

## **APPENDIX 'A' - GEOTECHNICAL REPORT**

The geotechnical report is provided to aid in the Contractor's evaluation of the existing pavement structure and/or soil conditions. The information presented is considered accurate at the locations shown on the Drawings and at the time of drilling. However, variations in pavement structure and/or soil conditions may exist between test holes and fluctuations in groundwater levels can be expected seasonally and may occur as a result of construction activities. The nature and extent of variations may not become evident until construction commences.



Stantec Consulting Ltd.  
199 Henlow Bay  
Winnipeg MB R3Y 1G4

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February 24, 2025

Project/File: 123317463-3

Geoff Kerr  
City of Winnipeg  
1155 Pacific Avenue  
Winnipeg, Manitoba R3E 3P1

Good day Geoff,

**Reference: 2025 Local Street Renewal Program (Contract 3) - Geotechnical Investigation**

Stantec Consulting Ltd. (Stantec) was retained to undertake a factual geotechnical investigation for the 2025 Local Street Renewal Program (Contract 3) in Winnipeg, Manitoba. Use of this report is subject to the Statement of General Conditions provided in Appendix A.

The coring and drilling program was conducted from January 8 to February 4, 2025. A total of 20 locations were investigated with pavement coring and/or subsurface geotechnical drilling. Pavement coring was performed by Stantec's geotechnical field technologist, and drilling services were provided by Maple Leaf Drilling Ltd. under the supervision of Stantec's technologist. A Borehole Location Plan is provided in Appendix B.

## **1. Pavement Coring**

A total of 15 pavement core samples were recovered to determine the in-place pavement thickness. In addition, 14 concrete core samples were tested to assess the in-place compressive strength of the concrete. One (1) concrete compressive strength test was cancelled due to the core sample being inadequate for testing (crumbly/fractured condition). The existing pavement thicknesses are summarized in Table 1 below, and the core photographs are provided in Appendix C.

## **2. Geotechnical Drilling**

A total of 5 boreholes were investigated by geotechnical drilling. The boreholes were terminated at a minimum depth of 2.0 m below the pavement, which resulted in borehole depths of 2.3 m. Soil samples were obtained directly from the auger flights at depths of 0.6 m, 0.9 m, 1.2 m, 1.6 m, and 2.0 m from the bottom of the existing pavement. The testholes were examined for evidence of sloughing and groundwater seepage upon completion of drilling.

Reference: 2025 Local Street Renewal Program (Contract 3) - Geotechnical Investigation

The borehole records are provided in Appendix D. The soil classification used in the borehole records is as per ASTM D2487 – *Standard Practice for Classification of Soils for Engineering Purposes (Unified Soil Classification System)*.

### 3. Existing Pavement Thicknesses

The existing pavement thicknesses are provided in the following table:

**Table 1 – Existing Pavement Thicknesses**

Borehole No.	Street	Asphalt Thickness (mm)	Concrete Thickness (mm)	Total Pavement Thickness (mm)
211	De Vries Ave	125	0	125
212	De Vries Ave	125	0	125
213	De Vries Ave	140	0	140
214	De Vries Ave	140	0	140
215	De Vries Ave	125	0	125
216	Boreholes cancelled; removed from scope of work.			
217				
218				
219	Kingsford Ave	0	170	170
220	Kingsford Ave	0	165	165
221	Kingsford Ave	0	140	140
222	Corrine St	0	160	160
223	Corrine St	0	140	140
224	Callum Cr	0	170	170
225	Callum Cr	0	155	155
226	Callum Cr	0	140	140
227	Callum Cr	0	150	150
228	Dunits Dr	0	160	160
229	Dunits Dr	0	150	150
230	Dunits Dr	0	150	150
231	Dunits Dr	0	150	150
232	Dunits Dr	0	135	135
233	Dunits Dr	0	155	155

Reference: 2025 Local Street Renewal Program (Contract 3) - Geotechnical Investigation

## 4. Laboratory Testing

Laboratory determination of moisture content (ASTM D2216) was conducted on all soil samples. The results are provided on the attached borehole records.

In addition, the following laboratory tests were conducted on select samples:

- ASTM D4318 - *Liquid Limit, Plastic Limit, and Plasticity Index of Soils*
- ASTM D7928 - *Particle-Size Distribution of Fine-Grained Soils Using The Sedimentation Analysis*
- ASTM D698 - *Laboratory Compaction Characteristics of Soil Using Standard Effort*
- ASTM D1883 - *California Bearing Ratio (CBR) of Laboratory-Compacted Soils*
- CSA A23.2-14C – *Obtaining and testing drilled cores for compressive strength testing*

The CBR tests were performed on test specimens compacted to 95% of the maximum dry density under soaked conditions.

Prior to compressive strength testing, the concrete core samples were conditioned in water at room temperature for 48 hours.

The laboratory test reports are provided in Appendix E.

Reference: 2025 Local Street Renewal Program (Contract 3) - Geotechnical Investigation

## 5. Closure

Please contact the undersigned if you have any questions regarding this report.

Regards,

**Stantec Consulting Ltd.**



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Attachment: Appendix A – Statement of General Conditions  
Appendix B – Borehole Location Plan  
Appendix C – Core Photographs  
Appendix D – Borehole Records  
Appendix E – Laboratory Test Reports

- Atterberg Limits Test Reports
- Particle-Size Analysis Reports
- Standard Proctor Test Reports
- CBR Test Reports
- Concrete Compressive Strength Test Results

## **Appendix A**

### Statement of General Conditions

## STATEMENT OF GENERAL CONDITIONS

**USE OF THIS REPORT:** This report has been prepared for the sole benefit of the Client or its agent and may not be used by any third party without the express written consent of Stantec and the Client. Any use which a third party makes of this report is the responsibility of such third party.

**BASIS OF THE REPORT:** The information, opinions, and/or recommendations made in this report are in accordance with Stantec's present understanding of the site-specific project as described by the Client. The applicability of these is restricted to the site conditions encountered at the time of the investigation or study. If the proposed site-specific project differs or is modified from what is described in this report or if the site conditions are altered, this report is no longer valid unless Stantec is requested by the Client to review and revise the report to reflect the differing or modified project specifics and/or the altered site conditions.

**STANDARD OF CARE:** Preparation of this report, and all associated work, was carried out in accordance with the normally accepted standard of care in the state or province of execution for the specific professional service provided to the Client. No other warranty is made.

**INTERPRETATION OF SITE CONDITIONS:** Soil, rock, or other material descriptions, and statements regarding their condition, made in this report are based on site conditions encountered by Stantec at the time of the work and at the specific testing and/or sampling locations. Classifications and statements of condition have been made in accordance with normally accepted practices which are judgmental in nature; no specific description should be considered exact, but rather reflective of the anticipated material behavior. Extrapolation of in situ conditions can only be made to some limited extent beyond the sampling or test points. The extent depends on variability of the soil, rock, and groundwater conditions as influenced by geological processes, construction activity, and site use.

**VARYING OR UNEXPECTED CONDITIONS:** Should any site or subsurface conditions be encountered that are different from those described in this report or encountered at the test locations, Stantec must be notified immediately to assess if the varying or unexpected conditions are substantial and if reassessments of the report conclusions or recommendations are required. Stantec will not be responsible to any party for damages incurred as a result of failing to notify Stantec that differing site or sub-surface conditions are present upon becoming aware of such conditions.

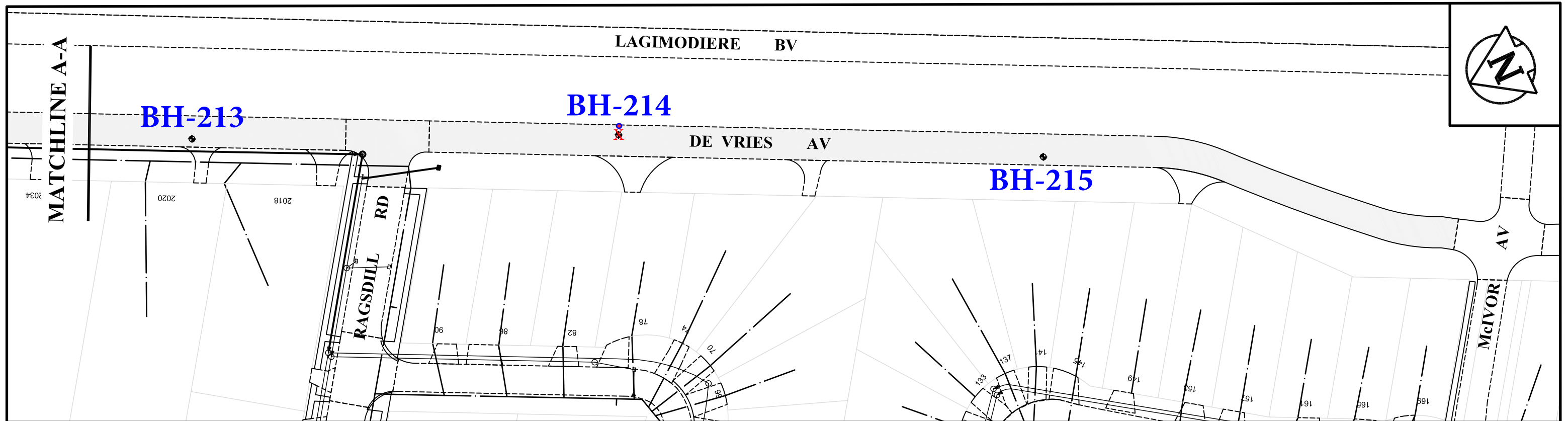
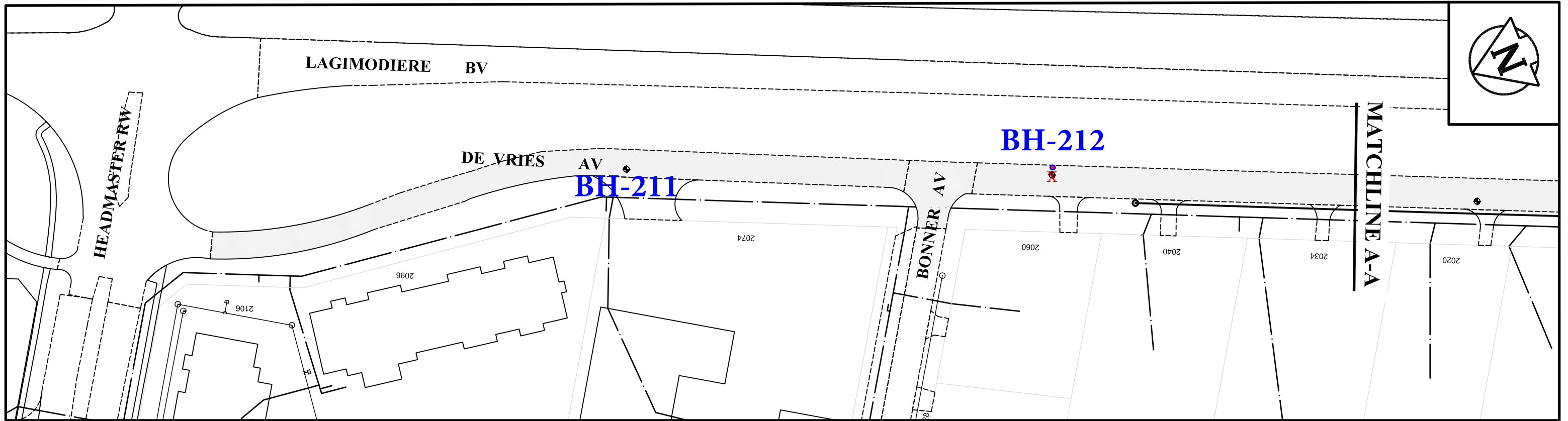
**PLANNING, DESIGN, OR CONSTRUCTION:** Development or design plans and specifications should be reviewed by Stantec, sufficiently ahead of initiating the next project stage (property acquisition, tender, construction, etc.), to confirm that this report completely addresses the elaborated project specifics and that the contents of this report have been properly interpreted. Specialty quality assurance services (field observations and testing) during construction are a necessary part of the evaluation of sub-subsurface conditions and site preparation works. Site work relating to the recommendations included in this report should only be carried out in the presence of a qualified geotechnical engineer; Stantec cannot be responsible for site work carried out without being present.



