than 75 mm. For particles larger than 75 mm, and for defining percent clay fraction in hydrometer results, definitions proposed by Canadian Foundation Engineering Manual, 4th Edition are used. The USCS provides a group symbol (e.g. SM) and group name (e.g. silty sand) for identification.

Terminology describing cobbles, boulders, and non-matrix materials (organic matter or debris):

Terminology describing materials outside the USCS, (e.g. particles larger than 75 mm, visible organic matter, and construction debris) is based upon the proportion of these materials present:

<i>Trace, or occasional</i>	Less than 10%
<i>Some</i>	10-20%
<i>Frequent</i>	> 20%

Terminology describing compactness of cohesionless soils:

The standard terminology to describe cohesionless soils includes compactness (formerly "relative density"), as determined by the Standard Penetration Test (SPT) N-Value - also known as N-Index. The SPT N-Value is described further on page 3. A relationship between compactness condition and N-Value is shown in the following table.

Compactness Condition	SPT N-Value
<i>Very Loose</i>	<4
<i>Loose</i>	4-10
<i>Compact</i>	10-30
<i>Dense</i>	30-50
<i>Very Dense</i>	>50

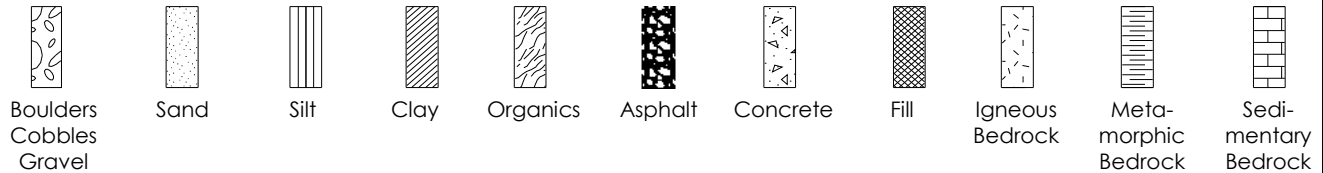
Terminology describing consistency of cohesive soils:

The standard terminology to describe cohesive soils includes the consistency, which is based on undrained shear strength as measured by *in situ* vane tests, penetrometer tests, or unconfined compression tests. Consistency may be crudely estimated from SPT N-Value based on the correlation shown in the following table (Terzaghi and Peck, 1967). The correlation to SPT N-Value is used with caution as it is only very approximate.

Consistency	Undrained Shear Strength		Approximate SPT N-Value
	kips/sq.ft.	kPa	
<i>Very Soft</i>	<0.25	<12.5	<2
<i>Soft</i>	0.25 - 0.5	12.5 - 25	2-4
<i>Firm</i>	0.5 - 1.0	25 - 50	4-8
<i>Stiff</i>	1.0 - 2.0	50 - 100	8-15
<i>Very Stiff</i>	2.0 - 4.0	100 - 200	15-30
<i>Hard</i>	>4.0	>200	>30

STRATA PLOT

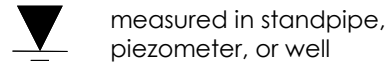
Strata plots symbolize the soil or bedrock description. They are combinations of the following basic symbols. The dimensions within the strata symbols are not indicative of the particle size, layer thickness, etc.



SAMPLE TYPE

SS	Split spoon sample (obtained by performing the Standard Penetration Test)
ST	Shelby tube or thin wall tube
DP	Direct-Push sample (small diameter tube sampler hydraulically advanced)
PS	Piston sample
BS	Bulk sample
HQ, NQ, BQ, etc.	Rock core samples obtained with the use of standard size diamond coring bits.

WATER LEVEL MEASUREMENT



measured in standpipe, piezometer, or well



inferred

RECOVERY

For soil samples, the recovery is recorded as the length of the soil sample recovered. For rock core, recovery is defined as the total cumulative length of all core recovered in the core barrel divided by the length drilled and is recorded as a percentage on a per run basis.

N-VALUE

Numbers in this column are the field results of the Standard Penetration Test: the number of blows of a 140 pound (63.5 kg) hammer falling 30 inches (760 mm), required to drive a 2 inch (50.8 mm) O.D. split spoon sampler one foot (300 mm) into the soil. In accordance with ASTM D1586, the N-Value equals the sum of the number of blows (N) required to drive the sampler over the interval of 6 to 18 in. (150 to 450 mm). However, when a 24 in. (610 mm) sampler is used, the number of blows (N) required to drive the sampler over the interval of 12 to 24 in. (300 to 610 mm) may be reported if this value is lower. For split spoon samples where insufficient penetration was achieved and N-Values cannot be presented, the number of blows are reported over sampler penetration in millimetres (e.g. 50/75). Some design methods make use of N-values corrected for various factors such as overburden pressure, energy ratio, borehole diameter, etc. No corrections have been applied to the N-values presented on the log.

DYNAMIC CONE PENETRATION TEST (DCPT)

Dynamic cone penetration tests are performed using a standard 60 degree apex cone connected to 'A' size drill rods with the same standard fall height and weight as the Standard Penetration Test. The DCPT value is the number of blows of the hammer required to drive the cone one foot (300 mm) into the soil. The DCPT is used as a probe to assess soil variability.

OTHER TESTS

S	Sieve analysis
H	Hydrometer analysis
k	Laboratory permeability
γ	Unit weight
G_s	Specific gravity of soil particles
CD	Consolidated drained triaxial
CU	Consolidated undrained triaxial with pore pressure measurements
UU	Unconsolidated undrained triaxial
DS	Direct Shear
C	Consolidation
Q_u	Unconfined compression
I_p	Point Load Index (I_p on Borehole Record equals $I_p(50)$ in which the index is corrected to a reference diameter of 50 mm)

	Single packer permeability test; test interval from depth shown to bottom of borehole
	Double packer permeability test; test interval as indicated
	Falling head permeability test using casing
	Falling head permeability test using well point or piezometer



BOREHOLE RECORD

BH-40

CLIENT: Dillon Consulting Ltd.

PROJECT NO.: 123316895

PROJECT: 24-R-02 Geotechnical Investigation

BH ELEVATION: N/A

LOCATION: Carruthers Avenue

DATUM: N/A

DATE BORED: January 16 2024

WATER LEVEL: N/A

DEPTH (m)	ELEVATION (m)	SOIL DESCRIPTION (MUSCS)	STRATA PLOT	SAMPLES				OTHER TESTS / REMARKS	UNDRAINED SHEAR STRENGTH, Cu (kPa)				BACKFILL	ELEVATION (m)
				TYPE	NUMBER	RECOVERY (mm) or TCR %	N-VALUE or RQD %		50 kPa	100 kPa	150 kPa	200 kPa		
0		CONCRETE							▲ LABORATORY TEST ◆ FIELD VANE TEST ★ POCKET PENETROMETER □ POCKET SHEAR VANE 50 kPa 100 kPa 150 kPa 200 kPa					
		FILL: compact tan crushed limestone, 19 mm maximum aggregate size							WATER CONTENT & ATTERBERG LIMITS W _p W W _L ✕ SPT (N-value) BLOWS/0.3m 10 20 30 40 50 60 70 80					
		End of Borehole • Auger refusal on suspected concrete at a depth of 0.24 m. • No groundwater seepage or soil sloughing was observed during or upon completion of drilling. • Borehole surface backfilled as per City of Winnipeg Street Cuts Manual.												

Printed Feb 8 2024 15:11:42 SOIL 123316895_24-R-02 GEOTECHNICAL INVESTIGATION.GPJ NEW TEMPLATE TEST PROJECT.GPJ 2/8/24

	BACKFILL SYMBOL		ASPHALT		GROUT		CONCRETE
	BENTONITE		DRILL CUTTINGS		SAND		SLOUGH

Drilling Contractor: Maple Leaf Drilling Ltd.	Logged By: LP
Drilling Method: 125 mm SSA	Reviewed By: GB
Completion Depth: 0.24 m	Page 1 of 1

CLIENT: Dillon Consulting Ltd.
 PROJECT: 24-R-02 Geotechnical Investigation
 LOCATION: Carruthers Avenue
 DATE BORED: January 16 2024

PROJECT NO.: 123316895
 BH ELEVATION: N/A
 DATUM: N/A

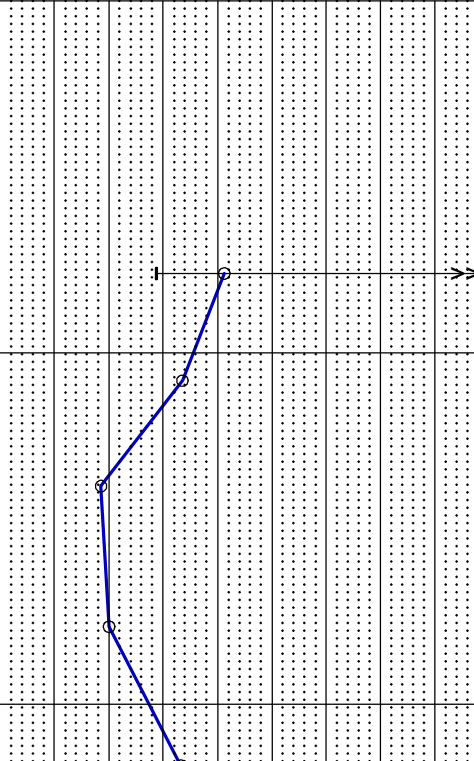
WATER LEVEL: N/A

DEPTH (m)	ELEVATION (m)	SOIL DESCRIPTION (MUSCS)	STRATA PLOT	SAMPLES				OTHER TESTS / REMARKS	UNDRAINED SHEAR STRENGTH, Cu (kPa)				BACKFILL	ELEVATION (m)
				TYPE	NUMBER	RECOVERY (mm) or TCR %	N-VALUE or RQD %		50 kPa	100 kPa	150 kPa	200 kPa		
0		CONCRETE												
		FILL: compact tan crushed limestone, 19 mm maximum aggregate size Firm to stiff black fat CLAY (CH) - silty, trace sand												
			AS											
1			AS											
		Soft tan lean CLAY (CL)	AS											
			AS											
2		Firm brown fat CLAY (CH)	AS											
			AS											
		<p>End of Borehole</p> <ul style="list-style-type: none"> Borehole terminated at a depth of 2.175 m. No groundwater seepage or soil sloughing was observed during or upon completion of drilling. Borehole backfilled with auger cuttings and bentonite chips. Borehole surface backfilled as per City of Winnipeg Street Cuts Manual. 												

Sieve/Hydro at 0.8 m
 G S M C
 0% 1% 28% 70%

WATER CONTENT & ATTERBERG LIMITS
 * SPT (N-value) BLOWS/0.3m

Water Content (%) and Blow Count
 10 20 30 40 50 60 70 80



Printed Feb 8 2024 15:11:43 SOIL 123316895_24-R-02 GEOTECHNICAL INVESTIGATION.GPJ NEW TEMPLATE TEST PROJECT.GPJ 2/8/24

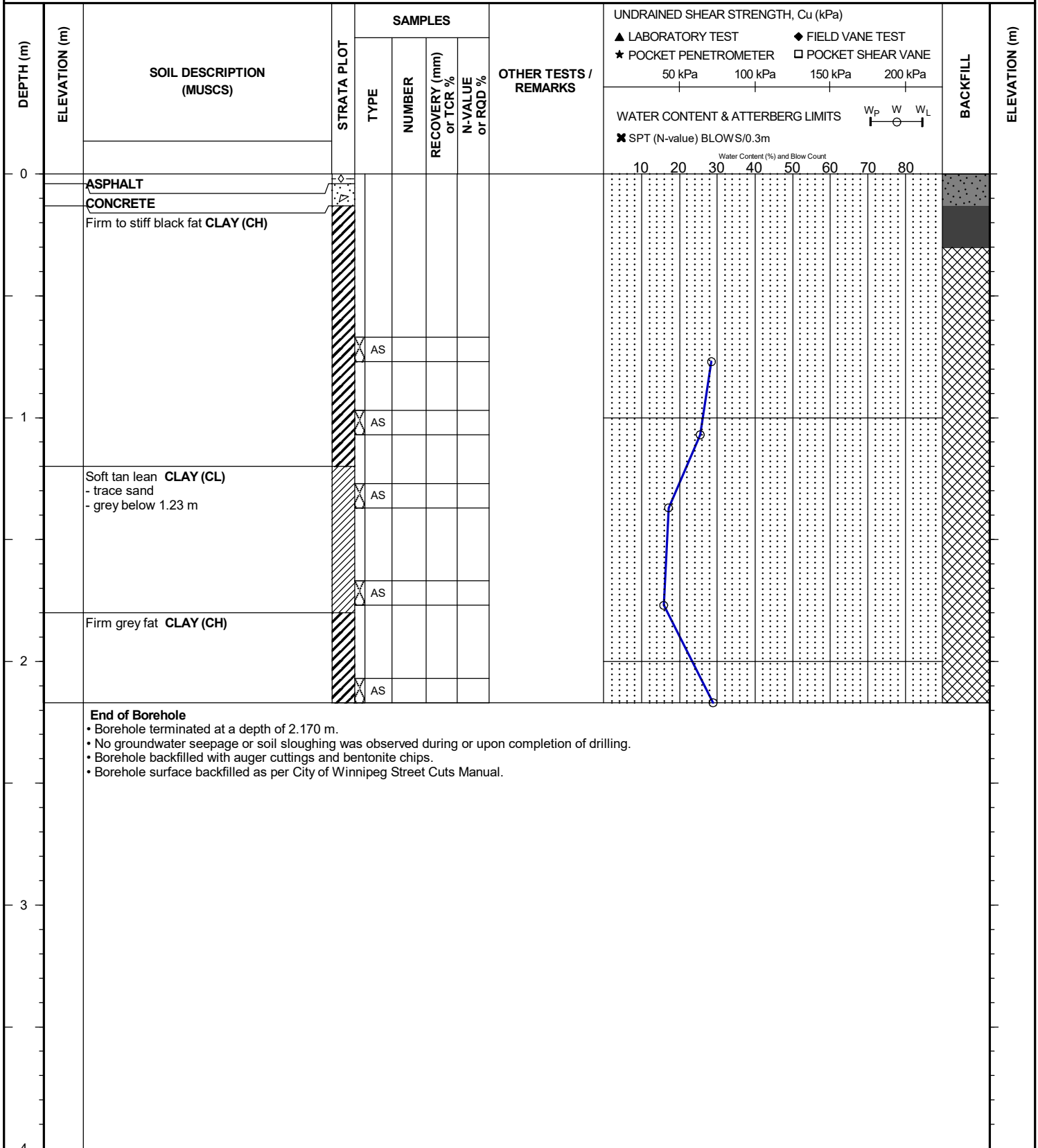
BACKFILL SYMBOL ASPHALT GROUT CONCRETE
 BENTONITE DRILL CUTTINGS SAND SLOUGH

Drilling Contractor: Maple Leaf Drilling Ltd. Logged By: LP
 Drilling Method: 125 mm SSA Reviewed By: GB
 Completion Depth: 2.175 m Page 1 of 1