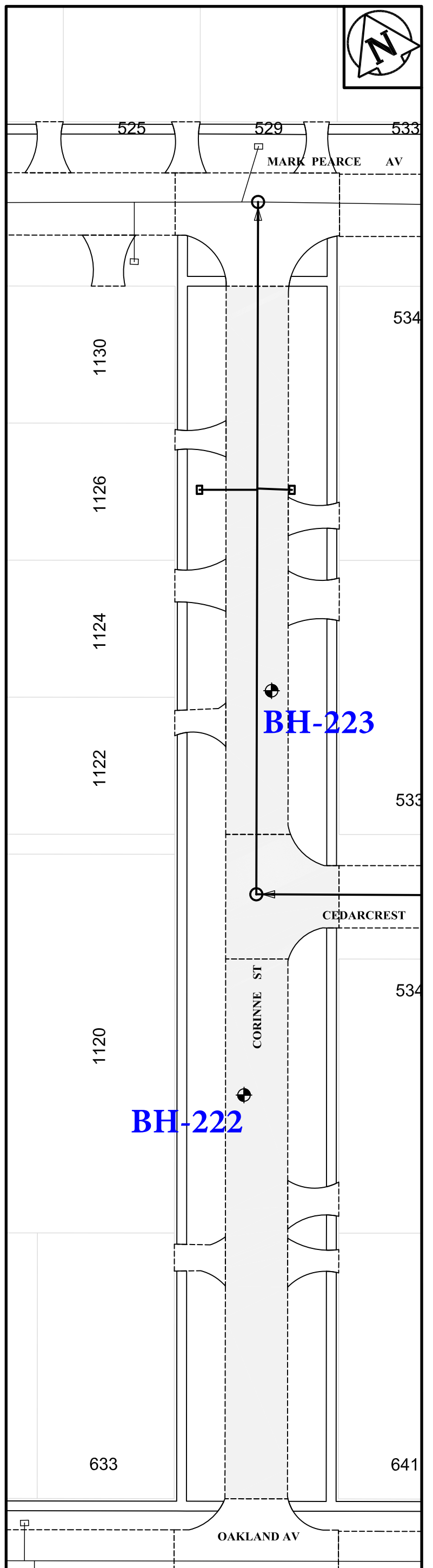
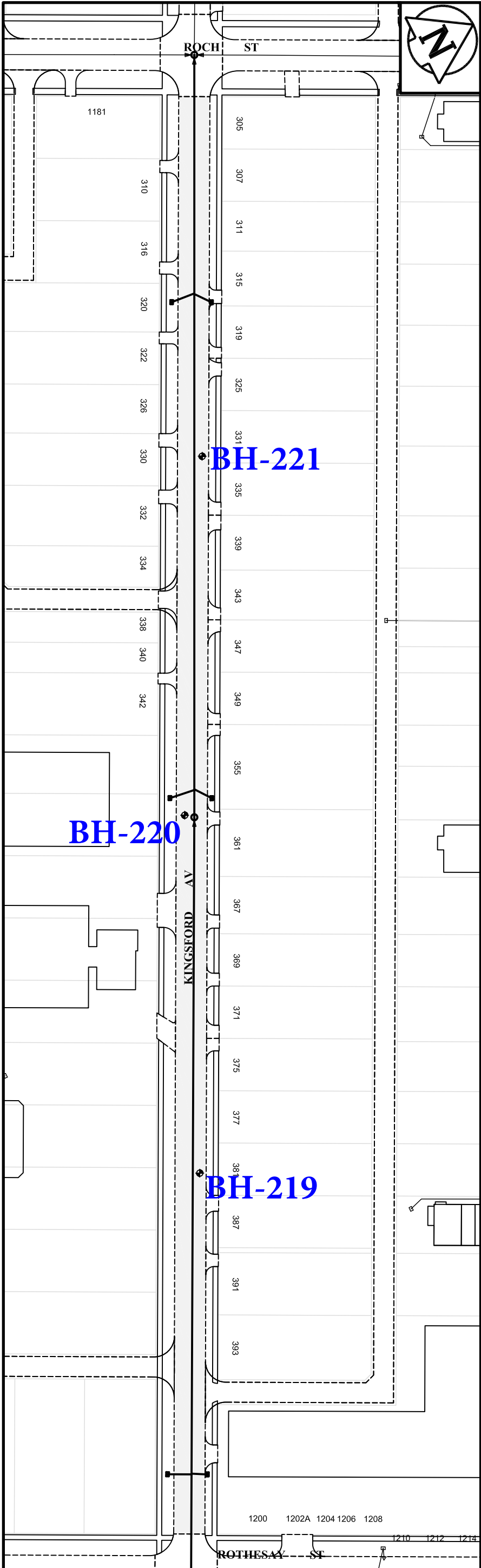
## **Appendix B**

### Borehole Location Plan





SEWER —	BOREHOLE ●	WATER MAIN/ WATERLINE —	DATE: 11/14/2024	DRAWING NO. 1 of 3	NOTE: DRILL 2.0m BOREHOLE AS PER SITE INVESTIGATION SPECIFICATION F3.4	2025 LOCAL STREET RENEWAL PROGRAM CORING DRAWING - CONTRACT 3 <b>DE VRIES AV FROM McIVOR AV TO HEADMASTER RW - REHAB AND RECON</b>
MANHOLE ○	CATCH BASIN □		DRAWN BY: J.W.	SCALE: 1 : 1000		



SEWER ——— PAVEMENT CORES ●

MANHOLE ○ CATCH BASIN □

DATE: 11/12/2024  
 DRAWN BY: J.W.

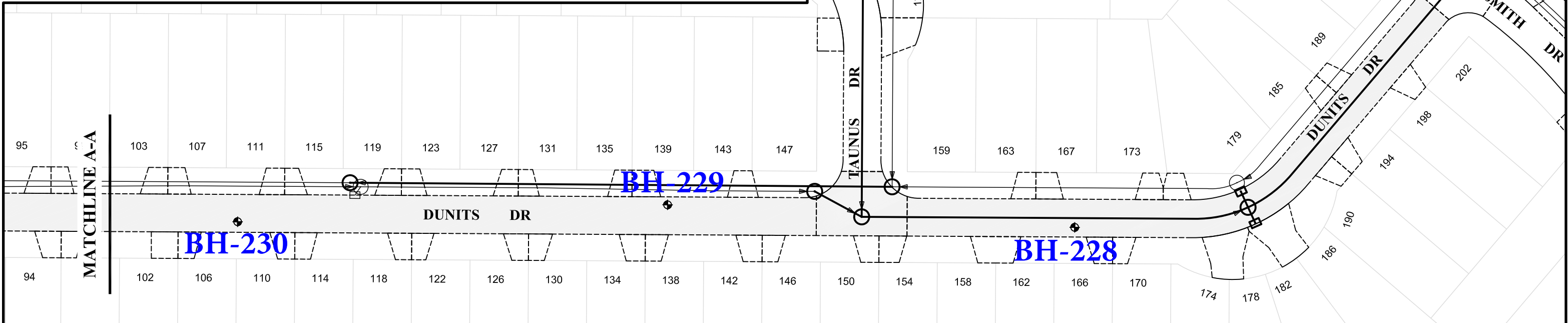
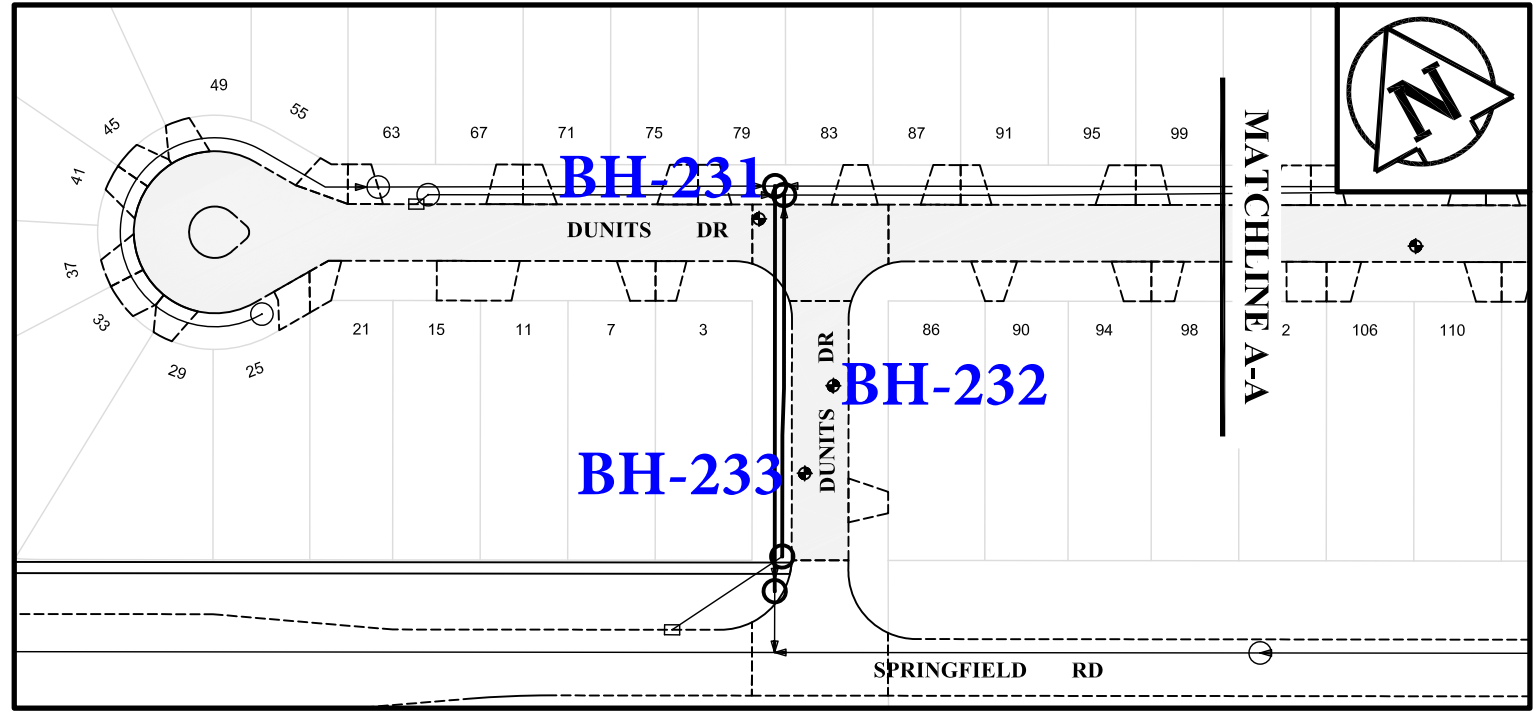
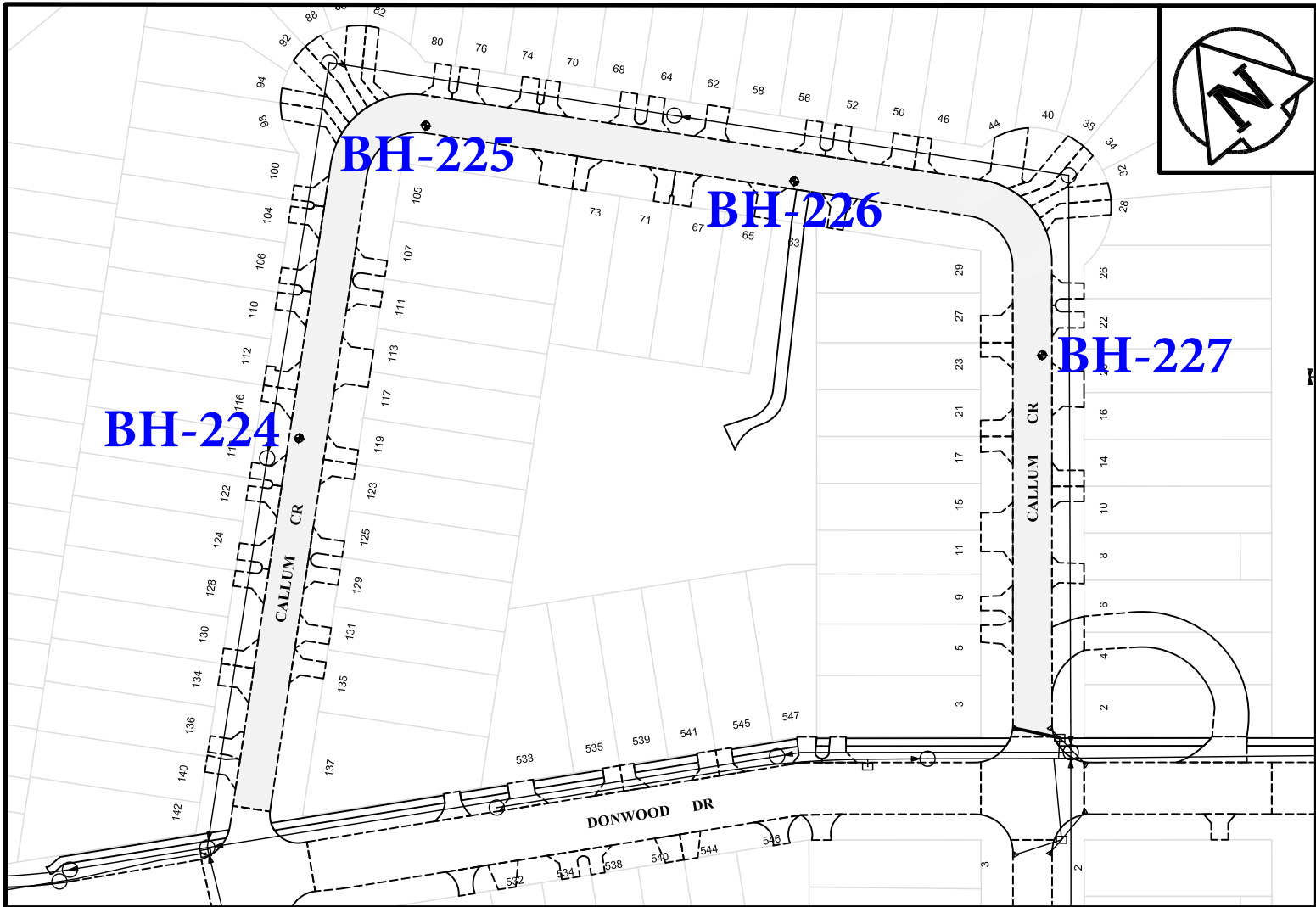
DRAWING NO. 2 of 3  
 SCALE: N.T.S.