CLIENT: Dillon Consulting Ltd.
 PROJECT: 24-R-02 Geotechnical Investigation
 LOCATION: McAdam Avenue
 DATE BORED: January 17 2024

PROJECT NO.: 123316895
 BH ELEVATION: N/A
 DATUM: N/A

WATER LEVEL: N/A



Printed Feb 8 2024 15:11:46 SOIL 123316895_24-R-02 GEOTECHNICAL INVESTIGATION.GPJ NEW TEMPLATE TEST PROJECT.GPJ 2/8/24

BACKFILL SYMBOL ASPHALT GROUT CONCRETE
 BENTONITE DRILL CUTTINGS SAND SLOUGH

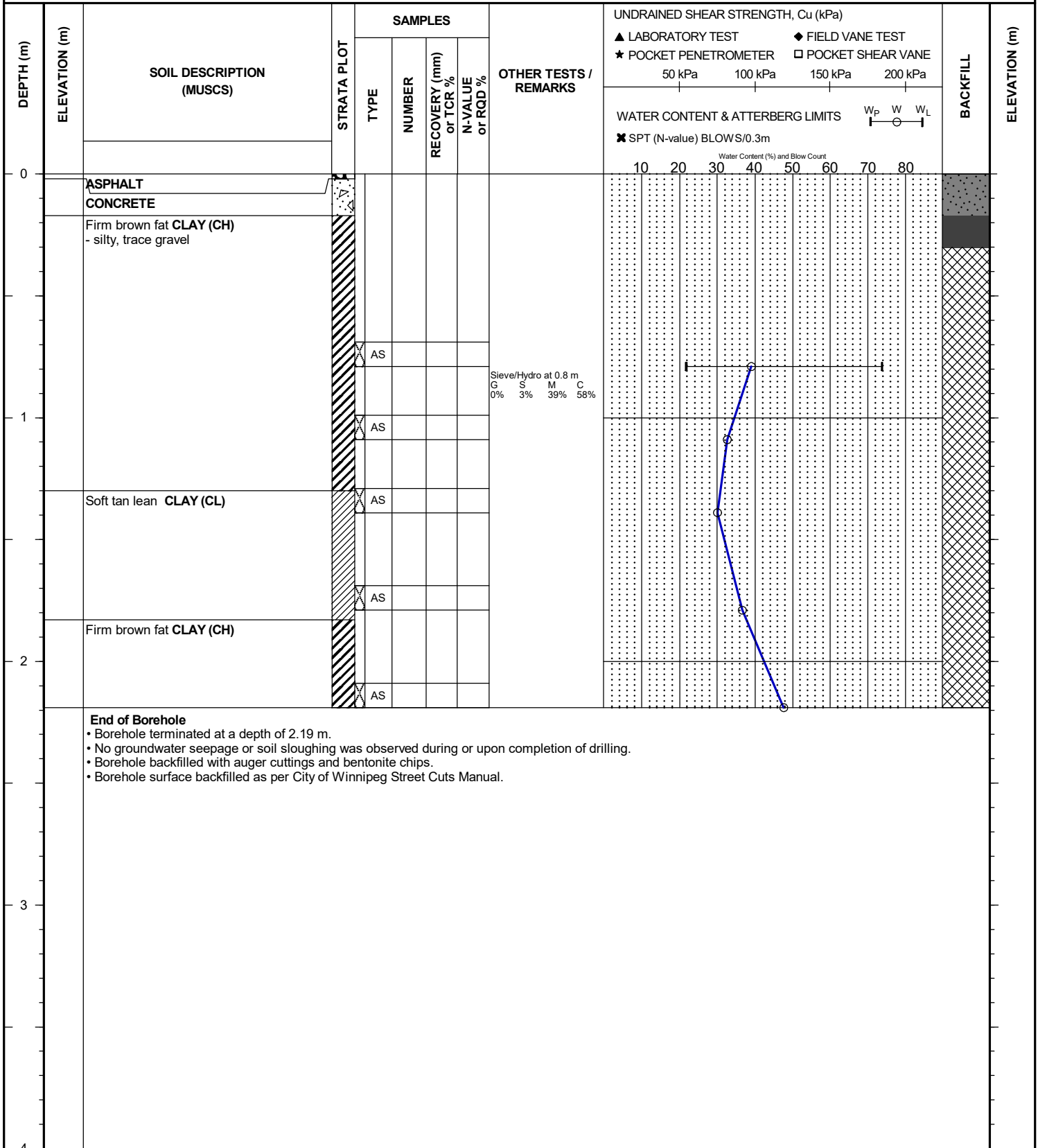
Drilling Contractor: Maple Leaf Drilling Ltd.
 Drilling Method: 125 mm SSA
 Completion Depth: 2.17 m

Logged By: KV
 Reviewed By: GB
 Page 1 of 1

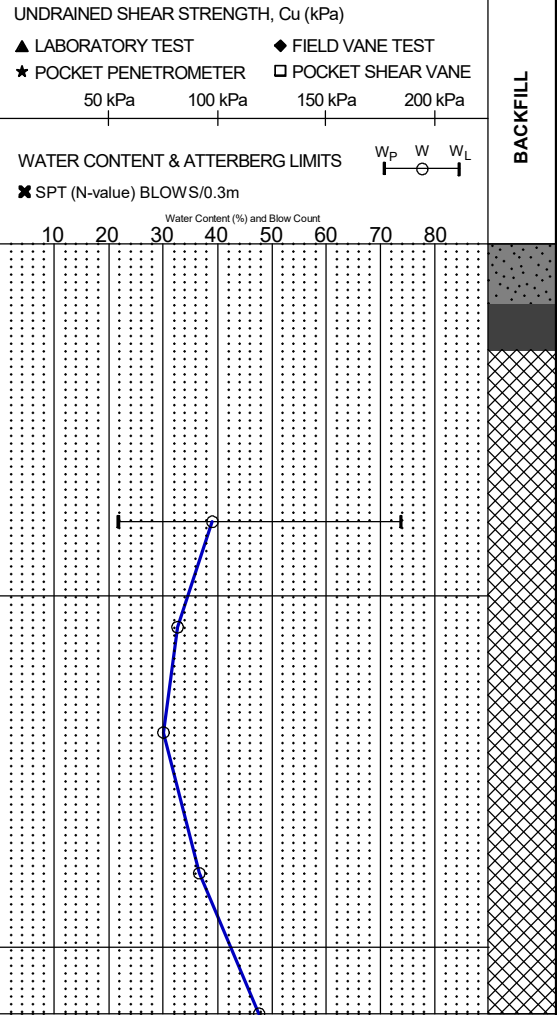
CLIENT: Dillon Consulting Ltd.
 PROJECT: 24-R-02 Geotechnical Investigation
 LOCATION: McAdam Avenue
 DATE BORED: January 17 2024

PROJECT NO.: 123316895
 BH ELEVATION: N/A
 DATUM: N/A

WATER LEVEL: N/A



Sieve/Hydro at 0.8 m
 G S M C
 0% 3% 39% 58%



Printed Feb 8 2024 15:11:46 SOIL 123316895_24-R-02 GEOTECHNICAL INVESTIGATION.GPJ NEW TEMPLATE TEST PROJECT.GPJ 2/8/24

BACKFILL SYMBOL: ASPHALT GROUT CONCRETE
 BENTONITE DRILL CUTTINGS SAND SLOUGH

Drilling Contractor: Maple Leaf Drilling Ltd. Logged By: KV
 Drilling Method: 125 mm SSA Reviewed By: GB
 Completion Depth: 2.19 m Page 1 of 1

CLIENT: Dillon Consulting Ltd.

PROJECT NO.: 123316895

PROJECT: 24-R-02 Geotechnical Investigation

BH ELEVATION: N/A

LOCATION: Gordon Avenue

DATUM: N/A

DATE BORED: January 17 2024

WATER LEVEL: N/A

DEPTH (m)	ELEVATION (m)	SOIL DESCRIPTION (MUSCS)	STRATA PLOT	SAMPLES				OTHER TESTS / REMARKS	UNDRAINED SHEAR STRENGTH, Cu (kPa)				BACKFILL	ELEVATION (m)
				TYPE	NUMBER	RECOVERY (mm) or TCR %	N-VALUE or RQD %		50 kPa	100 kPa	150 kPa	200 kPa		
0		ASPHALT												
		CONCRETE												
		Firm brown fat CLAY (CH) - silty, trace sand, trace gravel												
				AS										
1				AS										
		Soft tan lean CLAY (CL)												
				AS										
				AS										
2		Firm brown fat CLAY (CH)												
				AS										
		<p>End of Borehole</p> <ul style="list-style-type: none"> Borehole terminated at a depth of 2.255 m. No groundwater seepage or soil sloughing was observed during or upon completion of drilling. Borehole backfilled with auger cuttings and bentonite chips. Borehole surface backfilled as per City of Winnipeg Street Cuts Manual. 												

Sieve/Hydro at 0.9 m
G S M C
1% 4% 32% 63%

WATER CONTENT & ATTERBERG LIMITS

✱ SPT (N-value) BLOWS/0.3m

Water Content (%) and Blow Count

10 20 30 40 50 60 70 80

Printed Feb 8 2024 15:11:47 SOIL_123316895_24-R-02 GEOTECHNICAL INVESTIGATION.GPJ NEW TEMPLATE TEST PROJECT.GPJ 2/8/24

BACKFILL SYMBOL	ASPHALT	GROUT	CONCRETE
	BENTONITE	DRILL CUTTINGS	SAND
		SLOUGH	

Drilling Contractor: <u>Maple Leaf Drilling Ltd.</u>	Logged By: <u>KV</u>
Drilling Method: <u>125 mm SSA</u>	Reviewed By: <u>GB</u>
Completion Depth: <u>2.255 m</u>	Page <u>1 of 1</u>

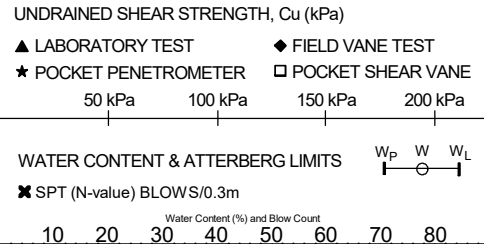
CLIENT: Dillon Consulting Ltd.
 PROJECT: 24-R-02 Geotechnical Investigation
 LOCATION: Gordon Avenue
 DATE BORED: January 17 2024

PROJECT NO.: 123316895
 BH ELEVATION: N/A
 DATUM: N/A
 WATER LEVEL: N/A

DEPTH (m)	ELEVATION (m)	SOIL DESCRIPTION (MUSCS)	STRATA PLOT	SAMPLES				OTHER TESTS / REMARKS	UNDRAINED SHEAR STRENGTH, C_u (kPa)				BACKFILL	ELEVATION (m)
				TYPE	NUMBER	RECOVERY (mm) or TCR %	N-VALUE or RQD %		50 kPa	100 kPa	150 kPa	200 kPa		
0		ASPHALT CONCRETE												
		Firm brown fat CLAY (CH) - silty, trace gravel												
1			AS											
			AS											
			AS											
2		Soft tan lean CLAY (CL)	AS											
			AS											
3														
4														

End of Borehole

- Borehole terminated at a depth of 2.17 m.
- No groundwater seepage or soil sloughing was observed during or upon completion of drilling.
- Borehole backfilled with auger cuttings and bentonite chips.
- Borehole surface backfilled as per City of Winnipeg Street Cuts Manual.



BACKFILL SYMBOL	ASPHALT	GROUT	CONCRETE
BENTONITE	DRILL CUTTINGS	SAND	SLOUGH

Drilling Contractor: Maple Leaf Drilling Ltd.	Logged By: KV
Drilling Method: 125 mm SSA	Reviewed By: GB
Completion Depth: 2.17 m	Page 1 of 1

CLIENT: Dillon Consulting Ltd.
 PROJECT: 24-R-02 Geotechnical Investigation
 LOCATION: Gordon Avenue
 DATE BORED: January 17 2024

PROJECT NO.: 123316895
 BH ELEVATION: N/A
 DATUM: N/A
 WATER LEVEL: N/A

DEPTH (m)	ELEVATION (m)	SOIL DESCRIPTION (MUSCS)	STRATA PLOT	SAMPLES				OTHER TESTS / REMARKS	UNDRAINED SHEAR STRENGTH, Cu (kPa)				BACKFILL	ELEVATION (m)
				TYPE	NUMBER	RECOVERY (mm) or TCR %	N-VALUE or RQD %		50 kPa	100 kPa	150 kPa	200 kPa		
0		ASPHALT												
		CONCRETE												
		Firm brown fat CLAY (CH) - silty, trace sand, trace gravel												
				AS										
1		Soft tan lean CLAY (CL)												
				AS										
		Firm brown fat CLAY (CH)												
2				AS										
		End of Borehole • Borehole terminated at a depth of 2.19 m. • No groundwater seepage or soil sloughing was observed during or upon completion of drilling. • Borehole backfilled with auger cuttings and bentonite chips. • Borehole surface backfilled as per City of Winnipeg Street Cuts Manual.												

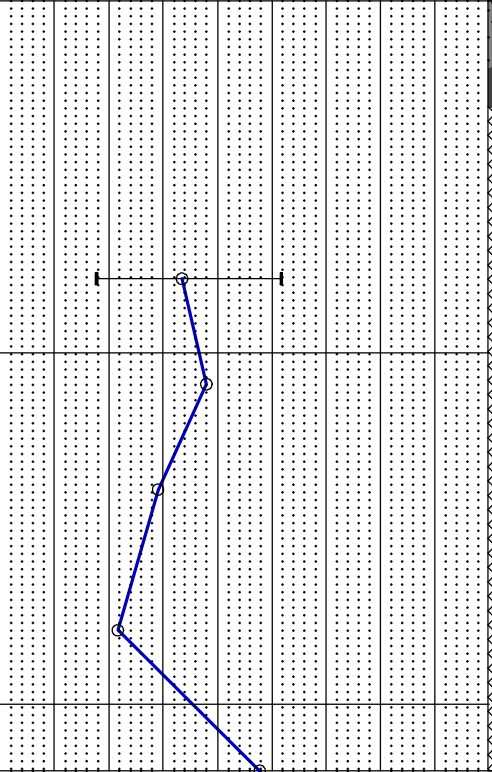
Sieve/Hydro at 0.8 m
 G S M C
 2% 7% 48% 43%

UNDRAINED SHEAR STRENGTH, Cu (kPa)
 ▲ LABORATORY TEST ◆ FIELD VANE TEST
 ★ POCKET PENETROMETER □ POCKET SHEAR VANE
 50 kPa 100 kPa 150 kPa 200 kPa

WATER CONTENT & ATTERBERG LIMITS W_p W W_L

✖ SPT (N-value) BLOWS/0.3m

Water Content (%) and Blow Count



BACKFILL SYMBOL ASPHALT GROUT CONCRETE
 BENTONITE DRILL CUTTINGS SAND SLOUGH

Drilling Contractor: Maple Leaf Drilling Ltd. Logged By: KV
 Drilling Method: 125 mm SSA Reviewed By: GB
 Completion Depth: 2.19 m Page 1 of 1

APPENDIX D

Core Photographs



Figure 1 – Core No. 40 (Carruthers Ave)



Figure 2 – Core No. 41 (Carruthers Ave)



Figure 3 – Core No. 42 (Carruthers Ave)



Figure 4 – Core No. 43 (McAdam Ave)



Figure 5 – Core No. 44 (McAdam Ave)



Figure 6 – Core No. 45 (McAdam Ave)



Figure 7 – Core No. 46 (Gordon Ave)



Figure 8 – Core No. 47 (Gordon Ave)



Figure 9 – Core No. 48 (Gordon Ave)

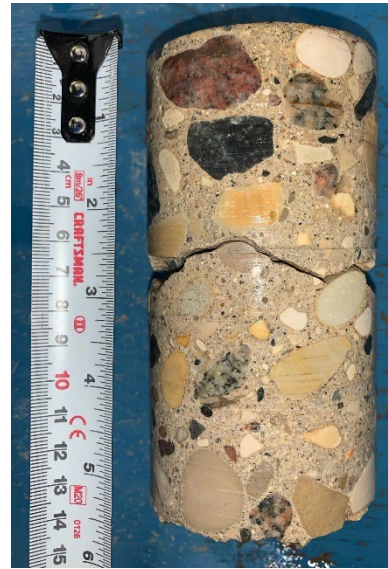


Figure 10 – Core No. 49 (Rudolph Bay)



Figure 11 – Core No. 50 (Rudolph Bay)



Figure 12 – Core No. 51 (Rudolph Bay)



Figure 13 – Core No. 52 (Rudolph Bay)



Figure 14 – Core No. 53 (Dahlia Alley)



Figure 15 – Core No. 54 (Dahlia Alley)



Figure 16 – Core No. 55 (Hood Ave)



Figure 17 – Core No. 56 (Hood Ave)



Figure 18 – Core No. 57 (Fortier Ave)



Figure 19 – Core No. 58 (Fortier Ave)



Figure 20 – Core No. 59 (Summerfield Way)



Figure 21 – Core No. 60 (Summerfield Way)



Figure 22 – Core No. 61 (Summerfield Way)



Figure 23 – Core No. 62 (Summerfield Way)



Figure 24 – Core No. 63 (Summerfield Way)



Figure 25 – Core No. 64 (Summerfield Way)



Figure 26 – Core No. 65 (Summerfield Way)



Figure 27 – Core No. 66 (Tranquility Cove)



Figure 28 – Core No. 67 (Tranquility Cove)



Figure 29 – Core No. 68 (Tranquility Cove)



Figure 30 – Core No. 69 (Snowdon Ave)



Figure 31 – Core No. 70 (Snowdon Ave)



Figure 32 – Core No. 71 (Snowdon Ave)



Figure 33 – Core No. 72 (Snowdon Ave)



Figure 34 – Core No. 73 (Snowdon Ave)



Figure 35 – Core No. 74 (Dearborn Ave)



Figure 36 – Core No. 75 (Dearborn Ave)



Figure 37 – Core No. 76 (Lacy St)



Figure 38 – Core No. 77 (Lacy St)



Figure 39 – Core No. 78 (Norilyn Bay)



Figure 40 – Core No. 79 (Norilyn Bay)



Figure 41 – Core No. 80 (Norilyn Bay)



Figure 42 – Core No. 81 (Norilyn Bay)



Figure 43 – Core No. 82 (Kullman St)



Figure 44 – Core No. 83 (Kullman St)

APPENDIX E

Laboratory Test Reports

ASTM D4318 - LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX OF SOILS (LL METHOD B - ONE-POINT)

TO Dillon Consulting Ltd.
 300 - 100 Innovation Drive
 Winnipeg, Manitoba
 R3T 6A8

PROJECT 24-R-02 - Local Street Package - Geotechnical Investigation

PROJECT NO. 123316892

ATTN Ali Campbell

REPORT NO. 1

DATE SAMPLED: 2024.Jan.16

DATE RECEIVED: 2024.Jan.16

DATE TESTED: 2024.Jan.30

SAMPLED BY: Stantec Consulting Ltd.

SUBMITTED BY: Stantec Consulting Ltd.

TESTED BY: Larry Presado

MATERIAL IDENTIFICATION

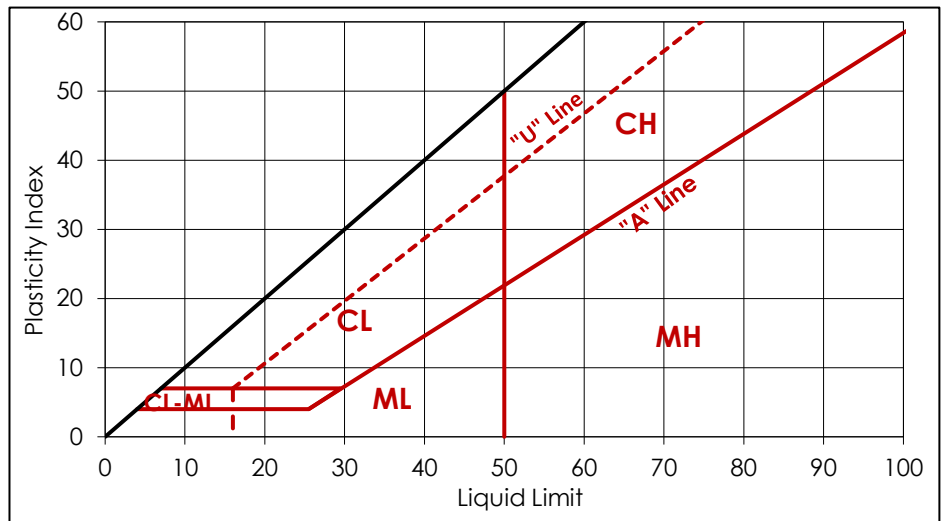
CLIENT FIELD ID BH-41, 775 mm

STANTEC SAMPLE NO. 2982

TRIAL	LIQUID LIMIT	
	1	2
BLOWS	22	22
MC (%)	91	94

TRIAL	PLASTIC LIMIT	
	1	2
MC (%)	29	30

LIQUID LIMIT, LL	91
PLASTIC LIMIT, PL	29
PLASTICITY INDEX, PI	61
AS REC'D MC (%)	41.77



COMMENTS
 No comments.



REPORT DATE 2024.Jan.31

REVIEWED BY Guillaume Beauce, P.Eng.
 Geotechnical Engineer - Materials Testing Services

ASTM D4318 - LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX OF SOILS (LL METHOD B - ONE-POINT)

TO Dillon Consulting Ltd.
 300 - 100 Innovation Drive
 Winnipeg, Manitoba
 R3T 6A8

PROJECT 24-R-02 - Local Street Package - Geotechnical Investigation

PROJECT NO. 123316892

ATTN Ali Campbell

REPORT NO. 2

DATE SAMPLED: 2024.Jan.16
 SAMPLED BY: Stantec Consulting Ltd.

DATE RECEIVED: 2024.Jan.16
 SUBMITTED BY: Stantec Consulting Ltd.

DATE TESTED: 2024.Jan.30
 TESTED BY: Larry Presado

MATERIAL IDENTIFICATION

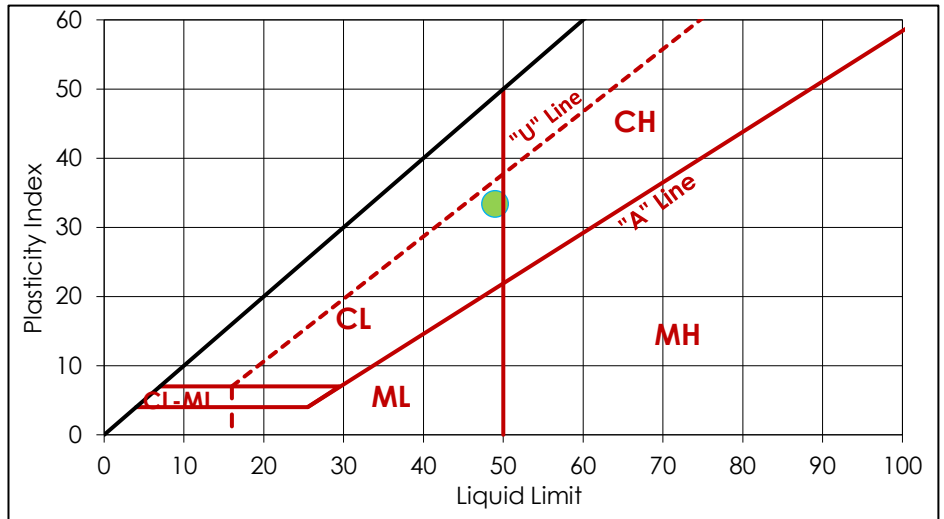
CLIENT FIELD ID BH-42, 740 mm

STANTEC SAMPLE NO. 2983

TRIAL	LIQUID LIMIT	
	1	2
BLOWS	24	24
MC (%)	49	50

TRIAL	PLASTIC LIMIT	
	1	2
MC (%)	16	15

LIQUID LIMIT, LL	49
PLASTIC LIMIT, PL	16
PLASTICITY INDEX, PI	33
AS REC'D MC (%)	26.33



COMMENTS
 No comments.

REPORT DATE 2024.Jan.31


 REVIEWED BY Guillaume Beauce, P.Eng.
 Geotechnical Engineer - Materials Testing Services

ASTM D4318 - LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX OF SOILS (LL METHOD B - ONE-POINT)

TO Dillon Consulting Ltd.
 300 - 100 Innovation Drive
 Winnipeg, Manitoba
 R3T 6A8

PROJECT 24-R-02 - Local Street Package - Geotechnical Investigation

PROJECT NO. 123316892

ATTN Ali Campbell

REPORT NO. 3

DATE SAMPLED: 2024.Jan.17
 SAMPLED BY: Stantec Consulting Ltd.

DATE RECEIVED: 2024.Jan.17
 SUBMITTED BY: Stantec Consulting Ltd.

DATE TESTED: 2024.Jan.31
 TESTED BY: Larry Presado

MATERIAL IDENTIFICATION

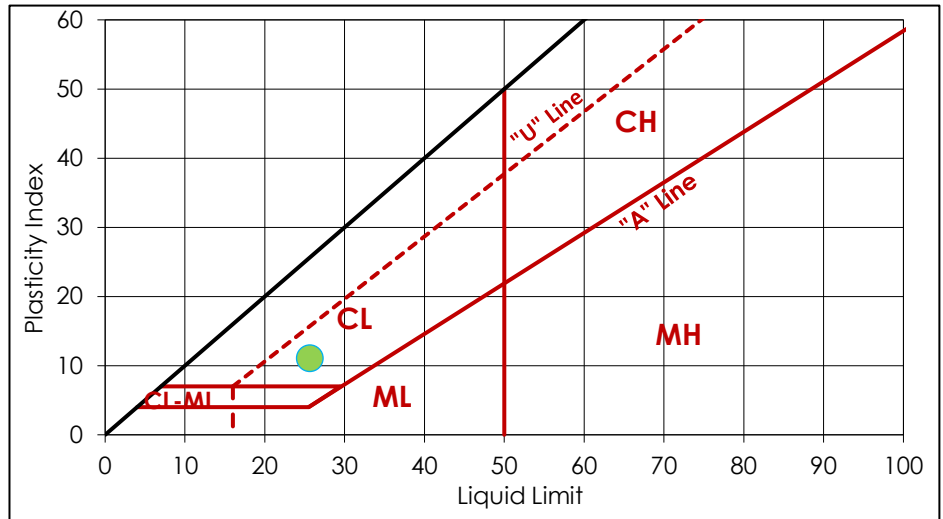
CLIENT FIELD ID BH-43, 775 mm

STANTEC SAMPLE NO. 4002

TRIAL	LIQUID LIMIT	
	1	2
BLOWS	23	23
MC (%)	26	26

TRIAL	PLASTIC LIMIT	
	1	2
MC (%)	15	14

LIQUID LIMIT, LL	26
PLASTIC LIMIT, PL	15
PLASTICITY INDEX, PI	11
AS REC'D MC (%)	13.60



COMMENTS
 No comments.



REPORT DATE 2024.Feb.01

REVIEWED BY Guillaume Beauce, P.Eng.
 Geotechnical Engineer - Materials Testing Services

ASTM D4318 - LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX OF SOILS (LL METHOD B - ONE-POINT)

TO Dillon Consulting Ltd.
 300 - 100 Innovation Drive
 Winnipeg, Manitoba
 R3T 6A8

PROJECT 24-R-02 - Local Street Package - Geotechnical Investigation

PROJECT NO. 123316892

ATTN Ali Campbell

REPORT NO. 4

DATE SAMPLED: 2024.Jan.17
 SAMPLED BY: Stantec Consulting Ltd.

DATE RECEIVED: 2024.Jan.17
 SUBMITTED BY: Stantec Consulting Ltd.

DATE TESTED: 2024.Feb.01
 TESTED BY: Larry Presado

MATERIAL IDENTIFICATION

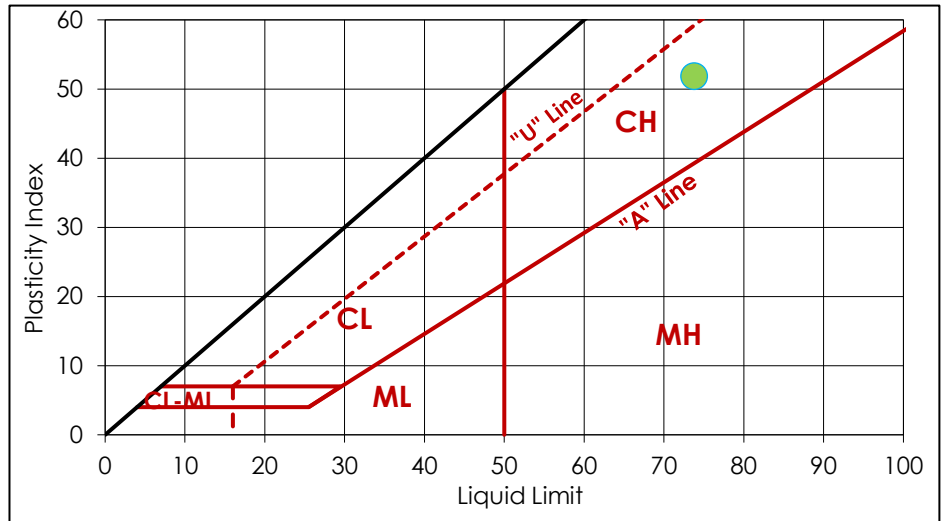
CLIENT FIELD ID BH-45, 790 mm

STANTEC SAMPLE NO. 4003

TRIAL	LIQUID LIMIT	
	1	2
BLOWS	22	22
MC (%)	75	75

TRIAL	PLASTIC LIMIT	
	1	2
MC (%)	22	22

LIQUID LIMIT, LL	74
PLASTIC LIMIT, PL	22
PLASTICITY INDEX, PI	52
AS REC'D MC (%)	39.60



COMMENTS
 No comments.