NOTE: DRILL PAVEMENT CORES AS PER SITE INVESTIGATION SPECIFICATION F3.5

2025 LOCAL STREET RENEWAL PROGRAM CORING DRAWING - CONTRACT 3

**KINGSFORD AV FROM ROTHESAY ST TO ROCH ST - MAJOR REHABILITATION**

**CORINNE ST FROM MARK PEARCE AV TO OAKLAND AV - MAJOR REHABILITATION**



SEWER — PAVEMENT CORES ⊕  
 MANHOLE ○ CATCH BASIN □

NOTE: DRILL PAVEMENT CORES AS PER SITE INVESTIGATION SPECIFICATION F3.5

DATE: 11/12/2024  
 DRAWING NO.: 3 of 3  
 DRAWN BY: J.W.  
 SCALE: NTS

2025 LOCAL STREET RENEWAL PROGRAM CORING DRAWING - **CONTRACT 3**  
 CALLUM CR FROM DONWOOD DR TO DONWOOD DR - MAJOR REHABILITATION  
 DUNITS DR FROM SPRINGFIELD RD TO JIM SMITH DR - MAJOR REHABILITATION

## **Appendix C**

### Core Photographs



Figure 1 – Core Sample No. 219 – Kingsford Ave



Figure 2 – Core Sample No. 220 – Kingsford Ave



Figure 3 – Core Sample No. 221 - Kingsford Ave



Figure 4 – Core Sample No. 222 – Corriner St



Figure 5 – Core Sample No. 223 – Corrine St



Figure 6 – Core Sample No. 224 – Callum Cr



Figure 7 – Core Sample No. 225 – Callum Cr



Figure 8 – Core Sample No. 226 – Callum Cr



Figure 9 – Core Sample No. 227 – Callum Cr



Figure 10 – Core Sample No. 228 – Dunits Dr



Figure 11 – Core Sample No. 229 – Dunits Dr



Figure 12 – Core Sample No. 230 – Dunits Dr



Figure 13 – Core Sample No. 231 – Dunits Dr



Figure 14 – Core Sample No. 232 – Dunits Dr



Figure 15 – Core Sample No. 233 – Dunits Dr



## **Appendix D**

### Borehole Records

## SYMBOLS AND TERMS USED ON BOREHOLE AND TEST PIT RECORDS

### SOIL DESCRIPTION

#### Terminology describing common soil genesis

<i>Rootmat</i>	vegetation, roots and moss with organic matter and topsoil typically forming a mattress at the ground surface
<i>Topsoil</i>	mixture of soil and humus capable of supporting vegetative growth
<i>Peat</i>	mixture of visible and invisible fragments of decayed organic matter
<i>Till</i>	unstratified glacial deposit which may range from clay to boulders
<i>Fill</i>	material below the surface identified as placed by humans (excluding buried services)

#### Terminology describing soil structure

<i>Desiccated</i>	having visible signs of weathering by oxidization of clay minerals, shrinkage cracks, etc.
<i>Fissured</i>	having cracks, and hence a blocky structure
<i>Varved</i>	composed of regular alternating layers of silt and clay
<i>Stratified</i>	composed of alternating successions of different soil types, e.g. silt and sand
<i>Layer</i>	> 75 mm in thickness
<i>Seam</i>	2 mm to 75 mm in thickness
<i>Parting</i>	< 2 mm in thickness

#### Terminology describing soil types

The classification of soil types are made on the basis of grain size and plasticity in accordance with the Unified Soil Classification System (USCS) (ASTM D 2487 or D 2488) which excludes particles larger than 75 mm. For particles larger than 75 mm, and for defining percent clay fraction in hydrometer results, definitions proposed by Canadian Foundation Engineering Manual, 4<sup>th</sup> Edition are used. The USCS provides a group symbol (e.g. SM) and group name (e.g. silty sand) for identification.

#### Terminology describing cobbles, boulders, and non-matrix materials (organic matter or debris)

Terminology describing materials outside the USCS, (e.g. particles larger than 75 mm, visible organic matter, and construction debris) is based upon the proportion of these materials present:

<i>Trace, or occasional</i>	Less than 10%
<i>Some</i>	10-20%
<i>Frequent</i>	> 20%

#### Terminology describing compactness of cohesionless soils

The standard terminology to describe cohesionless soils includes compactness (formerly "relative density"), as determined by the Standard Penetration Test (SPT) N-Value - also known as N-Index. The SPT N-Value is described further on Page 2. A relationship between compactness condition and N-Value is shown in the following table.

Compactness Condition	SPT N-Value
<i>Very Loose</i>	<4
<i>Loose</i>	4-10
<i>Compact</i>	10-30
<i>Dense</i>	30-50
<i>Very Dense</i>	>50

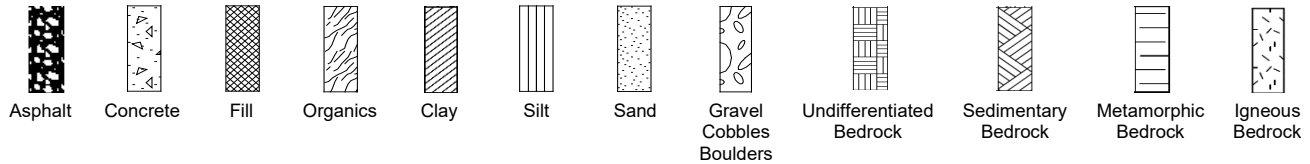
#### Terminology describing consistency of cohesive soils

The standard terminology to describe cohesive soils includes the consistency, which is based on undrained shear strength as measured by *in situ* vane tests, penetrometer tests, or unconfined compression tests. Consistency may be crudely estimated from SPT N-Value based on the correlation shown in the following table (Terzaghi and Peck, 1967). The correlation to SPT N-Value is used with caution as it is only very approximate.

Consistency	Undrained Shear Strength		Approximate SPT N-Value
	kips/sq.ft	kPa	
<i>Very Soft</i>	<0.25	<12.5	<2
<i>Soft</i>	0.25 - 0.5	12.5 - 25	2-4
<i>Firm</i>	0.5 - 1.0	25 - 50	4-8
<i>Stiff</i>	1.0 - 2.0	50 - 100	8-15
<i>Very Stiff</i>	2.0 - 4.0	100 - 200	15-30
<i>Hard</i>	>4.0	>200	>30

## STRATA PLOT

Strata plots symbolize the soil or bedrock description. They are combinations of the following basic symbols. The dimensions within the strata symbols are not indicative of the particle size, layer thickness, etc. Not all bedrock strata plots are shown.



## SAMPLE TYPE

AS, BS, GS		Auger sample; bulk sample; grab sample
DP		Direct-Push sample (small diameter tube sampler hydraulically advanced)
PS		Piston sample
SO		Sonic tube
SS		Split spoon sample (obtained by performing the Standard Penetration Test)
ST		Shelby Tube or thin wall tube
SV		Shear vane
RC HQ, NQ, BQ, etc.		Rock Core; samples obtained with the use of standard size diamond coring bits.

## WATER LEVEL



**Measured:**  
in standpipe, piezometer, or well



**Inferred:**  
seepage noted or water level measured during or at completion of drilling

## RECOVERY FOR SOIL SAMPLES

The recovery is recorded as the length of the soil sample recovered in the direct push, split spoon sampler, Shelby Tube, or sonic tube.

## N-VALUE

Numbers in this column are the field results of the Standard Penetration Test (SPT): the number of blows of a 140-pound (63.5 kg) hammer falling 30 inches (760 mm), required to drive a 2 inch (50.8 mm) O.D. split spoon sampler one foot (300 mm) into the soil. In accordance with ASTM D1586, the N-Value equals the sum of the number of blows (N) required to drive the sampler over the interval of 6 to 18 in. (150 to 450 mm). However, when a 24 in. (610 mm) sampler is used, the number of blows (N) required to drive the sampler over the interval of 12 to 24 in. (300 to 610 mm) may be reported if this value is lower. For split spoon samples where insufficient penetration was achieved and N-Values cannot be presented, the number of blows are reported over sampler penetration in millimetres (e.g. 50 for 75 mm or 50/75 mm). Some design methods make use of N-values corrected for various factors such as overburden pressure, energy ratio, borehole diameter, etc. No corrections have been applied to the N-values presented on the log.

## DYNAMIC CONE PENETRATION TEST (DCPT)

Dynamic cone penetration tests are performed using a standard 60-degree apex cone connected to 'A' size drill rods with the same standard fall height and weight as the Standard Penetration Test. The DCPT value is the number of blows of the hammer required to drive the cone one foot (300 mm) into the soil. The DCPT is used as a probe to assess soil variability.

## OTHER TESTS

S	Sieve analysis
H	Hydrometer analysis
k	Laboratory permeability
$\gamma$	Unit weight
$G_s$	Specific gravity of soil particles
CD	Consolidated drained triaxial
CU	Consolidated undrained triaxial with pore pressure measurements
UU	Unconsolidated undrained triaxial
DS	Direct Shear
C	Consolidation
$Q_u$	Unconfined compression
$I_p$	Point Load Index ( $I_p$ on Borehole Record equals $I_p(50)$ in which the index is corrected to a reference diameter of 50 mm)

	Single packer permeability test; test interval from depth shown to bottom of borehole
	Double packer permeability test; test interval as indicated
	Falling head permeability test using casing
	Falling head permeability test using well point or piezometer

## **ROCK DESCRIPTION**

Except where specified below, terminology for describing rock is as defined by the International Society for Rock Mechanics (ISRM) 2007 publication "The Complete ISRM Suggested Methods for Rock Characterization, Testing and Monitoring: 1974-2006"

**Total Core Recovery (TCR)** denotes the sum of all measurable rock core recovered in one drill run. The value is noted as a percentage of recovered rock core based on the total length of the drill run.

**Solid Core Recovery (SCR)** is defined as total length of solid core divided by the total drilled length, presented as a percentage. Solid core is defined as core with one full diameter.

**Rock Quality Designation (RQD)** is a modified core recovery that incorporates only pieces of solid core that are equal to or greater than 10 cm (4") along the core axis. It is calculated as the total cumulative length of solid core (> 10 cm) as measured along the centerline of the core divided by the total length of borehole drilled for each drill run or geotechnical interval, presented as a percentage. RQD is determined in accordance with ASTM D6032.

**Fracture Index (FI)** is defined as the number of naturally occurring fractures within a given length of core. The Fracture Index is reported as a simple count of natural occurring fractures.

### **Terminology describing rock quality**

<b>Rock Mass Quality</b>	<b>Rock Quality Designation Number (RQD)</b>	<b>Alternate (Colloquial) Rock Mass Quality</b>	
<i>Very Poor Quality</i>	0-25	<i>Very Severely Fractured</i>	<i>Crushed</i>
<i>Poor Quality</i>	25-50	<i>Severely Fractured</i>	<i>Shattered or Very Blocky</i>
<i>Fair Quality</i>	50-75	<i>Fractured</i>	<i>Blocky</i>
<i>Good Quality</i>	75-90	<i>Moderately Jointed</i>	<i>Sound</i>
<i>Excellent Quality</i>	90-100	<i>Intact</i>	<i>Very Sound</i>

### **Terminology describing rock strength**

<b>Strength Classification</b>	<b>Grade</b>	<b>Field Estimates of Uniaxial Compressive Strength</b>	<b>Unconfined Compressive Strength (MPa)</b>
<i>Extremely Weak</i>	R0	Indented by thumbnail	<1
<i>Very Weak</i>	R1	Crumbles under firm blows of geological hammer, can be peeled with a pocketknife	1 – 5
<i>Weak</i>	R2	Peeled by pocketknife with difficulty, shallow indentations made by firm blow with point of geological hammer	5 – 25
<i>Medium Strong</i>	R3	Cannot be scraped or peeled with a pocketknife, can be fractured with single firm blow of geological hammer	25 – 50
<i>Strong</i>	R4	More than one blow with geological hammer to fracture	50 – 100
<i>Very Strong</i>	R5	Many blows with geological hammer to fracture	100 – 250
<i>Extremely Strong</i>	R6	Can only be chipped with geological hammer	>250

### **Terminology describing rock weathering**

<b>Term</b>	<b>Symbol</b>	<b>Description</b>
<i>Fresh</i>	W1	No visible signs of rock weathering. Slight discoloration along major discontinuities
<i>Slightly</i>	W2	Discoloration indicates weathering of rock on discontinuity surfaces. All the rock material may be discolored.
<i>Moderately</i>	W3	Less than half the rock is decomposed and/or disintegrated into soil.
<i>Highly</i>	W4	More than half the rock is decomposed and/or disintegrated into soil.
<i>Completely</i>	W5	All the rock material is decomposed and/or disintegrated into soil. The original mass structure is still largely intact.
<i>Residual Soil</i>	W6	All the rock converted to soil. Structure and fabric destroyed.

### **Terminology describing rock with respect to discontinuity and bedding spacing**

<b>Spacing (mm)</b>	<b>Discontinuities Spacing</b>	<b>Bedding</b>
>6000	<i>Extremely Wide</i>	-
2000-6000	<i>Very Wide</i>	<i>Very Thick</i>
600-2000	<i>Wide</i>	<i>Thick</i>
200-600	<i>Moderate</i>	<i>Medium</i>
60-200	<i>Close</i>	<i>Thin</i>
20-60	<i>Very Close</i>	<i>Very Thin</i>
<20	<i>Extremely Close</i>	<i>Laminated</i>
<6	-	<i>Thinly Laminated</i>

CLIENT: City of Winnipeg  
 PROJECT: 2025 Local Street Renewal Program (Contract 3)  
 LOCATION: De Vries Ave  
 DATE BORED: January 08 2025

PROJECT NO.: 123317463-3  
 BH ELEVATION: N/A  
 DATUM: N/A  
 WATER LEVEL: N/A

DEPTH (m)	ELEVATION (m)	SOIL DESCRIPTION (USCS)	STRATA PLOT	SAMPLES				OTHER TESTS / REMARKS	UNDRAINED SHEAR STRENGTH, Cu (kPa)								BACKFILL	ELEVATION (m)						
				TYPE	NUMBER	RECOVERY (mm) or TCR %	N-VALUE or RQD %		50 kPa	100 kPa	150 kPa	200 kPa	WATER CONTENT & ATTERBERG LIMITS											
									▲ LABORATORY TEST      ◆ FIELD VANE TEST ★ POCKET PENETROMETER    □ POCKET SHEAR VANE				W <sub>P</sub> W    W <sub>L</sub>				✕ SPT (N-value) BLOWS/0.3m							
									Water Content (%) and Blow Count															
									10   20   30   40   50   60   70   80															
0		ASPHALT																						
		FILL: crushed limestone, 12.5 mm																						
		Brown silty sand (SM) FILL						Sieve/Hydro at 0.6 m G 9%   S 58%   M 22%   C 10%																
		Firm black fat clay (CH) FILL - trace to some fine gravel																						
1																								
		Firm black FAT CLAY (CH) - trace organics																						
2																								
3		<b>End of Borehole</b> • Borehole terminated at a depth of 2.3 m. • No groundwater seepage or soil sloughing was observed during or upon completion of drilling. • Borehole backfilled in accordance with the City of Winnipeg Street Cuts Manual.																						

Printed Feb 24 2025 08:43:01 SOIL\_123317463-3.GPJ\_2/24/25

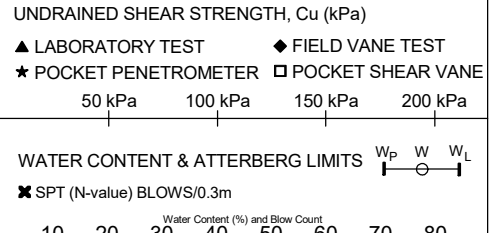
ASPHALT	GROUT	CONCRETE
BENTONITE	DRILL CUTTINGS	SAND
SLOUGH		

Drilling Contractor: Maple Leaf Drilling Ltd.	Logged By: LP
Drilling Method: 125 mm SSA	Reviewed By: GB
Completion Depth: 2.3 m	Page 1 of 1

CLIENT: City of Winnipeg  
 PROJECT: 2025 Local Street Renewal Program (Contract 3)  
 LOCATION: De Vries Ave  
 DATE BORED: January 08 2025

PROJECT NO.: 123317463-3  
 BH ELEVATION: N/A  
 DATUM: N/A  
 WATER LEVEL: N/A

DEPTH (m)	ELEVATION (m)	SOIL DESCRIPTION (USCS)	STRATA PLOT	SAMPLES				OTHER TESTS / REMARKS	UNDRAINED SHEAR STRENGTH, Cu (kPa)				BACKFILL	ELEVATION (m)
				TYPE	NUMBER	RECOVERY (mm) or TCR %	N-VALUE or RQD %		50 kPa	100 kPa	150 kPa	200 kPa		
0		ASPHALT												
		FILL: crushed limestone, 12.5 mm												
		Firm black fat clay (CH) FILL - trace fine gravel												
		Stiff black FAT CLAY (CH)		BS				Sieve/Hydro at 0.6 m G 0% S 3% M 43% C 55%						
1				AS										
				AS										
				AS										
				AS										
2				AS										
		- firm below 2.1 m		AS										
3		<b>End of Borehole</b> • Borehole terminated at a depth of 2.3 m. • No groundwater seepage or soil sloughing was observed during or upon completion of drilling. • Borehole backfilled in accordance with the City of Winnipeg Street Cuts Manual.												



BACKFILL SYMBOL: ASPHALT    GROUT    CONCRETE  
 BENTONITE    DRILL CUTTINGS    SAND    SLOUGH

Drilling Contractor: Maple Leaf Drilling Ltd.    Logged By: LP  
 Drilling Method: 125 mm SSA    Reviewed By: GB  
 Completion Depth: 2.3 m    Page 1 of 1

CLIENT: City of Winnipeg  
 PROJECT: 2025 Local Street Renewal Program (Contract 3)  
 LOCATION: De Vries Ave  
 DATE BORED: January 08 2025

PROJECT NO.: 123317463-3  
 BH ELEVATION: N/A  
 DATUM: N/A  
 WATER LEVEL: N/A

DEPTH (m)	ELEVATION (m)	SOIL DESCRIPTION (USCS)	STRATA PLOT	SAMPLES				OTHER TESTS / REMARKS	UNDRAINED SHEAR STRENGTH, Cu (kPa)				BACKFILL	ELEVATION (m)
				TYPE	NUMBER	RECOVERY (mm) or TCR %	N-VALUE or RQD %		50 kPa	100 kPa	150 kPa	200 kPa		
0		ASPHALT												
		FILL: crushed limestone, 12.5 mm												
		Stiff black FAT CLAY (CH)		BS				Sieve/Hydro at 0.6 m G 0% S 1% M 65% C 64%						
1				AS										
				AS										
				AS										
				AS										
2		- brown below 2.1 m		AS										
				AS										
3		<b>End of Borehole</b> • Borehole terminated at a depth of 2.3 m. • No groundwater seepage or soil sloughing was observed during or upon completion of drilling. • Borehole backfilled in accordance with the City of Winnipeg Street Cuts Manual.												

BACKFILL SYMBOL ASPHALT    GROUT    CONCRETE  
 BENTONITE    DRILL CUTTINGS    SAND    SLOUGH

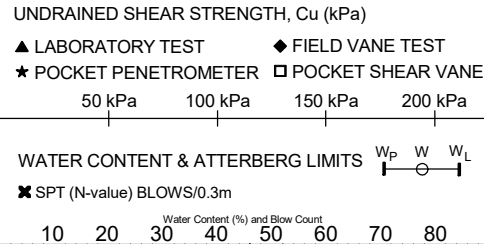
Drilling Contractor: Maple Leaf Drilling Ltd.    Logged By: LP  
 Drilling Method: 125 mm SSA    Reviewed By: GB  
 Completion Depth: 2.3 m    Page 1 of 1

CLIENT: City of Winnipeg  
 PROJECT: 2025 Local Street Renewal Program (Contract 3)  
 LOCATION: De Vries Ave  
 DATE BORED: January 08 2025

PROJECT NO.: 123317463-3  
 BH ELEVATION: N/A  
 DATUM: N/A  
 WATER LEVEL: N/A

DEPTH (m)	ELEVATION (m)	SOIL DESCRIPTION (USCS)	STRATA PLOT	SAMPLES				OTHER TESTS / REMARKS	UNDRAINED SHEAR STRENGTH, Cu (kPa)				BACKFILL	ELEVATION (m)
				TYPE	NUMBER	RECOVERY (mm) or TCR %	N-VALUE or RQD %		50 kPa	100 kPa	150 kPa	200 kPa		
0		ASPHALT												
		FILL: crushed limestone, 12.5 mm												
		Stiff black FAT CLAY (CH)		BS				Sieve/Hydro at 0.6 m G 0% S 0% M 36% C 63%						
1				AS										
				AS										
				AS										
		- firm and brown below 1.7 m		AS										
2				AS										
				AS										
3		End of Borehole												

**End of Borehole**  
 • Borehole terminated at a depth of 2.3 m.  
 • No groundwater seepage or soil sloughing was observed during or upon completion of drilling.  
 • Borehole backfilled in accordance with the City of Winnipeg Street Cuts Manual.