REPORT DATE 2024.Feb.02

REVIEWED BY Guillaume Beauce, P.Eng.
 Geotechnical Engineer - Materials Testing Services

ASTM D4318 - LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX OF SOILS (LL METHOD B - ONE-POINT)

TO Dillon Consulting Ltd.
 300 - 100 Innovation Drive
 Winnipeg, Manitoba
 R3T 6A8

PROJECT 24-R-02 - Local Street Package - Geotechnical Investigation

PROJECT NO. 123316892

ATTN Ali Campbell

REPORT NO. 5

DATE SAMPLED: 2024.Jan.17
 SAMPLED BY: Stantec Consulting Ltd.

DATE RECEIVED: 2024.Jan.17
 SUBMITTED BY: Stantec Consulting Ltd.

DATE TESTED: 2024.Feb.01
 TESTED BY: Larry Presado

MATERIAL IDENTIFICATION

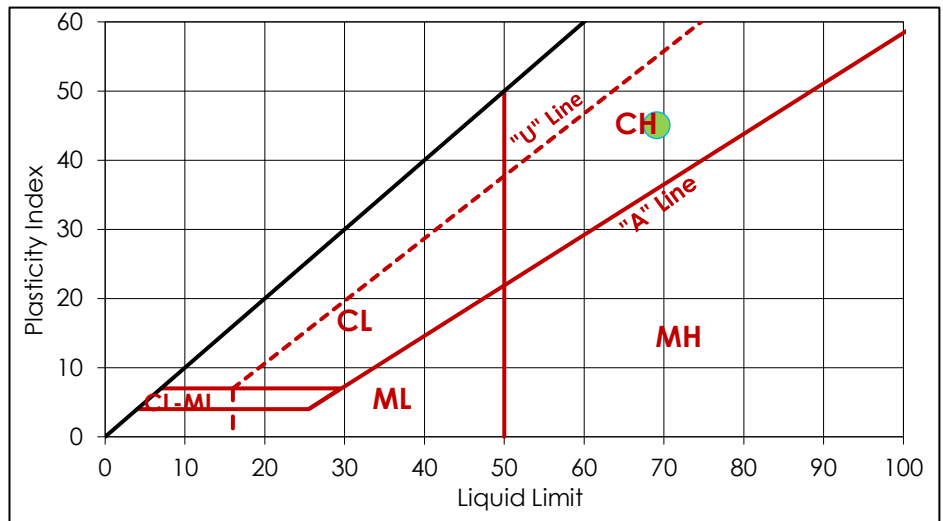
CLIENT FIELD ID BH-46, 855 mm

STANTEC SAMPLE NO. 4004

	LIQUID LIMIT	
TRIAL	1	2
BLOWS	27	28
MC (%)	69	68

	PLASTIC LIMIT	
TRIAL	1	2
MC (%)	24	24

LIQUID LIMIT, LL	69
PLASTIC LIMIT, PL	24
PLASTICITY INDEX, PI	45
AS REC'D MC (%)	34.70



COMMENTS
 No comments.

REPORT DATE 2024.Feb.02


 REVIEWED BY Guillaume Beauce, P.Eng.
 Geotechnical Engineer - Materials Testing Services

ASTM D4318 - LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX OF SOILS (LL METHOD B - ONE-POINT)

TO Dillon Consulting Ltd.
 300 - 100 Innovation Drive
 Winnipeg, Manitoba
 R3T 6A8

PROJECT 24-R-02 - Local Street Package - Geotechnical Investigation

PROJECT NO. 123316892

ATTN Ali Campbell

REPORT NO. 6

DATE SAMPLED: 2024.Jan.17
 SAMPLED BY: Stantec Consulting Ltd.

DATE RECEIVED: 2024.Jan.17
 SUBMITTED BY: Stantec Consulting Ltd.

DATE TESTED: 2024.Feb.01
 TESTED BY: Larry Presado

MATERIAL IDENTIFICATION

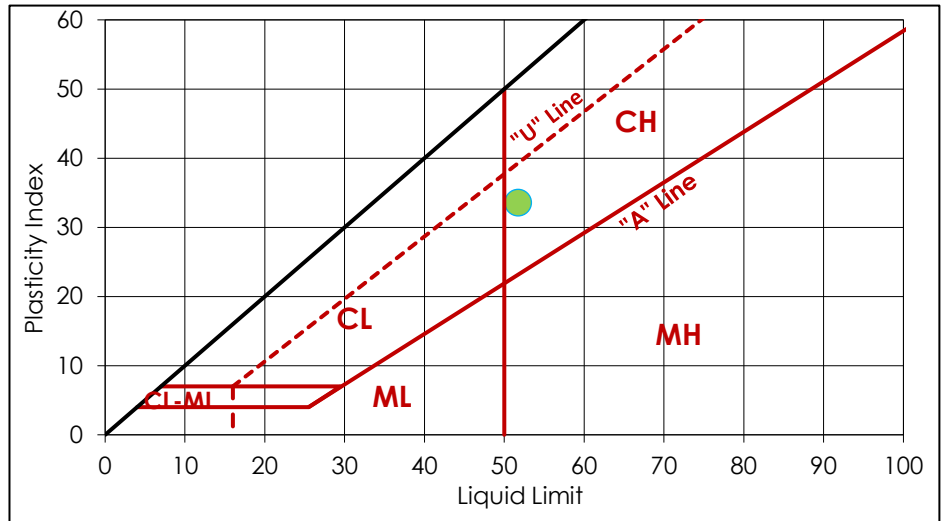
CLIENT FIELD ID BH-48, 790 mm

STANTEC SAMPLE NO. 4005

TRIAL	LIQUID LIMIT	
	1	2
BLOWS	25	26
MC (%)	52	52

TRIAL	PLASTIC LIMIT	
	1	2
MC (%)	19	18

LIQUID LIMIT, LL	52
PLASTIC LIMIT, PL	18
PLASTICITY INDEX, PI	34
AS REC'D MC (%)	34.00



COMMENTS
 No comments.



REPORT DATE 2024.Feb.02

REVIEWED BY Guillaume Beauce, P.Eng.
 Geotechnical Engineer - Materials Testing Services

ASTM D7928 - PARTICLE-SIZE DISTRIBUTION OF FINE-GRAINED SOILS USING THE SEDIMENTATION ANALYSIS

TO Dillon Consulting Ltd.
 300 - 100 Innovation Drive
 Winnipeg, Manitoba
 R3T 6A8

PROJECT 24-R-02 - Local Streets Package -
 Geotechnical Investigation

PROJECT NO. 123316895

ATTN Ali Campbell

REPORT NO. 1

DATE SAMPLED: 2024.Jan.16

DATE RECEIVED: 2024.Jan.16

DATE TESTED: 2024.Jan.23

SAMPLED BY: Stantec Consulting Ltd.

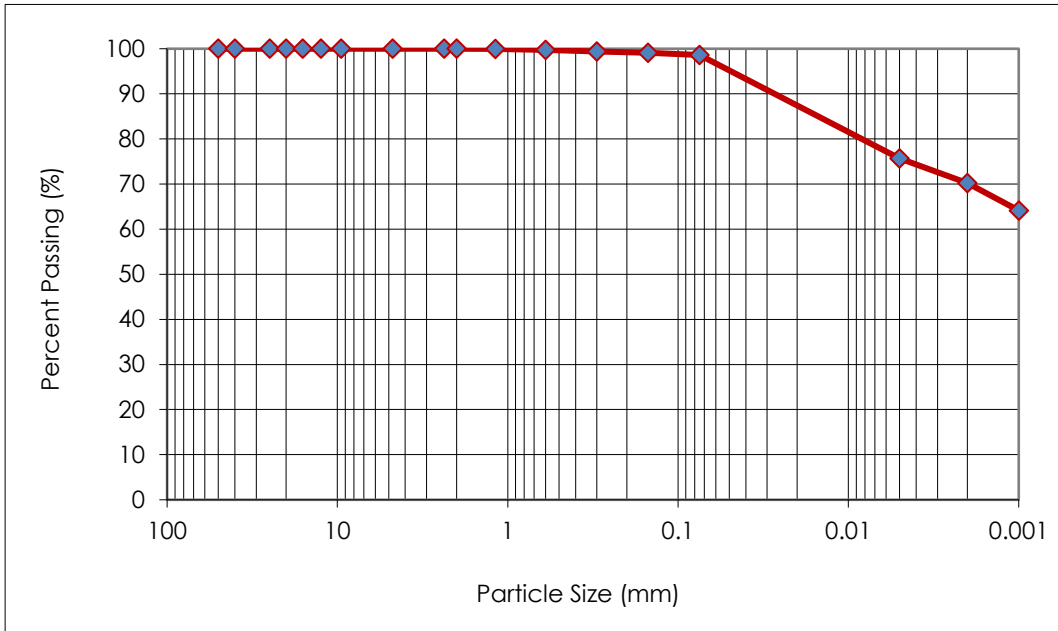
SUBMITTED BY: Stantec Consulting Ltd.

TESTED BY: Larry Presado

MATERIAL IDENTIFICATION

CLIENT FIELD ID BH-41, 775 mm

STANTEC SAMPLE NO. 2982



Sieve Size (mm)	% Passing
50.0	100.0
40.0	100.0
25.0	100.0
20.0	100.0
16.0	100.0
12.5	100.0
9.5	100.0
4.75	100.0
2.36	100.0
2.00	100.0
1.18	99.9
0.600	99.7
0.300	99.4
0.150	99.1
0.075	98.6
0.005	75.7
0.002	70.2
0.001	64.1

Gravel	Sand			Silt	Clay	Colloids
	Coarse	Medium	Fine			
0.0	0.0	0.5	0.9	28.4	70.2	64.1

COMMENTS
 No comments.



REPORT DATE 2024.Jan.25

REVIEWED BY Guillaume Beauce, P.Eng.
 Geotechnical Engineer - Materials Testing Services

ASTM D7928 - PARTICLE-SIZE DISTRIBUTION OF FINE-GRAINED SOILS USING THE SEDIMENTATION ANALYSIS

TO Dillon Consulting Ltd.
 300 - 100 Innovation Drive
 Winnipeg, Manitoba
 R3T 6A8

PROJECT 24-R-02 - Local Streets Package -
 Geotechnical Investigation

PROJECT NO. 123316895

ATTN Ali Campbell

REPORT NO. 2

DATE SAMPLED: 2024.Jan.16

DATE RECEIVED: 2024.Jan.16

DATE TESTED: 2024.Jan.23

SAMPLED BY: Stantec Consulting Ltd.

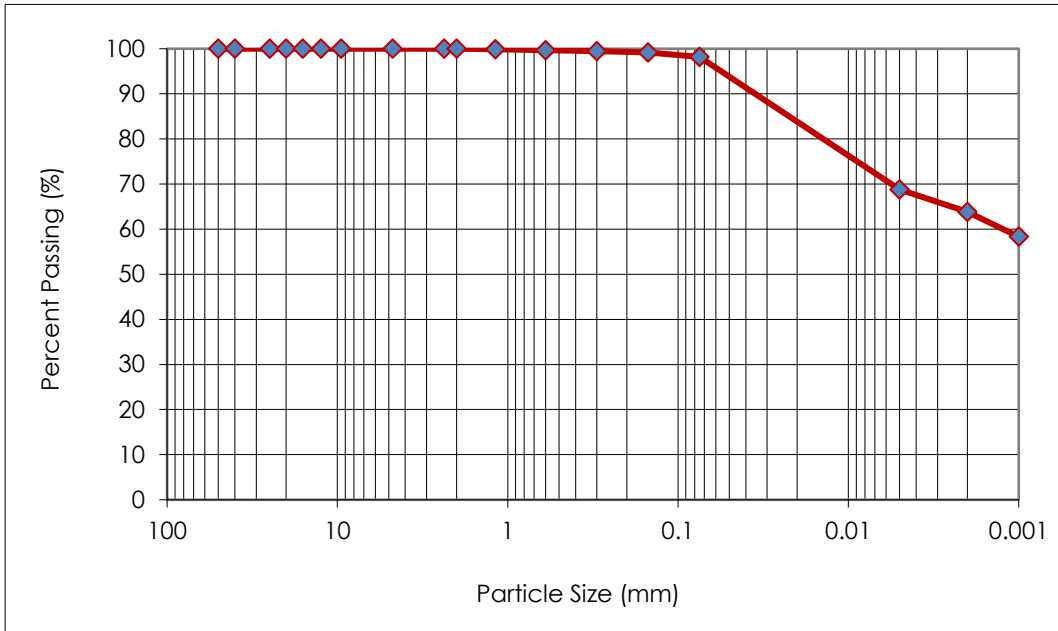
SUBMITTED BY: Stantec Consulting Ltd.

TESTED BY: Larry Presado

MATERIAL IDENTIFICATION

CLIENT FIELD ID BH-42, 740 mm

STANTEC SAMPLE NO. 2983



Sieve Size (mm)	% Passing
50.0	100.0
40.0	100.0
25.0	100.0
20.0	100.0
16.0	100.0
12.5	100.0
9.5	100.0
4.75	100.0
2.36	100.0
2.00	100.0
1.18	99.9
0.600	99.7
0.300	99.5
0.150	99.2
0.075	98.2
0.005	68.8
0.002	63.8
0.001	58.3

Gravel	Sand			Silt	Clay	Colloids
	Coarse	Medium	Fine			
0.0	0.0	0.4	1.4	34.4	63.8	58.3

COMMENTS
 No comments.



REPORT DATE 2024.Jan.25

REVIEWED BY Guillaume Beauce, P.Eng.
 Geotechnical Engineer - Materials Testing Services

ASTM D7928 - PARTICLE-SIZE DISTRIBUTION OF FINE-GRAINED SOILS USING THE SEDIMENTATION ANALYSIS

TO Dillon Consulting Ltd.
 300 - 100 Innovation Drive
 Winnipeg, Manitoba
 R3T 6A8

PROJECT 24-R-02 - Local Streets Package -
 Geotechnical Investigation

PROJECT NO. 123316895

ATTN Ali Campbell

REPORT NO. 3

DATE SAMPLED: 2024.Jan.17

DATE RECEIVED: 2024.Jan.17

DATE TESTED: 2024.Jan.25

SAMPLED BY: Stantec Consulting Ltd.