	ASPHALT		GROUT		CONCRETE
	BENTONITE		DRILL CUTTINGS		SAND
	SLOUGH				

Drilling Contractor: Maple Leaf Drilling Ltd.	Logged By: LP
Drilling Method: 125 mm SSA	Reviewed By: GB
Completion Depth: 2.3 m	Page 1 of 1



CLIENT: City of Winnipeg  
 PROJECT: 2025 Local Street Renewal Program (Contract 3)  
 LOCATION: De Vries Ave  
 DATE BORED: January 08 2025

PROJECT NO.: 123317463-3  
 BH ELEVATION: N/A  
 DATUM: N/A  
 WATER LEVEL: N/A

DEPTH (m)	ELEVATION (m)	SOIL DESCRIPTION (USCS)	STRATA PLOT	SAMPLES				OTHER TESTS / REMARKS	UNDRAINED SHEAR STRENGTH, Cu (kPa)				BACKFILL	ELEVATION (m)
				TYPE	NUMBER	RECOVERY (mm) or TCR %	N-VALUE or RQD %		50 kPa	100 kPa	150 kPa	200 kPa		
0		ASPHALT	ASPHALT						▲ LABORATORY TEST      ◆ FIELD VANE TEST ★ POCKET PENETROMETER    □ POCKET SHEAR VANE WATER CONTENT & ATTERBERG LIMITS    W <sub>P</sub> W    W <sub>L</sub> ✖ SPT (N-value) BLOWS/0.3m 10    20    30    40    50    60    70    80				BACKFILL	
		FILL: crushed limestone, 12.5 mm	FILL						Water Content (%) and Blow Count Sieve/Hydro at 0.6 m G    S    M    C 0%   0%   39%   61%				BACKFILL	
1		Stiff black FAT CLAY (CH)  - grey below 0.9 m  - firm below 1.5 m	CLAY	BS AS AS AS AS AS									BACKFILL	
2			CLAY	AS									BACKFILL	
3		<b>End of Borehole</b> • Borehole terminated at a depth of 2.3 m. • No groundwater seepage or soil sloughing was observed during or upon completion of drilling. • Borehole backfilled in accordance with the City of Winnipeg Street Cuts Manual.	CLAY	AS									BACKFILL	

Printed Feb 24 2025 08:43:05 SOIL\_123317463-3.GPJ 2/24/25

## **Appendix E**

### Laboratory Testing Reports

- Atterberg Limits
- Particle-Size Analysis
- Standard Proctor
- California Bearing Ratio
- Concrete Compressive Strength

# ASTM D4318 - LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX OF SOILS (LL METHOD B - ONE-POINT)

TO City of Winnipeg, Public Works Dept.  
 104 - 1155 Pacific Avenue  
 Winnipeg, Manitoba  
 R3E 2P1

PROJECT 2025 Local Street Renewal Program  
 Contract 3

PROJECT NO. 123317463-3

ATTN Geoff Kerr

REPORT NO. 1

DATE SAMPLED: 2025.Jan.08

DATE RECEIVED: 2025.Jan.08

DATE TESTED: 2025.Jan.31

SAMPLED BY: Stantec Consulting Ltd.

SUBMITTED BY: Stantec Consulting Ltd.

TESTED BY: Rimanshi Gorasiya

**MATERIAL IDENTIFICATION**

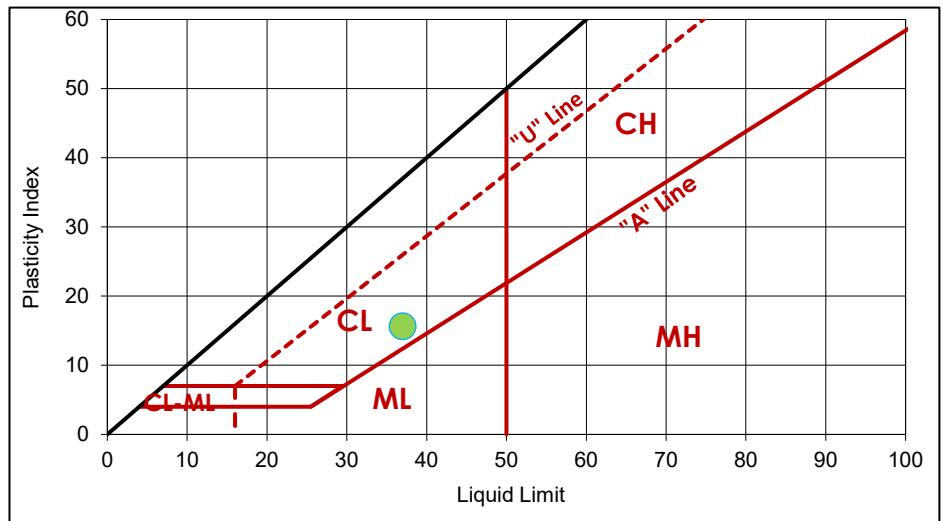
CLIENT FIELD ID BH-211, 0.7 m, DeVries Ave.

STANTEC SAMPLE NO. 5620

	LIQUID LIMIT	
TRIAL	1	2
BLOWS	22	24
MC (%)	38	37

	PLASTIC LIMIT	
TRIAL	1	2
MC (%)	21	22

LIQUID LIMIT, LL	37
PLASTIC LIMIT, PL	21
PLASTICITY INDEX, PI	16
AS REC'D MC (%)	22.2



COMMENTS  
 No comments.



REPORT DATE 2025.Feb.06

REVIEWED BY Guillaume Beauce, P.Eng.  
 Geotechnical Engineer - Materials Testing Services

## ASTM D4318 - LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX OF SOILS (LL METHOD B - ONE-POINT)

TO City of Winnipeg, Public Works Dept.  
 104 - 1155 Pacific Avenue  
 Winnipeg, Manitoba  
 R3E 2P1

PROJECT 2025 Local Street Renewal Program  
 Contract 3

PROJECT NO. 123317463-3

ATTN Geoff Kerr

REPORT NO. 2

DATE SAMPLED: 2025.Jan.08

DATE RECEIVED: 2025.Jan.08

DATE TESTED: 2025.Jan.31

SAMPLED BY: Stantec Consulting Ltd.

SUBMITTED BY: Stantec Consulting Ltd.

TESTED BY: Rimanshi Gorasiya

**MATERIAL IDENTIFICATION**

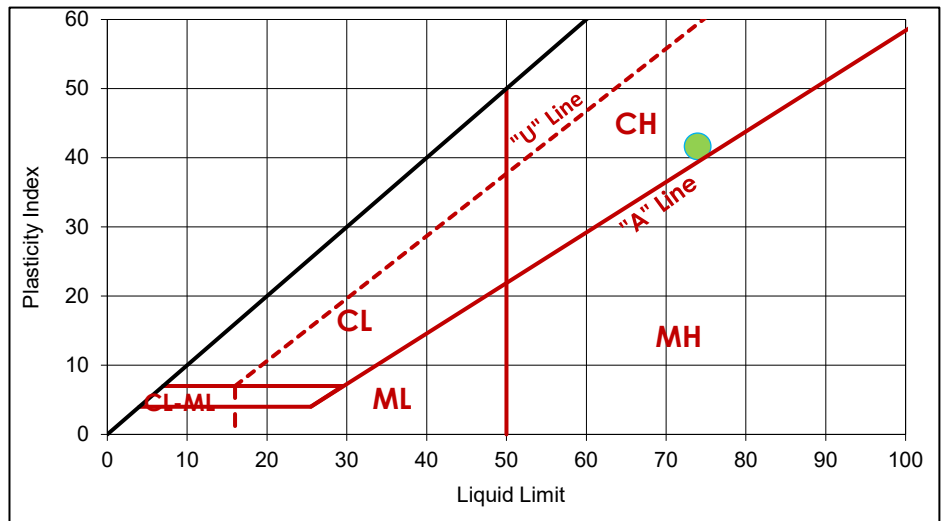
CLIENT FIELD ID BH-212, 0.7 m, DeVries Ave.

STANTEC SAMPLE NO. 5621

	LIQUID LIMIT	
TRIAL	1	2
BLOWS	27	26
MC (%)	74	73

	PLASTIC LIMIT	
TRIAL	1	2
MC (%)	32	32

LIQUID LIMIT, LL	74
PLASTIC LIMIT, PL	32
PLASTICITY INDEX, PI	42
AS REC'D MC (%)	34.5



COMMENTS  
 No comments.



REPORT DATE 2025.Feb.06

REVIEWED BY Guillaume Beauce, P.Eng.  
 Geotechnical Engineer - Materials Testing Services

# ASTM D4318 - LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX OF SOILS (LL METHOD B - ONE-POINT)

TO City of Winnipeg, Public Works Dept.  
 104 - 1155 Pacific Avenue  
 Winnipeg, Manitoba  
 R3E 2P1

PROJECT 2025 Local Street Renewal Program  
 Contract 3

PROJECT NO. 123317463-3

ATTN Geoff Kerr

REPORT NO. 3

DATE SAMPLED: 2025.Jan.08

DATE RECEIVED: 2025.Jan.08

DATE TESTED: 2025.Jan.31

SAMPLED BY: Stantec Consulting Ltd.

SUBMITTED BY: Stantec Consulting Ltd.

TESTED BY: Rimanshi Gorasiya

**MATERIAL IDENTIFICATION**

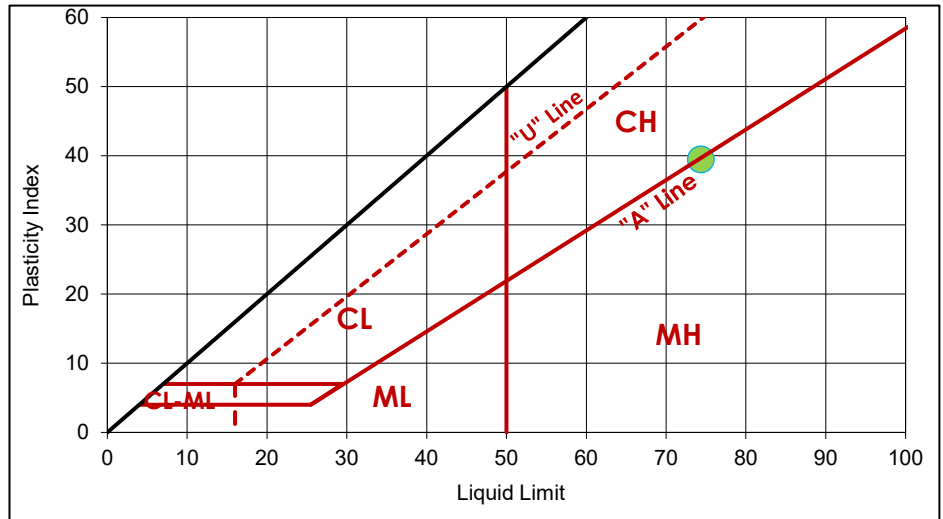
CLIENT FIELD ID BH-213, 0.7 m, DeVries Ave.

STANTEC SAMPLE NO. 5622

TRIAL	LIQUID LIMIT	
	1	2
BLOWS	28	29
MC (%)	73	73

TRIAL	PLASTIC LIMIT	
	1	2
MC (%)	35	35

LIQUID LIMIT, LL	74
PLASTIC LIMIT, PL	35
PLASTICITY INDEX, PI	39
AS REC'D MC (%)	33.5



COMMENTS  
 No comments.



REPORT DATE 2025.Feb.06

REVIEWED BY Guillaume Beauce, P.Eng.  
 Geotechnical Engineer - Materials Testing Services

# ASTM D4318 - LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX OF SOILS (LL METHOD B - ONE-POINT)

TO City of Winnipeg, Public Works Dept.  
 104 - 1155 Pacific Avenue  
 Winnipeg, Manitoba  
 R3E 2P1

PROJECT 2025 Local Street Renewal Program  
 Contract 3

PROJECT NO. 123317463-3

ATTN Geoff Kerr

REPORT NO. 4

DATE SAMPLED: 2025.Jan.08

DATE RECEIVED: 2025.Jan.08

DATE TESTED: 2025.Feb.03

SAMPLED BY: Stantec Consulting Ltd.

SUBMITTED BY: Stantec Consulting Ltd.

TESTED BY: Rimanshi Gorasiya

**MATERIAL IDENTIFICATION**

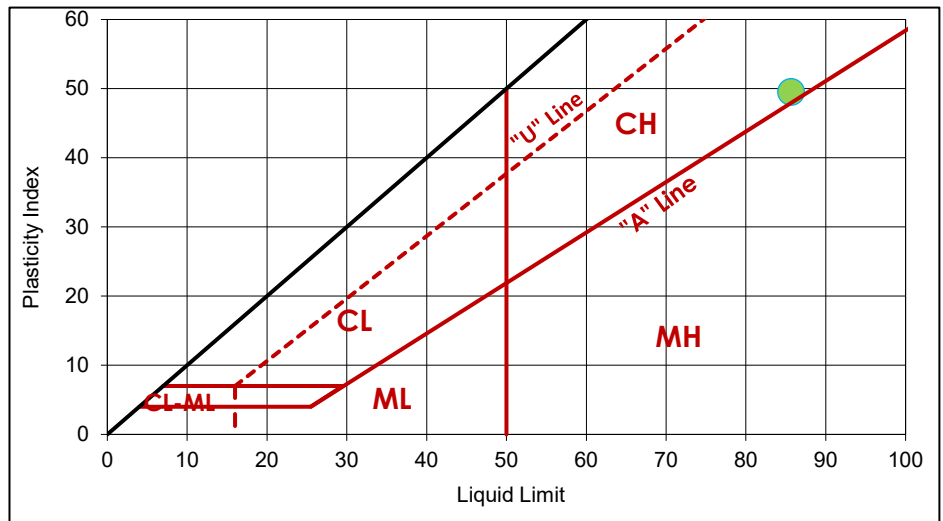
CLIENT FIELD ID BH-214, 0.7 m, DeVries Ave.