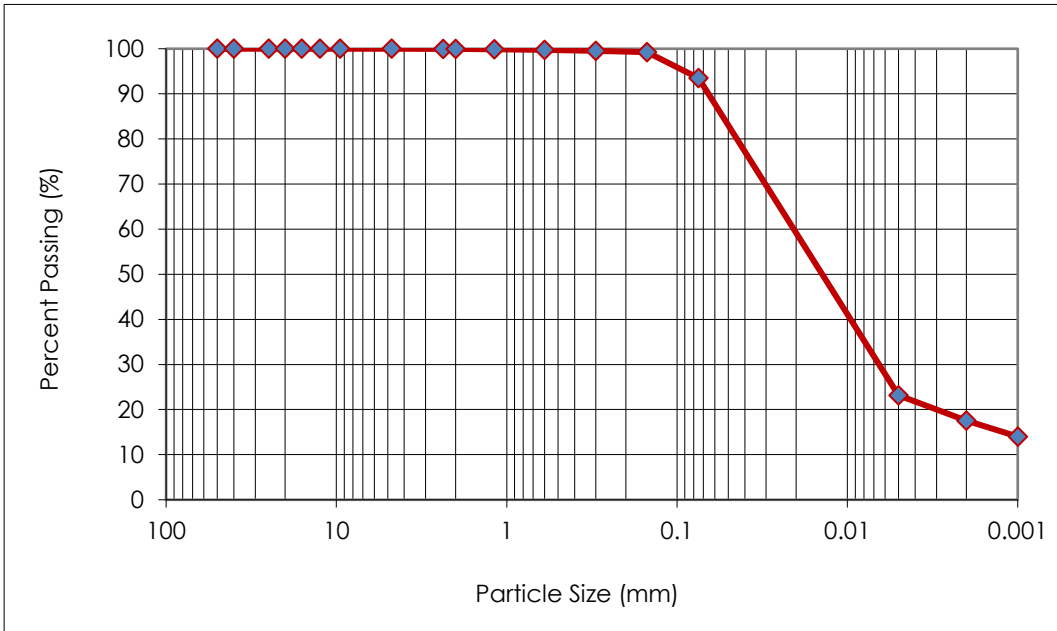
SUBMITTED BY: Stantec Consulting Ltd.

TESTED BY: Larry Presado

MATERIAL IDENTIFICATION

CLIENT FIELD ID BH-43, 775 mm

STANTEC SAMPLE NO. 4002



Sieve Size (mm)	% Passing
50.0	100.0
40.0	100.0
25.0	100.0
20.0	100.0
16.0	100.0
12.5	100.0
9.5	100.0
4.75	100.0
2.36	100.0
2.00	100.0
1.18	99.9
0.600	99.8
0.300	99.6
0.150	99.3
0.075	93.5
0.005	23.2
0.002	17.6
0.001	14.0

Gravel	Sand			Silt	Clay	Colloids
	Coarse	Medium	Fine			
0.0	0.0	0.4	6.1	75.9	17.6	14.0

COMMENTS
 No comments.



REPORT DATE 2024.Jan.29

REVIEWED BY Guillaume Beauce, P.Eng.
 Geotechnical Engineer - Materials Testing Services

ASTM D7928 - PARTICLE-SIZE DISTRIBUTION OF FINE-GRAINED SOILS USING THE SEDIMENTATION ANALYSIS

TO Dillon Consulting Ltd.
 300 - 100 Innovation Drive
 Winnipeg, Manitoba
 R3T 6A8

PROJECT 24-R-02 - Local Streets Package -
 Geotechnical Investigation

PROJECT NO. 123316895

ATTN Ali Campbell

REPORT NO. 4

DATE SAMPLED: 2024.Jan.17

DATE RECEIVED: 2024.Jan.17

DATE TESTED: 2024.Jan.25

SAMPLED BY: Stantec Consulting Ltd.

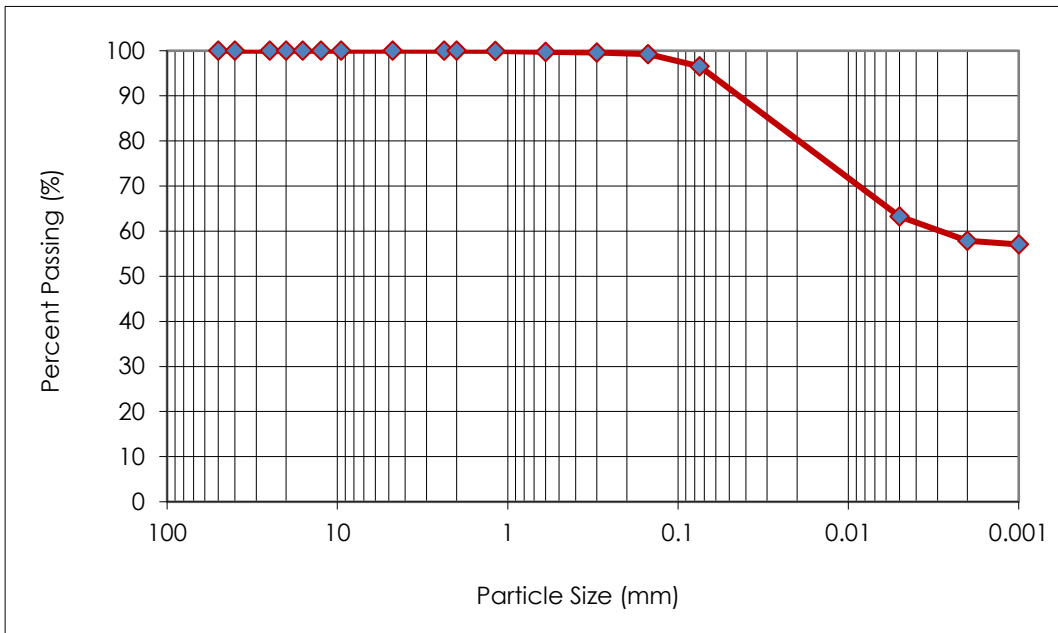
SUBMITTED BY: Stantec Consulting Ltd.

TESTED BY: Larry Presado

MATERIAL IDENTIFICATION

CLIENT FIELD ID BH-45, 790 mm

STANTEC SAMPLE NO. 4003



Sieve Size (mm)	% Passing
50.0	100.0
40.0	100.0
25.0	100.0
20.0	100.0
16.0	100.0
12.5	100.0
9.5	100.0
4.75	100.0
2.36	100.0
2.00	100.0
1.18	99.9
0.600	99.8
0.300	99.6
0.150	99.3
0.075	96.6
0.005	63.3
0.002	57.9
0.001	57.1

Gravel	Sand			Silt	Clay	Colloids
	Coarse	Medium	Fine			
0.0	0.0	0.3	3.1	38.7	57.9	57.1

COMMENTS
 No comments.



REPORT DATE 2024.Jan.29

REVIEWED BY Guillaume Beauce, P.Eng.
 Geotechnical Engineer - Materials Testing Services

ASTM D7928 - PARTICLE-SIZE DISTRIBUTION OF FINE-GRAINED SOILS USING THE SEDIMENTATION ANALYSIS

TO Dillon Consulting Ltd.
 300 - 100 Innovation Drive
 Winnipeg, Manitoba
 R3T 6A8

PROJECT 24-R-02 - Local Streets Package -
 Geotechnical Investigation

PROJECT NO. 123316895

ATTN Ali Campbell

REPORT NO. 5

DATE SAMPLED: 2024.Jan.17

DATE RECEIVED: 2024.Jan.17

DATE TESTED: 2024.Jan.25

SAMPLED BY: Stantec Consulting Ltd.

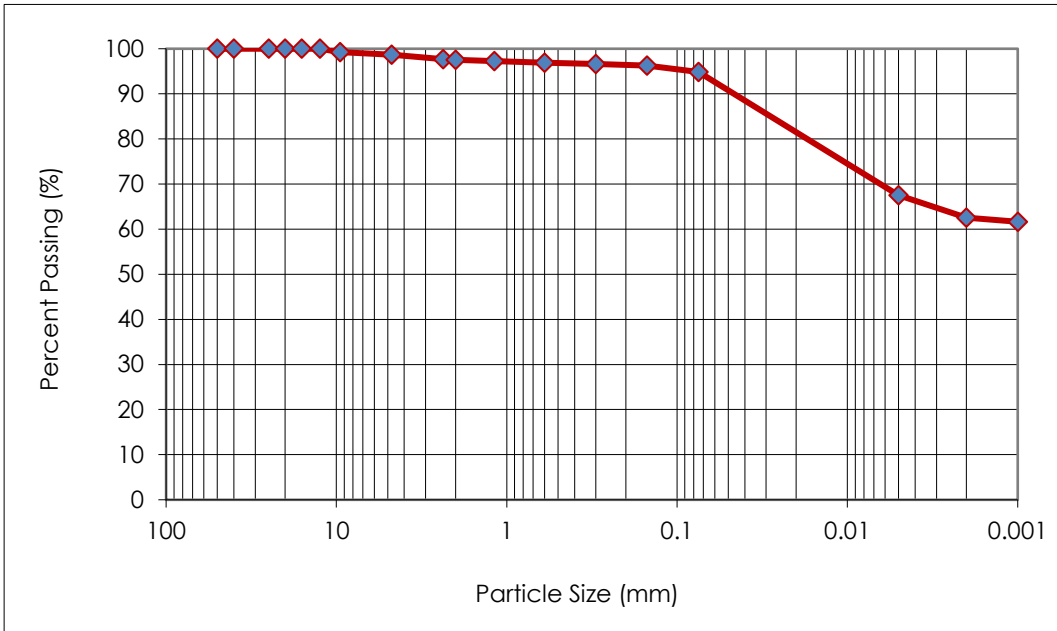
SUBMITTED BY: Stantec Consulting Ltd.

TESTED BY: Larry Presado

MATERIAL IDENTIFICATION

CLIENT FIELD ID BH-46, 855 mm

STANTEC SAMPLE NO. 4004



Sieve Size (mm)	% Passing
50.0	100.0
40.0	100.0
25.0	100.0
20.0	100.0
16.0	100.0
12.5	100.0
9.5	99.3
4.75	98.7
2.36	97.7
2.00	97.5
1.18	97.2
0.600	96.9
0.300	96.6
0.150	96.3
0.075	94.9
0.005	67.5
0.002	62.6
0.001	61.6

Gravel	Sand			Silt	Clay	Colloids
	Coarse	Medium	Fine			
1.3	1.2	0.8	1.8	32.3	62.6	61.6

COMMENTS
 No comments.



REPORT DATE 2024.Jan.29

REVIEWED BY Guillaume Beauce, P.Eng.
 Geotechnical Engineer - Materials Testing Services

ASTM D7928 - PARTICLE-SIZE DISTRIBUTION OF FINE-GRAINED SOILS USING THE SEDIMENTATION ANALYSIS

TO Dillon Consulting Ltd.
 300 - 100 Innovation Drive
 Winnipeg, Manitoba
 R3T 6A8

PROJECT 24-R-02 - Local Streets Package -
 Geotechnical Investigation

PROJECT NO. 123316895

ATTN Ali Campbell

REPORT NO. 6

DATE SAMPLED: 2024.Jan.17

DATE RECEIVED: 2024.Jan.17

DATE TESTED: 2024.Jan.25

SAMPLED BY: Stantec Consulting Ltd.

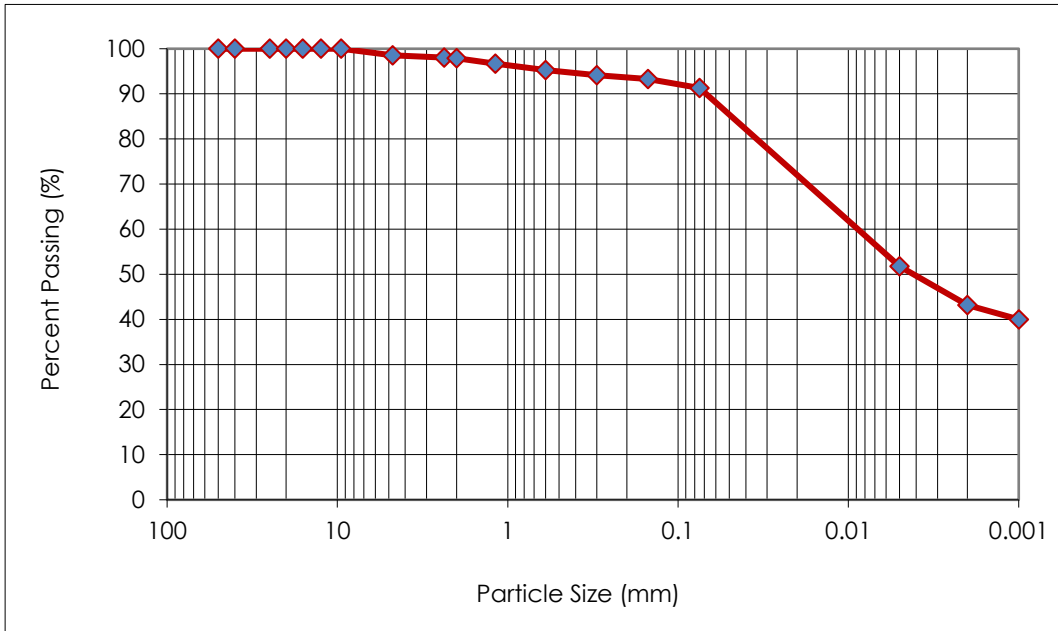
SUBMITTED BY: Stantec Consulting Ltd.

TESTED BY: Larry Presado

MATERIAL IDENTIFICATION

CLIENT FIELD ID BH-48, 790 mm

STANTEC SAMPLE NO. 4005



Sieve Size (mm)	% Passing
50.0	100.0
40.0	100.0
25.0	100.0
20.0	100.0
16.0	100.0
12.5	100.0
9.5	100.0
4.75	98.5
2.36	98.0
2.00	97.9
1.18	96.7
0.600	95.3
0.300	94.1
0.150	93.3
0.075	91.3
0.005	51.8
0.002	43.2
0.001	40.0

Gravel	Sand			Silt	Clay	Colloids
	Coarse	Medium	Fine			
1.5	0.6	3.3	3.3	48.1	43.2	40.0

COMMENTS
 No comments.



REPORT DATE 2024.Jan.29

REVIEWED BY Guillaume Beauce, P.Eng.
 Geotechnical Engineer - Materials Testing Services

PROCTOR TEST REPORT

TO Dillon Consulting Ltd.
 300 - 100 Innovation Dr.
 Winnipeg, MB
 R3T 6A8

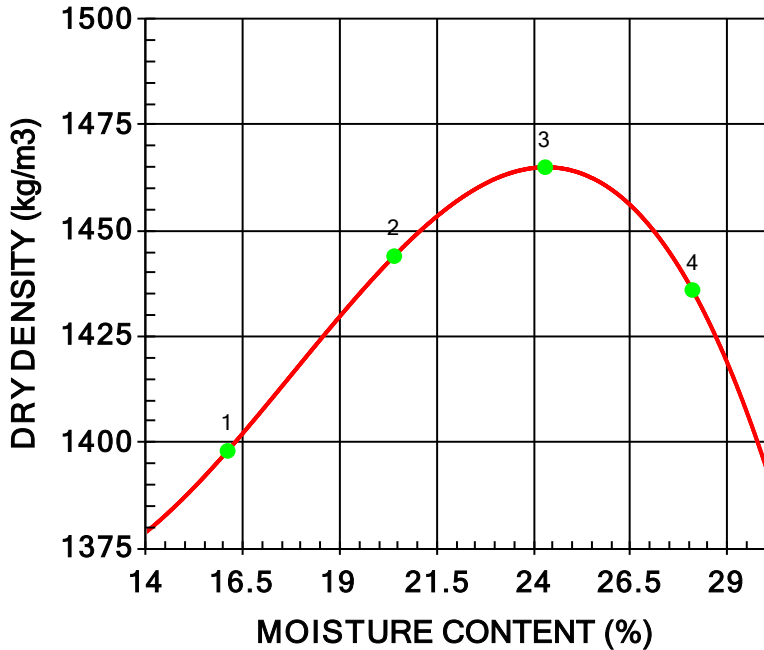
CLIENT Dillon Consulting Ltd.
 C.C.

ATTN: Ali Campbell

PROJECT 24-R-02 Local Streets Package

PROJECT NO. 123316895
 PROCTOR NO. 1 DATE SAMPLED 2024.Jan.16 DATE RECEIVED 2024.Jan.16 DATE TESTED 2024.Jan.26

INSITU MOISTURE	29.3 %	COMPACTION STANDARD	Standard Proctor, ASTM D698
TESTED BY	Donald Eliazar	COMPACTION PROCEDURE	A: 101.6mm Mold, Passing 4.75mm
MATERIAL IDENTIFICATION		RAMMER TYPE	Automatic
MAJOR COMPONENT	Subgrade	PREPARATION	Dry
SIZE		OVERSIZE CORRECTION METHOD	None
DESCRIPTION	Fat CLAY (CH)	RETAINED 4.75mm SCREEN	N/A %
SUPPLIER	Existing Material		
SOURCE	Carruthers Ave - BH-41, 0.775 m		



TRIAL NUMBER	WET DENSITY (kg/m³)	DRY DENSITY (kg/m³)	MOISTURE CONTENT (%)
1	1623	1398	16.1
2	1738	1444	20.4
3	1821	1465	24.3
4	1839	1436	28.1

	MAXIMUM DRY DENSITY (kg/m³)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	1460	24.5
OVERSIZE CORRECTED		

COMMENTS

Stantec Sample no. 2982.

PROCTOR TEST REPORT

TO Dillon Consulting Ltd.
 300 - 100 Innovation Dr.
 Winnipeg, MB
 R3T 6A8

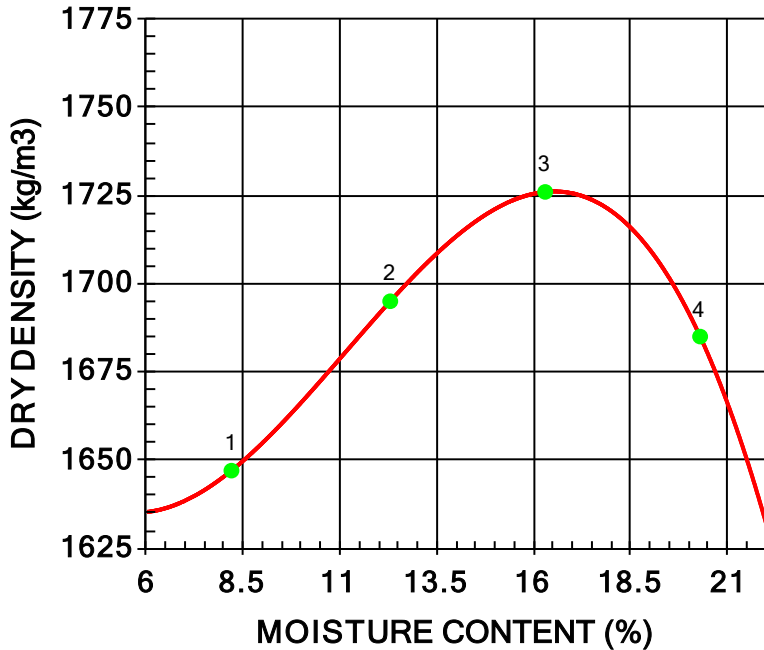
CLIENT Dillon Consulting Ltd.
 C.C.

ATTN: Ali Campbell

PROJECT 24-R-02 Local Streets Package

PROJECT NO. 123316895
 PROCTOR NO. 2 DATE SAMPLED 2024.Jan.16 DATE RECEIVED 2024.Jan.16 DATE TESTED 2024.Jan.26

INSITU MOISTURE	22.5 %	COMPACTION STANDARD	Standard Proctor, ASTM D698
TESTED BY	Donald Eliazar	COMPACTION PROCEDURE	A: 101.6mm Mold, Passing 4.75mm
MATERIAL IDENTIFICATION		RAMMER TYPE	Automatic
MAJOR COMPONENT	Subgrade	PREPARATION	Dry
SIZE		OVERSIZE CORRECTION METHOD	None
DESCRIPTION	Lean CLAY (CL)	RETAINED 4.75mm SCREEN	N/A %
SUPPLIER	Existing Material		
SOURCE	Carruthers Ave - BH-42, 0.740 m		



TRIAL NUMBER	WET DENSITY (kg/m³)	DRY DENSITY (kg/m³)	MOISTURE CONTENT (%)
1	1782	1647	8.2
2	1903	1695	12.3
3	2007	1726	16.3
4	2027	1685	20.3

	MAXIMUM DRY DENSITY (kg/m³)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	1730	16.5
OVERSIZE CORRECTED		

COMMENTS

Stantec Sample no. 2983.

PROCTOR TEST REPORT

TO Dillon Consulting Ltd.
 300 - 100 Innovation Dr.
 Winnipeg, MB
 R3T 6A8

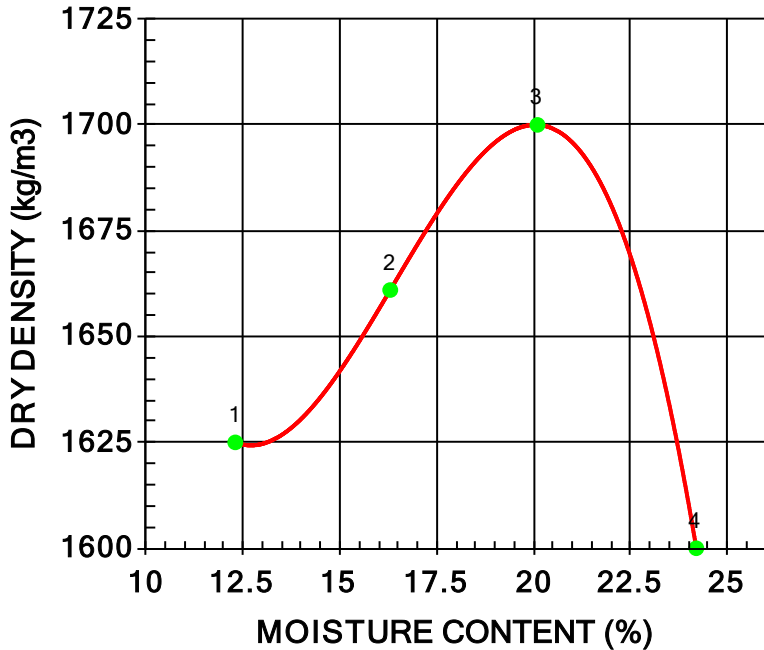
CLIENT Dillon Consulting Ltd.
 C.C.

ATTN: Ali Campbell

PROJECT 24-R-02 Local Streets Package

PROJECT NO. 123316895
 PROCTOR NO. 3 DATE SAMPLED 2024.Jan.17 DATE RECEIVED 2024.Jan.17 DATE TESTED 2024.Feb.05

INSITU MOISTURE	36.5 %	COMPACTION STANDARD	Standard Proctor, ASTM
TESTED BY	Donald Eliazar		D698
MATERIAL IDENTIFICATION		COMPACTION PROCEDURE	A: 101.6mm Mold, Passing 4.75mm
MAJOR COMPONENT	Subgrade	RAMMER TYPE	Manual
SIZE	Lean CLAY (CL)	PREPARATION	Moist
DESCRIPTION		OVERSIZE CORRECTION METHOD	None
SUPPLIER	Existing Materials	RETAINED 4.75mm SCREEN	N/A %
SOURCE	McAdam Ave - BH-43, 0.775 m		



TRIAL NUMBER	WET DENSITY (kg/m³)	DRY DENSITY (kg/m³)	MOISTURE CONTENT (%)
1	1825	1625	12.3
2	1932	1661	16.3
3	2042	1700	20.1
4	1987	1600	24.2

	MAXIMUM DRY DENSITY (kg/m³)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	1700	20.0
OVERSIZE CORRECTED		

COMMENTS

Stantec Sample No. 4002.

PROCTOR TEST REPORT

TO Dillon Consulting Ltd.
 300 - 100 Innovation Dr.
 Winnipeg, MB
 R3T 6A8

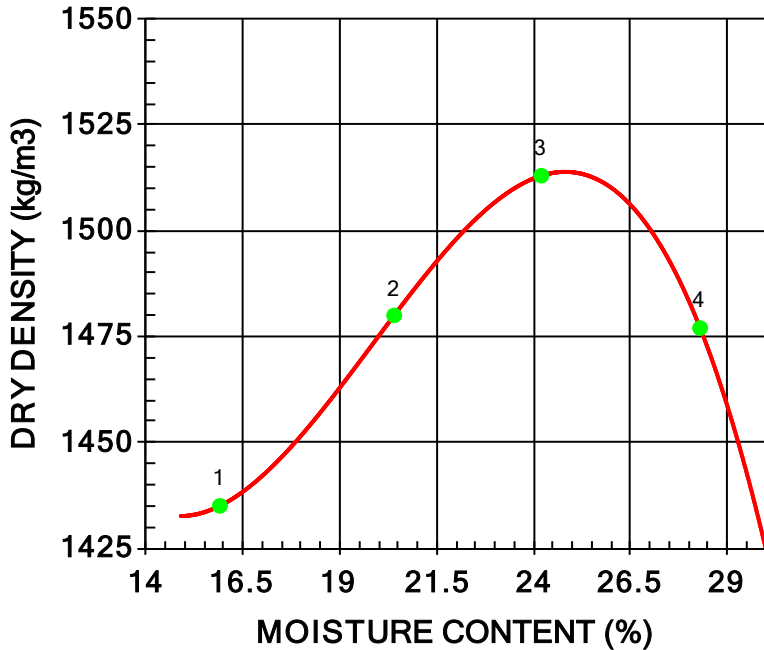
CLIENT Dillon Consulting Ltd.
 C.C.

ATTN: Ali Campbell

PROJECT 24-R-02 Local Streets Package

PROJECT NO. 123316895
 PROCTOR NO. 4 DATE SAMPLED 2024.Jan.17 DATE RECEIVED 2024.Jan.17 DATE TESTED 2024.Feb.06

INSITU MOISTURE	34.1 %	COMPACTION STANDARD	Standard Proctor, ASTM
TESTED BY	Donald Eliazar		D698
MATERIAL IDENTIFICATION		COMPACTION PROCEDURE	A: 101.6mm Mold, Passing 4.75mm
MAJOR COMPONENT	Subgrade	RAMMER TYPE	Manual
SIZE	Fat CLAY (CH)	PREPARATION	Moist
DESCRIPTION		OVERSIZE CORRECTION METHOD	None
SUPPLIER	Existing Materials	RETAINED 4.75mm SCREEN	N/A %
SOURCE	McAdam Ave - BH-45, 0.790 m		



TRIAL NUMBER	WET DENSITY (kg/m³)	DRY DENSITY (kg/m³)	MOISTURE CONTENT (%)
1	1663	1435	15.9
2	1782	1480	20.4
3	1879	1513	24.2
4	1895	1477	28.3

	MAXIMUM DRY DENSITY (kg/m³)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	1510	25.0
OVERSIZE CORRECTED		

COMMENTS

Stantec Sample No. 4003.

PROCTOR TEST REPORT

TO Dillon Consulting Ltd.
 300 - 100 Innovation Dr.
 Winnipeg, MB
 R3T 6A8

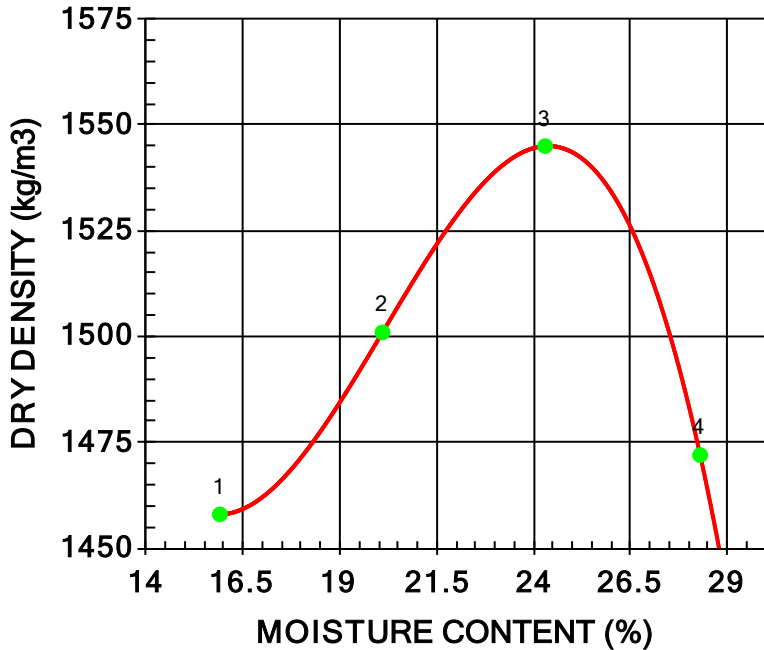
CLIENT Dillon Consulting Ltd.
 C.C.