STANTEC SAMPLE NO. 5623

	LIQUID LIMIT	
TRIAL	1	2
BLOWS	26	24
MC (%)	86	85

	PLASTIC LIMIT	
TRIAL	1	2
MC (%)	36	36

LIQUID LIMIT, LL	86
PLASTIC LIMIT, PL	36
PLASTICITY INDEX, PI	50
AS REC'D MC (%)	45.0



COMMENTS  
 No comments.



REPORT DATE 2025.Feb.06

REVIEWED BY Guillaume Beauce, P.Eng.  
 Geotechnical Engineer - Materials Testing Services

# ASTM D4318 - LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX OF SOILS (LL METHOD B - ONE-POINT)

TO City of Winnipeg, Public Works Dept.  
 104 - 1155 Pacific Avenue  
 Winnipeg, Manitoba  
 R3E 2P1

PROJECT 2025 Local Street Renewal Program  
 Contract 3

PROJECT NO. 123317463-3

ATTN Geoff Kerr

REPORT NO. 5

DATE SAMPLED: 2025.Jan.08

DATE RECEIVED: 2025.Jan.08

DATE TESTED: 2025.Feb.03

SAMPLED BY: Stantec Consulting Ltd.

SUBMITTED BY: Stantec Consulting Ltd.

TESTED BY: Rimanshi Gorasiya

**MATERIAL IDENTIFICATION**

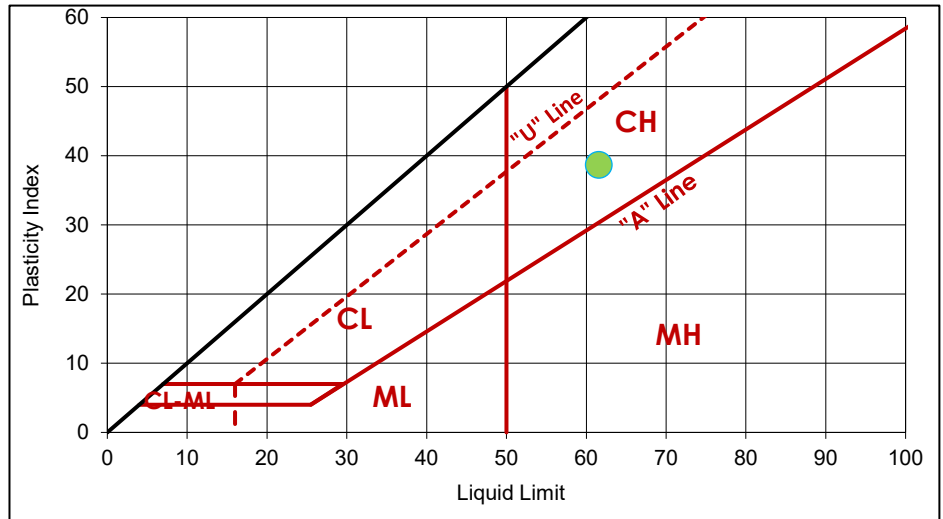
CLIENT FIELD ID BH-215, 0.7 m, DeVries Ave.

STANTEC SAMPLE NO. 5624

	LIQUID LIMIT	
TRIAL	1	2
BLOWS	27	29
MC (%)	61	61

	PLASTIC LIMIT	
TRIAL	1	2
MC (%)	23	23

LIQUID LIMIT, LL	62
PLASTIC LIMIT, PL	23
PLASTICITY INDEX, PI	39
AS REC'D MC (%)	39.6



COMMENTS  
 No comments.



REPORT DATE 2025.Feb.06

REVIEWED BY Guillaume Beauce, P.Eng.  
 Geotechnical Engineer - Materials Testing Services

## ASTM D7928 - PARTICLE-SIZE DISTRIBUTION OF FINE-GRAINED SOILS USING THE SEDIMENTATION ANALYSIS

TO City of Winnipeg, Public Works Dept.  
 104 - 1155 Pacific Avenue  
 Winnipeg, Manitoba  
 R3E 2P1

PROJECT 2025 Local Street Renewal Program  
 Contract 3

PROJECT NO. 123317463-3

ATTN Geoff Kerr

REPORT NO. 1

DATE SAMPLED: 2025.Jan.08

DATE RECEIVED: 2025.Jan.08

DATE TESTED: 2025.Jan.24

SAMPLED BY: Stantec Consulting Ltd.

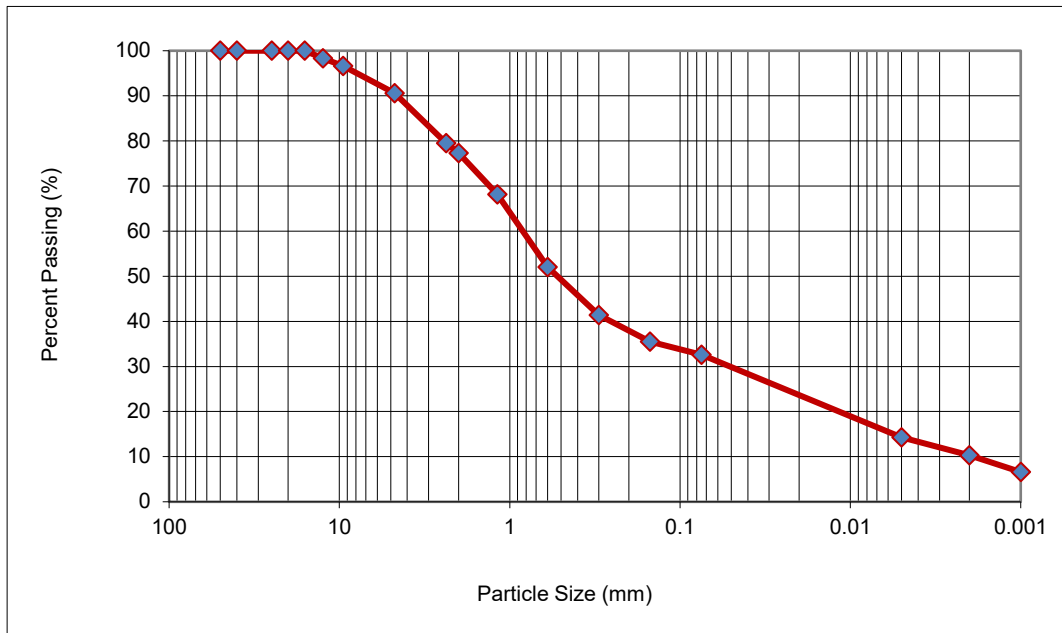
SUBMITTED BY: Stantec Consulting Ltd.

TESTED BY: Rimanshi Gorasiya

**MATERIAL IDENTIFICATION**

CLIENT FIELD ID BH-211. 0.7 m, DeVries Ave.

STANTEC SAMPLE NO. 5620



Sieve Size (mm)	% Passing
50.0	100.0
40.0	100.0
25.0	100.0
20.0	100.0
16.0	100.0
12.5	98.3
9.5	96.7
4.75	90.6
2.36	79.5
2.00	77.3
1.18	68.2
0.600	52.0
0.300	41.4
0.150	35.5
0.075	32.6
0.005	14.3
0.002	10.3
0.001	6.6

Gravel	Sand			Silt	Clay	Colloids
	Coarse	Medium	Fine			
9.4	13.3	31.5	13.2	22.3	10.3	6.6

COMMENTS  
 No comments.



REPORT DATE 2025.Feb.06

REVIEWED BY Guillaume Beauce, P.Eng.  
 Geotechnical Engineer - Materials Testing Services



## ASTM D7928 - PARTICLE-SIZE DISTRIBUTION OF FINE-GRAINED SOILS USING THE SEDIMENTATION ANALYSIS

TO City of Winnipeg, Public Works Dept.  
 104 - 1155 Pacific Avenue  
 Winnipeg, Manitoba  
 R3E 2P1

PROJECT 2025 Local Street Renewal Program  
 Contract 3

PROJECT NO. 123317463-3

ATTN Geoff Kerr

REPORT NO. 2

DATE SAMPLED: 2025.Jan.08

DATE RECEIVED: 2025.Jan.08

DATE TESTED: 2025.Jan.24

SAMPLED BY: Stantec Consulting Ltd.

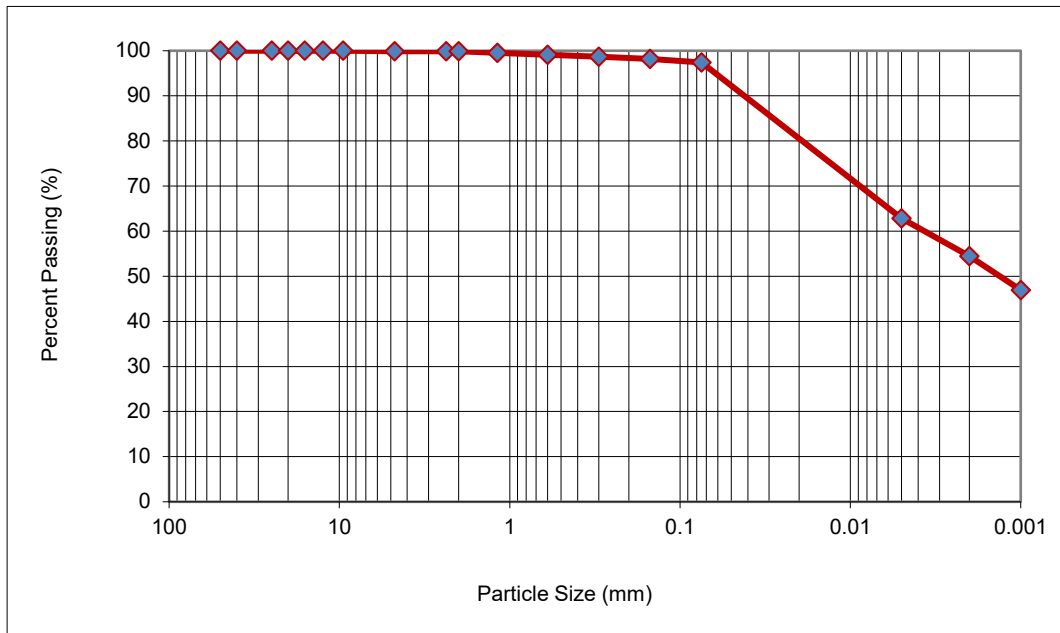
SUBMITTED BY: Stantec Consulting Ltd.

TESTED BY: Rimanshi Gorasiya

**MATERIAL IDENTIFICATION**

CLIENT FIELD ID BH-212. 0.7 m, DeVries Ave.

STANTEC SAMPLE NO. 5621



Sieve Size (mm)	% Passing
50.0	100.0
40.0	100.0
25.0	100.0
20.0	100.0
16.0	100.0
12.5	100.0
9.5	100.0
4.75	99.9
2.36	99.9
2.00	99.9
1.18	99.5
0.600	99.1
0.300	98.7
0.150	98.2
0.075	97.4
0.005	62.8
0.002	54.5
0.001	47.0

Gravel	Sand			Silt	Clay	Colloids
	Coarse	Medium	Fine			
0.1	0.0	1.0	1.5	42.9	54.5	47.0

COMMENTS  
 No comments.