ATTN: Ali Campbell

PROJECT 24-R-02 Local Streets Package

PROJECT NO. 123316895
 PROCTOR NO. 5 DATE SAMPLED 2024.Jan.17 DATE RECEIVED 2024.Jan.17 DATE TESTED 2024.Feb.06

INSITU MOISTURE	36.8 %	COMPACTION STANDARD	Standard Proctor, ASTM D698
TESTED BY	Donald Eliazar	COMPACTION PROCEDURE	A: 101.6mm Mold, Passing 4.75mm
MATERIAL IDENTIFICATION		RAMMER TYPE	Manual
MAJOR COMPONENT	Subgrade	PREPARATION	Moist
SIZE	Fat CLAY (CH)	OVERSIZE CORRECTION METHOD	None
DESCRIPTION		RETAINED 4.75mm SCREEN	N/A %
SUPPLIER	Existing Materials		
SOURCE	Gordon Ave - BH-46, 0.855 m		



TRIAL NUMBER	WET DENSITY (kg/m³)	DRY DENSITY (kg/m³)	MOISTURE CONTENT (%)
1	1690	1458	15.9
2	1803	1501	20.1
3	1920	1545	24.3
4	1889	1472	28.3

	MAXIMUM DRY DENSITY (kg/m³)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	1540	24.5
OVERSIZE CORRECTED		

COMMENTS

Stantec Sample No. 4004.

PROCTOR TEST REPORT

TO Dillon Consulting Ltd.
 300 - 100 Innovation Dr.
 Winnipeg, MB
 R3T 6A8

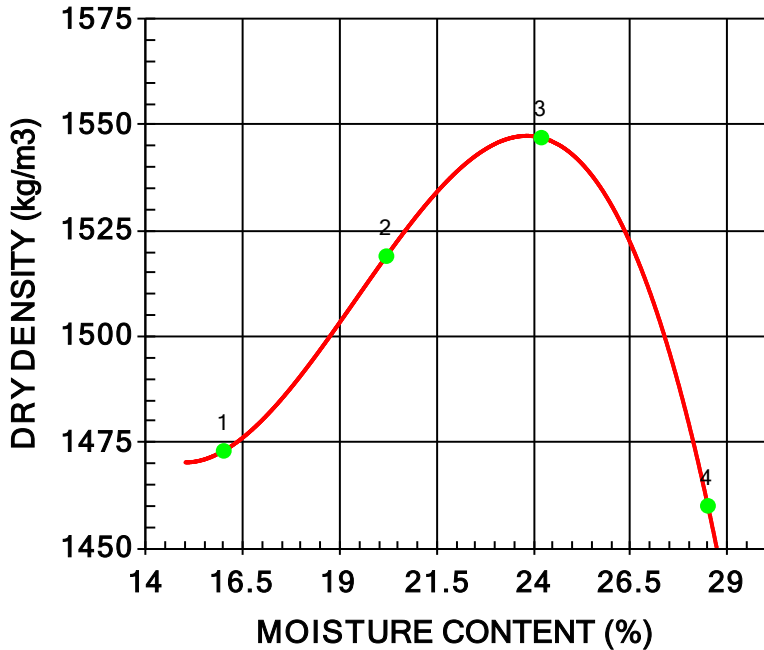
CLIENT Dillon Consulting Ltd.
 C.C.

ATTN: Ali Campbell

PROJECT 24-R-02 Local Streets Package

PROJECT NO. 123316895
 PROCTOR NO. 6 DATE SAMPLED 2024.Jan.17 DATE RECEIVED 2024.Jan.17 DATE TESTED 2024.Feb.07

INSITU MOISTURE	31.4 %	COMPACTION STANDARD	Standard Proctor, ASTM
TESTED BY	Donald Eliazar		D698
MATERIAL IDENTIFICATION		COMPACTION PROCEDURE	A: 101.6mm Mold, Passing 4.75mm
MAJOR COMPONENT	Subgrade	RAMMER TYPE	Manual
SIZE	Fat CLAY (CH)	PREPARATION	Moist
DESCRIPTION		OVERSIZE CORRECTION METHOD	None
SUPPLIER	Existing Materials	RETAINED 4.75mm SCREEN	N/A %
SOURCE	Gordon Ave - BH-48, 0.790 m		



TRIAL NUMBER	WET DENSITY (kg/m³)	DRY DENSITY (kg/m³)	MOISTURE CONTENT (%)
1	1709	1473	16.0
2	1826	1519	20.2
3	1921	1547	24.2
4	1876	1460	28.5

	MAXIMUM DRY DENSITY (kg/m³)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	1550	24.0
OVERSIZE CORRECTED		

COMMENTS

Stantec Sample No. 4005.

ASTM D1883 - CALIFORNIA BEARING RATIO (CBR) OF LABORATORY-COMPACTED SOILS

TO Dillon Consulting Ltd.
 300 - 100 Innovation Drive
 Winnipeg, Manitoba
 R3T 6A8

PROJECT 24-R-02 - Local Streets Package -
 Geotechnical Investigation

PROJECT NO. 123316895

ATTN Ali Campbell

REPORT NO. 1

DATE SAMPLED: 2024.Jan.16

DATE RECEIVED: 2024.Jan.16

DATE TESTED: 2024.Feb.02

SAMPLED BY: Stantec Consulting Ltd.

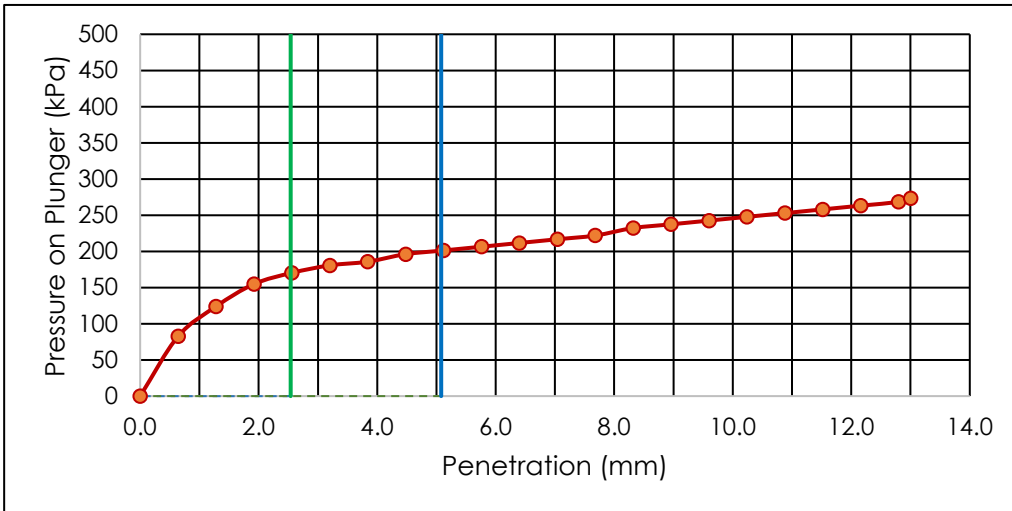
SUBMITTED BY: Stantec Consulting Ltd.

TESTED BY: Donald Eliazar

MATERIAL IDENTIFICATION

MATERIAL USE	Subgrade	SUPPLIER	Existing Material
MAX. NOMINAL SIZE	4.75 mm	SOURCE	Existing Material
MATERIAL TYPE	Fat CLAY (CH)	SAMPLE LOCATION	Carruthers Ave - BH-41, 0.775 m
SPECIFICATION ID	Not Applicable	STANTEC SAMPLE NO.	2982

IMMERSION PERIOD	96 ± 2 hr	TARGET MAX. DRY DENSITY	1460 kg/m ³
CONDITION OF SAMPLE	Soaked	TARGET OPTIMUM MOISTURE	24.5 %
SURCHARGE MASS	4.54 kg		
+19 mm OVERSIZE	0 %	AS-COMPACTED DRY DENSITY	1388 kg/m ³
SWELL OF SAMPLE	4.13 %	AS-COMPACTED MOISTURE	24.4 %
POST-TEST MOISTURE	38.1 %	AS-COMPACTED % COMPACTION	95 %



**CBR VALUE AT 2.54 mm
PENETRATION**
2.5

**CBR VALUE AT 5.08 mm
PENETRATION**
2.0

COMMENTS

Sample prepared to 95% of the maximum dry density at the optimum moisture content as determined from ASTM D698.

REPORT DATE 2024.Feb.12

REVIEWED BY  Jason Thompson, C.E.T.
 Principal - Manager of Materials Testing Services

ASTM D1883 - CALIFORNIA BEARING RATIO (CBR) OF LABORATORY-COMPACTED SOILS

TO Dillon Consulting Ltd.
 300 - 100 Innovation Drive
 Winnipeg, Manitoba
 R3T 6A8

PROJECT 24-R-02 - Local Streets Package -
 Geotechnical Investigation

PROJECT NO. 123316895

ATTN Ali Campbell

REPORT NO. 2

DATE SAMPLED: 2024.Jan.16

DATE RECEIVED: 2024.Jan.16

DATE TESTED: 2024.Feb.02

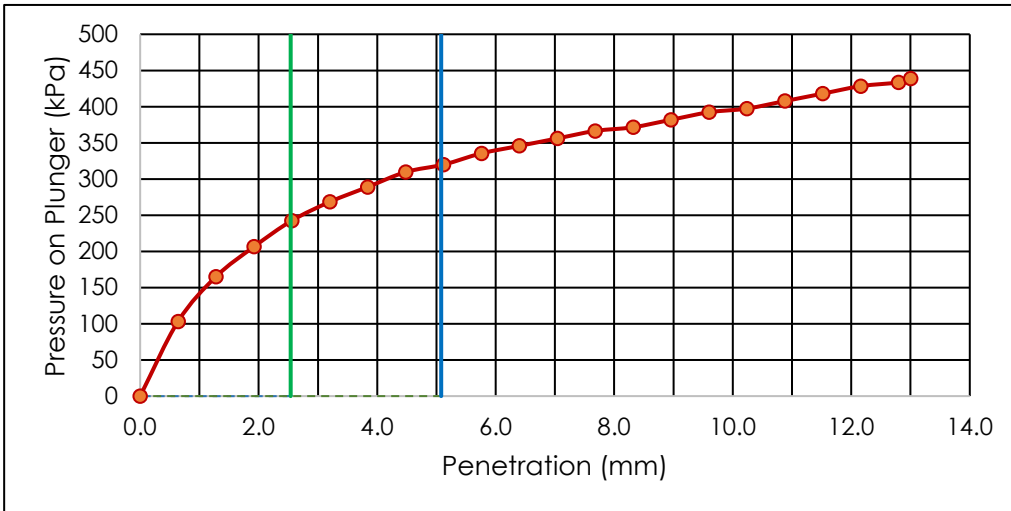
SAMPLED BY: Stantec Consulting Ltd.

SUBMITTED BY: Stantec Consulting Ltd.

TESTED BY: Donald Eliazar

MATERIAL IDENTIFICATION

MATERIAL USE	Subgrade	SUPPLIER	Existing Material
MAX. NOMINAL SIZE	4.75 mm	SOURCE	Existing Material
MATERIAL TYPE	Lean CLAY (CL)	SAMPLE LOCATION	Carruthers Ave - BH-42, 0.740 m
SPECIFICATION ID	Not Applicable	STANTEC SAMPLE NO.	2983
IMMERSION PERIOD	96 ± 2 hr	TARGET MAX. DRY DENSITY	1730 kg/m ³
CONDITION OF SAMPLE	Soaked	TARGET OPTIMUM MOISTURE	16.5 %
SURCHARGE MASS	4.54 kg		
+19 mm OVERSIZE	0 %	AS-COMPACTED DRY DENSITY	1644 kg/m ³
SWELL OF SAMPLE	2.60 %	AS-COMPACTED MOISTURE	16.4 %
POST-TEST MOISTURE	23.8 %	AS-COMPACTED % COMPACTION	95 %



**CBR VALUE AT 2.54 mm
PENETRATION
3.5**

**CBR VALUE AT 5.08 mm
PENETRATION
3.2**

COMMENTS

Sample prepared to 95% of the maximum dry density at the optimum moisture content as determined from ASTM D698.

REPORT DATE 2024.Feb.12

REVIEWED BY  Jason Thompson, C.E.T.
 Principal - Manager of Materials Testing Services

ASTM D1883 - CALIFORNIA BEARING RATIO (CBR) OF LABORATORY-COMPACTED SOILS

TO Dillon Consulting Ltd.
 300 - 100 Innovation Drive
 Winnipeg, Manitoba
 R3T 6A8

PROJECT 24-R-02 - Local Streets Package -
 Geotechnical Investigation

PROJECT NO. 123316895

ATTN Ali Campbell

REPORT NO. 3

DATE SAMPLED: 2024.Jan.17

DATE RECEIVED: 2024.Jan.17

DATE TESTED: 2024.Feb.19

SAMPLED BY: Stantec Consulting Ltd.

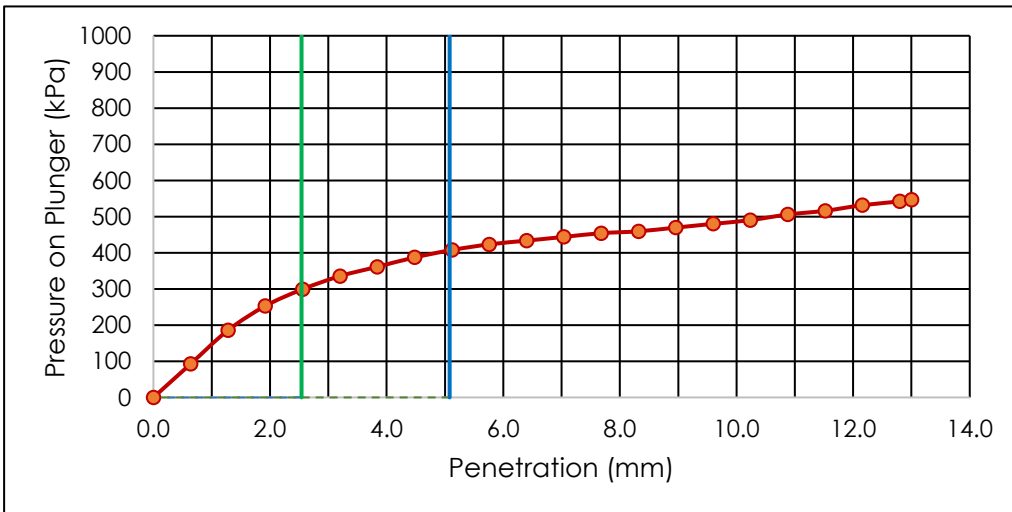
SUBMITTED BY: Stantec Consulting Ltd.