REPORT DATE 2025.Feb.06

REVIEWED BY Guillaume Beauce, P.Eng.  
 Geotechnical Engineer - Materials Testing Services

## ASTM D7928 - PARTICLE-SIZE DISTRIBUTION OF FINE-GRAINED SOILS USING THE SEDIMENTATION ANALYSIS

TO City of Winnipeg, Public Works Dept.  
 104 - 1155 Pacific Avenue  
 Winnipeg, Manitoba  
 R3E 2P1

PROJECT 2025 Local Street Renewal Program  
 Contract 3

PROJECT NO. 123317463-3

ATTN Geoff Kerr

REPORT NO. 3

DATE SAMPLED: 2025.Jan.08

DATE RECEIVED: 2025.Jan.08

DATE TESTED: 2025.Jan.24

SAMPLED BY: Stantec Consulting Ltd.

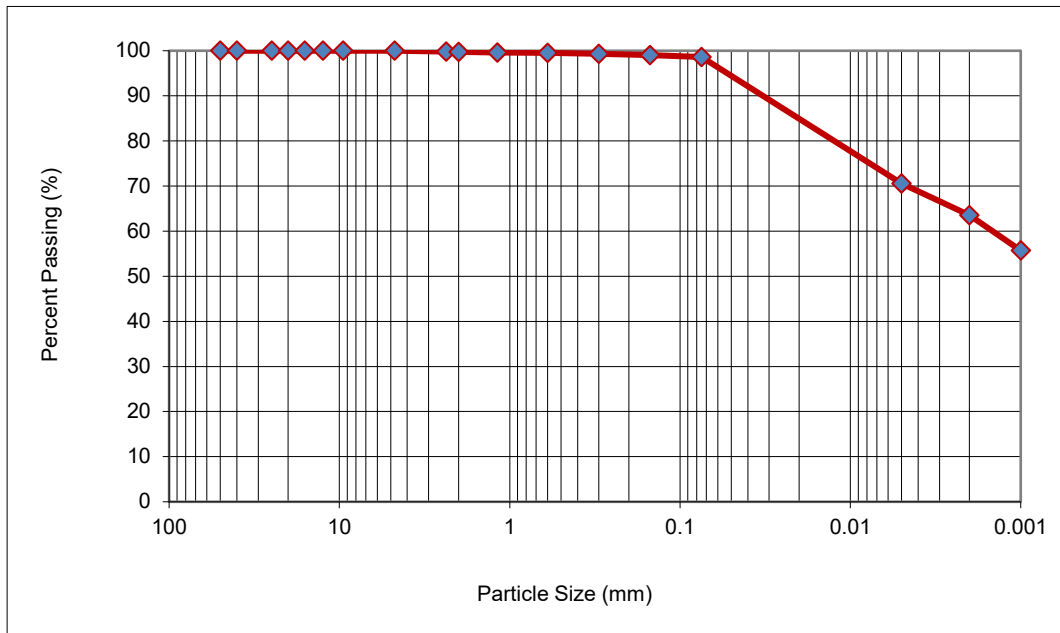
SUBMITTED BY: Stantec Consulting Ltd.

TESTED BY: Rimanshi Gorasiya

**MATERIAL IDENTIFICATION**

CLIENT FIELD ID BH-213. 0.7 m, DeVries Ave.

STANTEC SAMPLE NO. 5622



Sieve Size (mm)	% Passing
50.0	100.0
40.0	100.0
25.0	100.0
20.0	100.0
16.0	100.0
12.5	100.0
9.5	100.0
4.75	100.0
2.36	99.8
2.00	99.7
1.18	99.6
0.600	99.5
0.300	99.3
0.150	99.0
0.075	98.6
0.005	70.6
0.002	63.5
0.001	55.7

Gravel	Sand			Silt	Clay	Colloids
	Coarse	Medium	Fine			
0.0	0.3	0.3	0.8	35.1	63.5	55.7

**COMMENTS**

No comments.



REPORT DATE 2025.Feb.06

REVIEWED BY Guillaume Beauce, P.Eng.  
 Geotechnical Engineer - Materials Testing Services

## ASTM D7928 - PARTICLE-SIZE DISTRIBUTION OF FINE-GRAINED SOILS USING THE SEDIMENTATION ANALYSIS

TO City of Winnipeg, Public Works Dept.  
 104 - 1155 Pacific Avenue  
 Winnipeg, Manitoba  
 R3E 2P1

PROJECT 2025 Local Street Renewal Program  
 Contract 3

PROJECT NO. 123317463-3

ATTN Geoff Kerr

REPORT NO. 4

DATE SAMPLED: 2025.Jan.08

DATE RECEIVED: 2025.Jan.08

DATE TESTED: 2025.Jan.24

SAMPLED BY: Stantec Consulting Ltd.

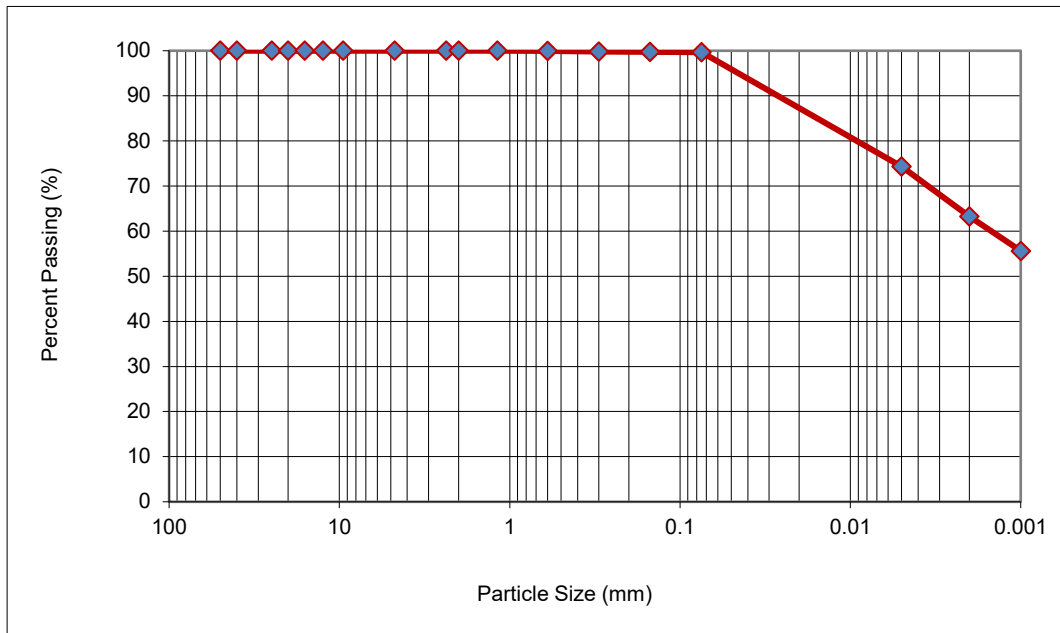
SUBMITTED BY: Stantec Consulting Ltd.

TESTED BY: Rimanshi Gorasiya

**MATERIAL IDENTIFICATION**

CLIENT FIELD ID BH-214. 0.7 m, DeVries Ave.

STANTEC SAMPLE NO. 5623



Sieve Size (mm)	% Passing
50.0	100.0
40.0	100.0
25.0	100.0
20.0	100.0
16.0	100.0
12.5	100.0
9.5	100.0
4.75	100.0
2.36	100.0
2.00	100.0
1.18	100.0
0.600	100.0
0.300	99.8
0.150	99.7
0.075	99.6
0.005	74.4
0.002	63.2
0.001	55.6

Gravel	Sand			Silt	Clay	Colloids
	Coarse	Medium	Fine			
0.0	0.0	0.1	0.3	36.4	63.2	55.6

COMMENTS  
 No comments.



REPORT DATE 2025.Feb.06

REVIEWED BY Guillaume Beauce, P.Eng.  
 Geotechnical Engineer - Materials Testing Services

## ASTM D7928 - PARTICLE-SIZE DISTRIBUTION OF FINE-GRAINED SOILS USING THE SEDIMENTATION ANALYSIS

TO City of Winnipeg, Public Works Dept.  
 104 - 1155 Pacific Avenue  
 Winnipeg, Manitoba  
 R3E 2P1

PROJECT 2025 Local Street Renewal Program  
 Contract 3

PROJECT NO. 123317463-3

ATTN Geoff Kerr

REPORT NO. 5

DATE SAMPLED: 2025.Jan.08

DATE RECEIVED: 2025.Jan.08

DATE TESTED: 2025.Jan.24

SAMPLED BY: Stantec Consulting Ltd.

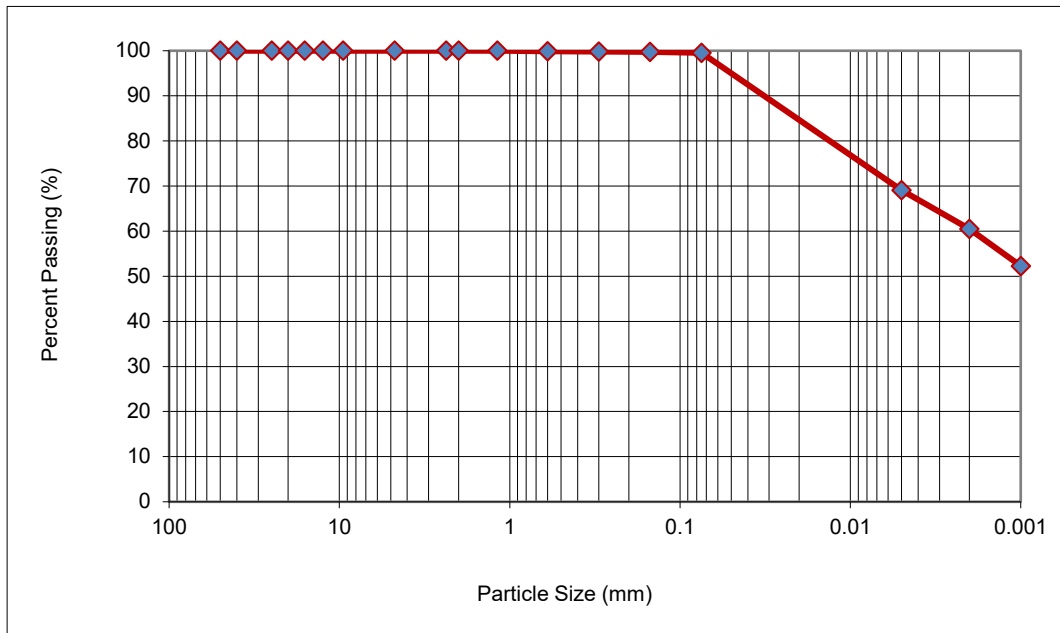
SUBMITTED BY: Stantec Consulting Ltd.

TESTED BY: Rimanshi Gorasiya

**MATERIAL IDENTIFICATION**

CLIENT FIELD ID BH-215. 0.7 m, DeVries Ave.

STANTEC SAMPLE NO. 5624



Sieve Size (mm)	% Passing
50.0	100.0
40.0	100.0
25.0	100.0
20.0	100.0
16.0	100.0
12.5	100.0
9.5	100.0
4.75	100.0
2.36	100.0
2.00	100.0
1.18	100.0
0.600	99.9
0.300	99.8
0.150	99.7
0.075	99.6
0.005	69.1
0.002	60.5
0.001	52.3

Gravel	Sand			Silt	Clay	Colloids
	Coarse	Medium	Fine			
0.0	0.0	0.1	0.3	39.1	60.5	52.3

**COMMENTS**

No comments.



REPORT DATE 2025.Feb.06

REVIEWED BY Guillaume Beauce, P.Eng.  
 Geotechnical Engineer - Materials Testing Services

# PROCTOR TEST REPORT

TO City of Winnipeg  
 104 - 1155 Pacific Ave.  
 Winnipeg, MB  
 R3E 2P1

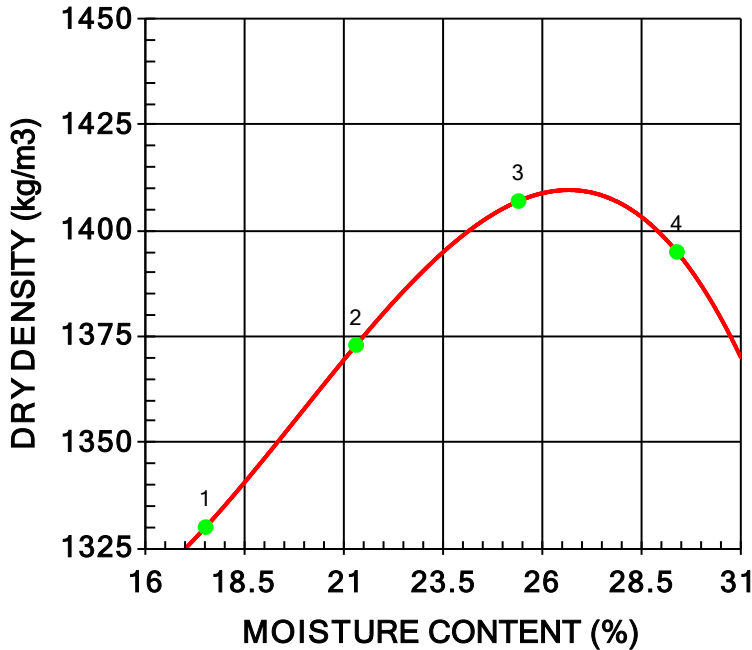
CLIENT City of Winnipeg  
 C.C.