TESTED BY: Donald Eliazar

MATERIAL IDENTIFICATION

MATERIAL USE	Subgrade	SUPPLIER	Existing Material
MAX. NOMINAL SIZE	4.75 mm	SOURCE	Existing Material
MATERIAL TYPE	Lean CLAY (CL)	SAMPLE LOCATION	McAdam Ave - BH-43, 0.775 m
SPECIFICATION ID	Not Applicable	STANTEC SAMPLE NO.	2983

IMMERSION PERIOD	96 ± 2 hr	TARGET MAX. DRY DENSITY	1700 kg/m ³
CONDITION OF SAMPLE	Soaked	TARGET OPTIMUM MOISTURE	20.0 %
SURCHARGE MASS	4.54 kg		
+19 mm OVERSIZE	0 %	AS-COMPACTED DRY DENSITY	1617 kg/m ³
SWELL OF SAMPLE	1.56 %	AS-COMPACTED MOISTURE	19.8 %
POST-TEST MOISTURE	26.6 %	AS-COMPACTED % COMPACTION	95 %



**CBR VALUE AT 2.54 mm
PENETRATION**
4.3

**CBR VALUE AT 5.08 mm
PENETRATION**
4.1

COMMENTS

Sample prepared to 95% of the maximum dry density at the optimum moisture content as determined from ASTM D698.

REPORT DATE 2024.Feb.26

REVIEWED BY  Jason Thompson, C.E.T.
 Principal - Manager of Materials Testing Services

ASTM D1883 - CALIFORNIA BEARING RATIO (CBR) OF LABORATORY-COMPACTED SOILS

TO Dillon Consulting Ltd.
 300 - 100 Innovation Drive
 Winnipeg, Manitoba
 R3T 6A8

PROJECT 24-R-02 - Local Streets Package -
 Geotechnical Investigation

PROJECT NO. 123316895

ATTN Ali Campbell

REPORT NO. 4

DATE SAMPLED: 2024.Jan.17
 SAMPLED BY: Stantec Consulting Ltd.

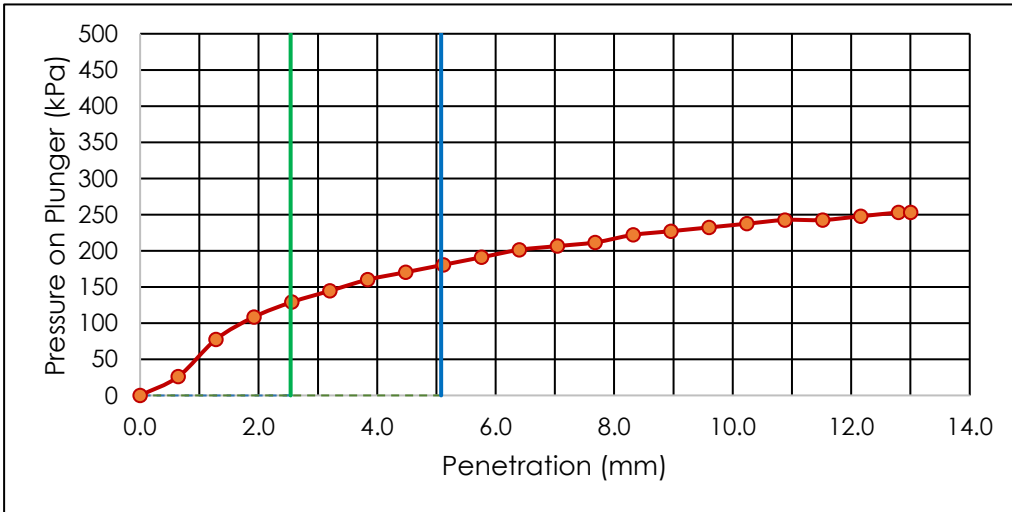
DATE RECEIVED: 2024.Jan.17
 SUBMITTED BY: Stantec Consulting Ltd.

DATE TESTED: 2024.Feb.19
 TESTED BY: Donald Eliazar

MATERIAL IDENTIFICATION

MATERIAL USE	Subgrade	SUPPLIER	Existing Material
MAX. NOMINAL SIZE	4.75 mm	SOURCE	Existing Material
MATERIAL TYPE	Fat CLAY (CH)	SAMPLE LOCATION	McAdam Ave - BH-45, 0.790 m
SPECIFICATION ID	Not Applicable	STANTEC SAMPLE NO.	4003

IMMERSION PERIOD	96 ± 2 hr	TARGET MAX. DRY DENSITY	1510 kg/m ³
CONDITION OF SAMPLE	Soaked	TARGET OPTIMUM MOISTURE	25.0 %
SURCHARGE MASS	4.54 kg		
+19 mm OVERSIZE	0 %	AS-COMPACTED DRY DENSITY	1435 kg/m ³
SWELL OF SAMPLE	3.25 %	AS-COMPACTED MOISTURE	25.0 %
POST-TEST MOISTURE	37.7 %	AS-COMPACTED % COMPACTION	95 %



**CBR VALUE AT 2.54 mm
PENETRATION**
1.9

**CBR VALUE AT 5.08 mm
PENETRATION**
1.8

COMMENTS

Sample prepared to 95% of the maximum dry density at the optimum moisture content as determined from ASTM D698.

REPORT DATE 2024.Feb.26

REVIEWED BY  Jason Thompson, C.E.T.
 Principal - Manager of Materials Testing Services

ASTM D1883 - CALIFORNIA BEARING RATIO (CBR) OF LABORATORY-COMPACTED SOILS

TO Dillon Consulting Ltd.
 300 - 100 Innovation Drive
 Winnipeg, Manitoba
 R3T 6A8

PROJECT 24-R-02 - Local Streets Package -
 Geotechnical Investigation

PROJECT NO. 123316895

ATTN Ali Campbell

REPORT NO. 5

DATE SAMPLED: 2024.Jan.17
 SAMPLED BY: Stantec Consulting Ltd.

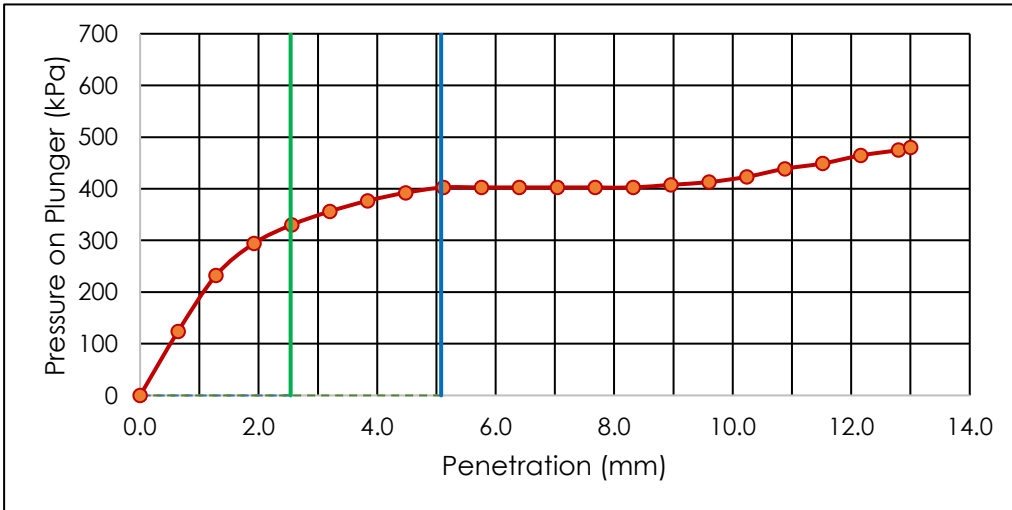
DATE RECEIVED: 2024.Jan.17
 SUBMITTED BY: Stantec Consulting Ltd.

DATE TESTED: 2024.Feb.19
 TESTED BY: Donald Eliazar

MATERIAL IDENTIFICATION

MATERIAL USE	Subgrade	SUPPLIER	Existing Material
MAX. NOMINAL SIZE	4.75 mm	SOURCE	Existing Material
MATERIAL TYPE	Fat CLAY (CH)	SAMPLE LOCATION	Gordon Ave - BH-46, 0.855 m
SPECIFICATION ID	Not Applicable	STANTEC SAMPLE NO.	4004

IMMERSION PERIOD	96 ± 2 hr	TARGET MAX. DRY DENSITY	1540 kg/m ³
CONDITION OF SAMPLE	Soaked	TARGET OPTIMUM MOISTURE	24.5 %
SURCHARGE MASS	4.54 kg		
+19 mm OVERSIZE	0 %	AS-COMPACTED DRY DENSITY	1465 kg/m ³
SWELL OF SAMPLE	1.60 %	AS-COMPACTED MOISTURE	24.4 %
POST-TEST MOISTURE	31.8 %	AS-COMPACTED % COMPACTION	95 %



**CBR VALUE AT 2.54 mm
PENETRATION**
4.8

**CBR VALUE AT 5.08 mm
PENETRATION**
4.0

COMMENTS

Sample prepared to 95% of the maximum dry density at the optimum moisture content as determined from ASTM D698.

REPORT DATE 2024.Feb.26

REVIEWED BY  Jason Thompson, C.E.T.
 Principal - Manager of Materials Testing Services

ASTM D1883 - CALIFORNIA BEARING RATIO (CBR) OF LABORATORY-COMPACTED SOILS

TO Dillon Consulting Ltd.
 300 - 100 Innovation Drive
 Winnipeg, Manitoba
 R3T 6A8

PROJECT 24-R-02 - Local Streets Package -
 Geotechnical Investigation

PROJECT NO. 123316895

ATTN Ali Campbell

REPORT NO. 6

DATE SAMPLED: 2024.Jan.17
 SAMPLED BY: Stantec Consulting Ltd.

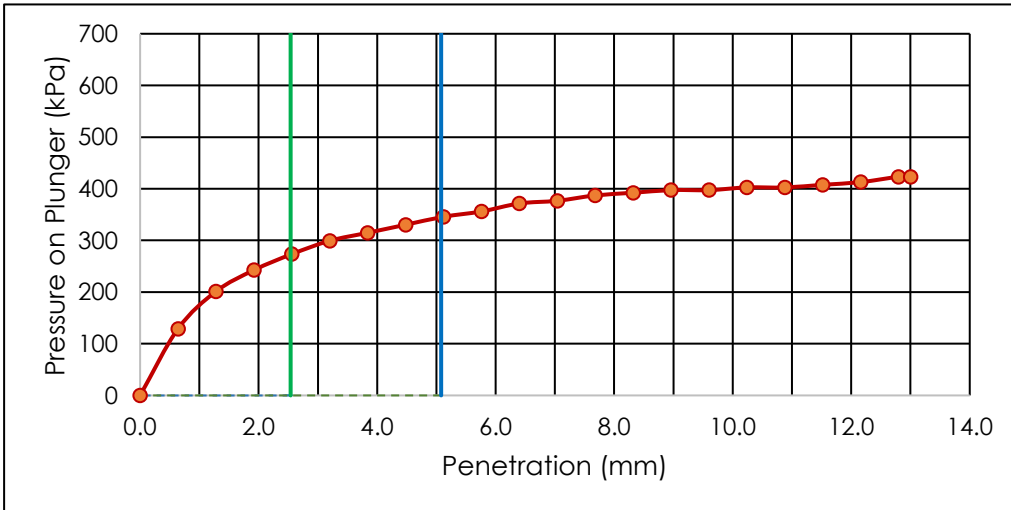
DATE RECEIVED: 2024.Jan.17
 SUBMITTED BY: Stantec Consulting Ltd.

DATE TESTED: 2024.Feb.19
 TESTED BY: Donald Eliazar

MATERIAL IDENTIFICATION

MATERIAL USE	Subgrade	SUPPLIER	Existing Material
MAX. NOMINAL SIZE	4.75 mm	SOURCE	Existing Material
MATERIAL TYPE	Fat CLAY (CH)	SAMPLE LOCATION	Gordon Ave - BH-48, 0.790 m
SPECIFICATION ID	Not Applicable	STANTEC SAMPLE NO.	4005

IMMERSION PERIOD	96 ± 2 hr	TARGET MAX. DRY DENSITY	1550 kg/m ³
CONDITION OF SAMPLE	Soaked	TARGET OPTIMUM MOISTURE	24.0 %
SURCHARGE MASS	4.54 kg		
+19 mm OVERSIZE	0 %	AS-COMPACTED DRY DENSITY	1472 kg/m ³
SWELL OF SAMPLE	2.17 %	AS-COMPACTED MOISTURE	24.1 %
POST-TEST MOISTURE	32.6 %	AS-COMPACTED % COMPACTION	95 %



**CBR VALUE AT 2.54 mm
PENETRATION
4.0**

**CBR VALUE AT 5.08 mm
PENETRATION
3.4**

COMMENTS

Sample prepared to 95% of the maximum dry density at the optimum moisture content as determined from ASTM D698.

REPORT DATE 2024.Feb.26

REVIEWED BY  Jason Thompson, C.E.T.
 Principal - Manager of Materials Testing Services

Table 2 - Compressive Strength Test Data

Street	Core ID	Diameter (mm)	Length (mm)	L/D Ratio	Correction Factor	Peak Load (kN)	Compressive Strength (MPa)	
							Measured	Corrected
Rudolph Bay	BH-51	75.35	175.20	2.325	1.0000	201.72	45.24	45.24
Rudolph Bay	BH-52	75.50	133.64	1.770	0.9816	231.47	51.70	50.75
Dahlia Alley	BH-53	75.62	125.62	1.661	0.9729	138.6	30.86	30.02
Dahlia Alley	BH-54	75.53	115.58	1.530	0.9624	237.66	53.04	51.05
Hood Ave	BH-55	75.42	151.09	2.003	1.0000	275.38	61.64	61.64
Hood Ave	BH-56	99.05	161.44	1.630	0.9704	404.01	52.43	50.88
Fortier Ave	BH-57	75.81	172.52	2.276	1.0000	185.3	41.05	41.05
Fortier Ave	BH-58	75.82	152.24	2.008	1.0000	195.4	43.28	43.28
Summerfield Way	BH-60	75.39	151.17	2.005	1.0000	191.4	42.88	42.88
Summerfield Way	BH-64	75.63	157.72	2.085	1.0000	191.75	42.68	42.68
Tranquility Cove	BH-66	75.13	164.16	2.185	1.0000	207.05	46.70	46.70
Tranquility Cove	BH-68	75.69	159.83	2.112	1.0000	160.97	35.77	35.77
Snowdon Ave	BH-70	75.81	145.08	1.914	0.9931	237.48	52.61	52.25
Snowdon Ave	BH-71	75.93	177.83	2.342	1.0000	269.99	59.63	59.63
Dearborn Ave	BH-74	75.78	155.87	2.057	1.0000	196.47	43.56	43.56
Dearborn Ave	BH-75	75.44	149.82	1.986	0.9989	161.2	36.06	36.02
Lacy St	BH-76	75.90	161.18	2.124	1.0000	97.41	21.53	21.53
Lacy St	BH-77	75.66	189.34	2.503	1.0000	249.89	55.58	55.58
Norilyn Bay	BH-78	75.78	169.81	2.241	1.0000	185.88	41.21	41.21
Norilyn Bay	BH-80	75.63	147.56	1.951	0.9961	248.2	55.25	55.03
Kullman St	BH-82	75.84	154.72	2.040	1.0000	189.93	42.04	42.04
Kullman St	BH-83	75.81	163.75	2.160	1.0000	199.63	44.23	44.23