ATTN: Geoff Kerr

PROJECT 2025 Local Street Renewal Program

PROJECT NO. 123317463-3 - Contract 3  
 PROCTOR NO. 1 DATE SAMPLED 2025.Jan.07 DATE RECEIVED 2025.Jan.07 DATE TESTED 2025.Jan.27

INSITU MOISTURE	38.3 %	COMPACTION STANDARD	Standard Proctor, ASTM
TESTED BY	Donald Eliazar		D698
MATERIAL IDENTIFICATION		COMPACTION PROCEDURE	A: 101.6mm Mold, Passing 4.75mm
MAJOR COMPONENT	Subgrade	RAMMER TYPE	Manual
SIZE	Silty Sand (SM)	PREPARATION	Moist
DESCRIPTION		OVERSIZE CORRECTION METHOD	None
SUPPLIER	Existing Materials	RETAINED 4.75mm SCREEN	N/A %
SOURCE	BH-211, 0.7 m (De Vries Ave)		



TRIAL NUMBER	WET DENSITY (kg/m³)	DRY DENSITY (kg/m³)	MOISTURE CONTENT (%)
1	1563	1330	17.5
2	1665	1373	21.3
3	1764	1407	25.4
4	1805	1395	29.4

	MAXIMUM DRY DENSITY (kg/m³)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	1410	26.5
OVERSIZE CORRECTED		

**COMMENTS**

Stantec Sample No. 5620.

# PROCTOR TEST REPORT

TO City of Winnipeg  
 104 - 1155 Pacific Ave.  
 Winnipeg, MB  
 R3E 2P1

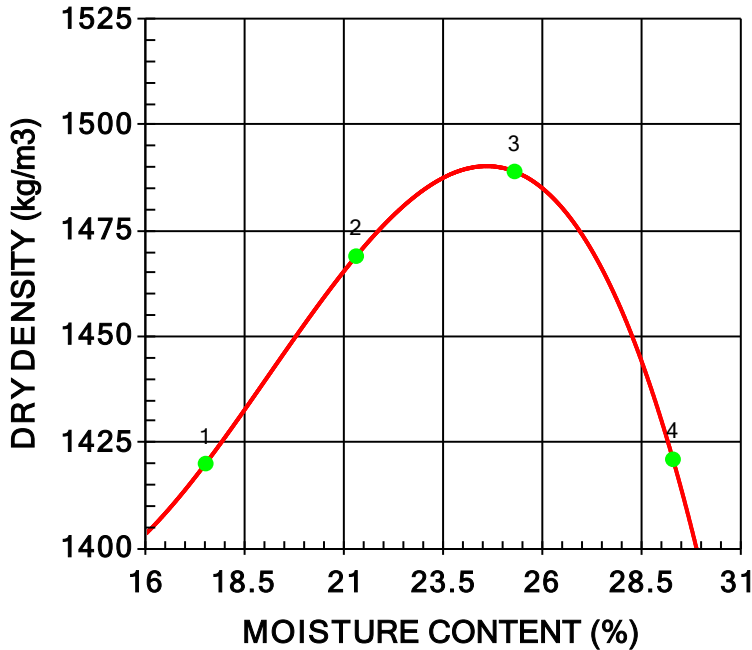
CLIENT City of Winnipeg  
 C.C.

ATTN: Geoff Kerr

PROJECT 2025 Local Street Renewal Program

PROJECT NO. 123317463-3 - Contract 3  
 PROCTOR NO. 2 DATE SAMPLED 2025.Jan.07 DATE RECEIVED 2025.Jan.07 DATE TESTED 2025.Jan.27

INSITU MOISTURE	29.5 %	COMPACTION STANDARD	Standard Proctor, ASTM
TESTED BY	Donald Eliazar		D698
MATERIAL IDENTIFICATION		COMPACTION PROCEDURE	A: 101.6mm Mold, Passing 4.75mm
MAJOR COMPONENT	Subgrade	RAMMER TYPE	Manual
SIZE	Fat Clay (CH)	PREPARATION	Moist
DESCRIPTION		OVERSIZE CORRECTION METHOD	None
SUPPLIER	Existing Materials	RETAINED 4.75mm SCREEN	N/A %
SOURCE	BH-212, 0.7 m (De Vries Ave)		



TRIAL NUMBER	WET DENSITY (kg/m³)	DRY DENSITY (kg/m³)	MOISTURE CONTENT (%)
1	1668	1420	17.5
2	1782	1469	21.3
3	1866	1489	25.3
4	1837	1421	29.3

	MAXIMUM DRY DENSITY (kg/m³)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	1490	24.5
OVERSIZE CORRECTED		

**COMMENTS**

Stantec Sample No. 5621.



Jason Thompson, C.E.T.

# PROCTOR TEST REPORT

TO City of Winnipeg  
 104 - 1155 Pacific Ave.  
 Winnipeg, MB  
 R3E 2P1

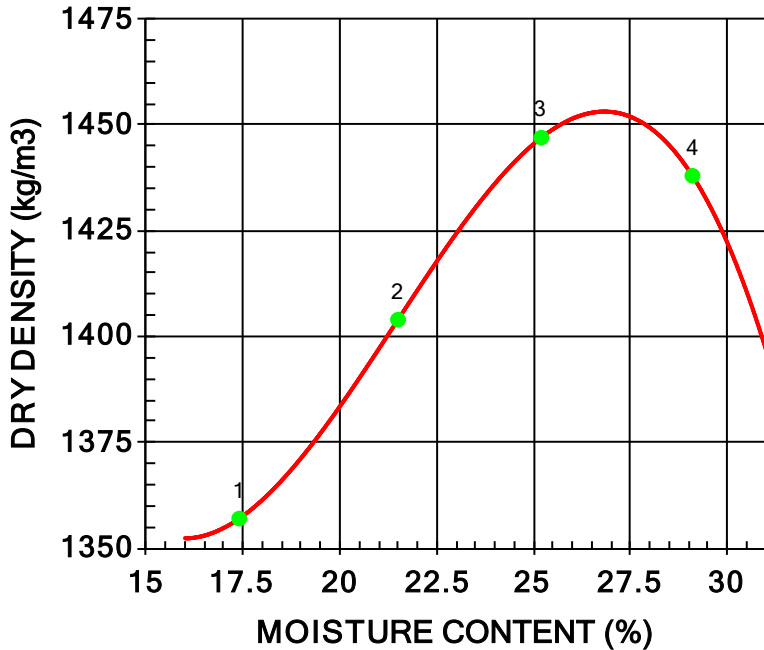
CLIENT City of Winnipeg  
 C.C.

ATTN: Geoff Kerr

PROJECT 2025 Local Street Renewal Program

PROJECT NO. 123317463-3 - Contract 3  
 PROCTOR NO. 3 DATE SAMPLED 2025.Jan.07 DATE RECEIVED 2025.Jan.07 DATE TESTED 2025.Jan.27

INSITU MOISTURE	32.5 %	COMPACTION STANDARD	Standard Proctor, ASTM
TESTED BY	Donald Eliazar		D698
MATERIAL IDENTIFICATION		COMPACTION PROCEDURE	A: 101.6mm Mold, Passing 4.75mm
MAJOR COMPONENT	Subgrade	RAMMER TYPE	Manual
SIZE	Fat Clay (CH)	PREPARATION	Moist
DESCRIPTION		OVERSIZE CORRECTION METHOD	None
SUPPLIER	Existing Materials	RETAINED 4.75mm SCREEN	N/A %
SOURCE	BH-213, 0.7 m (De Vries Ave)		



TRIAL NUMBER	WET DENSITY (kg/m³)	DRY DENSITY (kg/m³)	MOISTURE CONTENT (%)
1	1593	1357	17.4
2	1706	1404	21.5
3	1812	1447	25.2
4	1856	1438	29.1

	MAXIMUM DRY DENSITY (kg/m³)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	1450	27.0
OVERSIZE CORRECTED		

**COMMENTS**

Stantec Sample No. 5622.

# PROCTOR TEST REPORT

TO City of Winnipeg  
 104 - 1155 Pacific Ave.  
 Winnipeg, MB  
 R3E 2P1

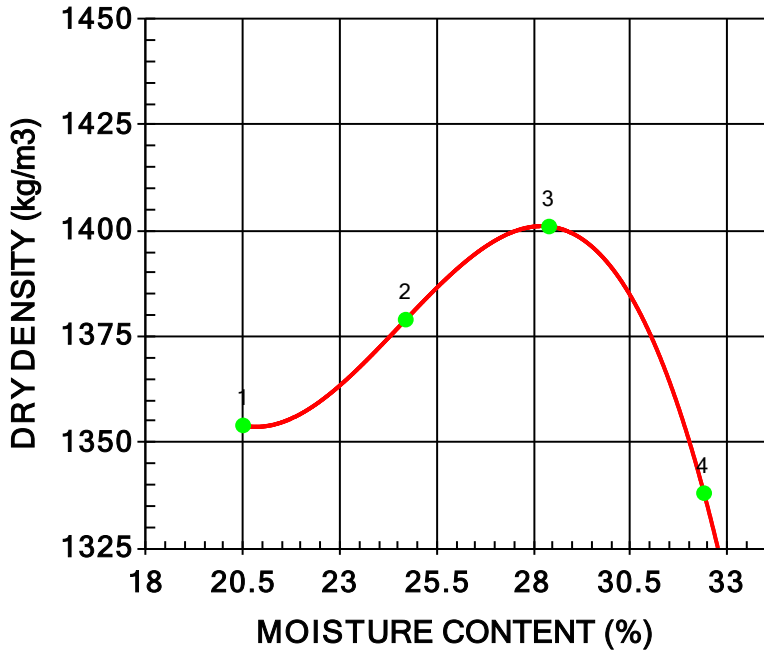
CLIENT City of Winnipeg  
 C.C.

ATTN: Geoff Kerr

PROJECT 2025 Local Street Renewal Program

PROJECT NO. 123317463-3 - Contract 3  
 PROCTOR NO. 4 DATE SAMPLED 2025.Jan.08 DATE RECEIVED 2025.Jan.09 DATE TESTED 2025.Jan.30

INSITU MOISTURE	34.5 %	COMPACTION STANDARD	Standard Proctor, ASTM
TESTED BY	Donald Eliazar		D698
MATERIAL IDENTIFICATION		COMPACTION PROCEDURE	A: 101.6mm Mold, Passing 4.75mm
MAJOR COMPONENT	Subgrade	RAMMER TYPE	Manual
SIZE	Fat Clay (CH)	PREPARATION	Moist
DESCRIPTION		OVERSIZE CORRECTION METHOD	None
SUPPLIER	Existing Material	RETAINED 4.75mm SCREEN	N/A %
SOURCE	BH-214, 0.7 m (De Vries Ave)		



TRIAL NUMBER	WET DENSITY (kg/m³)	DRY DENSITY (kg/m³)	MOISTURE CONTENT (%)
1	1632	1354	20.5
2	1720	1379	24.7
3	1799	1401	28.4
4	1772	1338	32.4

	MAXIMUM DRY DENSITY (kg/m³)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	1400	28.0
OVERSIZE CORRECTED		

**COMMENTS**

Stantec Sample No. 5623.



# PROCTOR TEST REPORT

TO City of Winnipeg  
 104 - 1155 Pacific Ave.  
 Winnipeg, MB  
 R3E 2P1

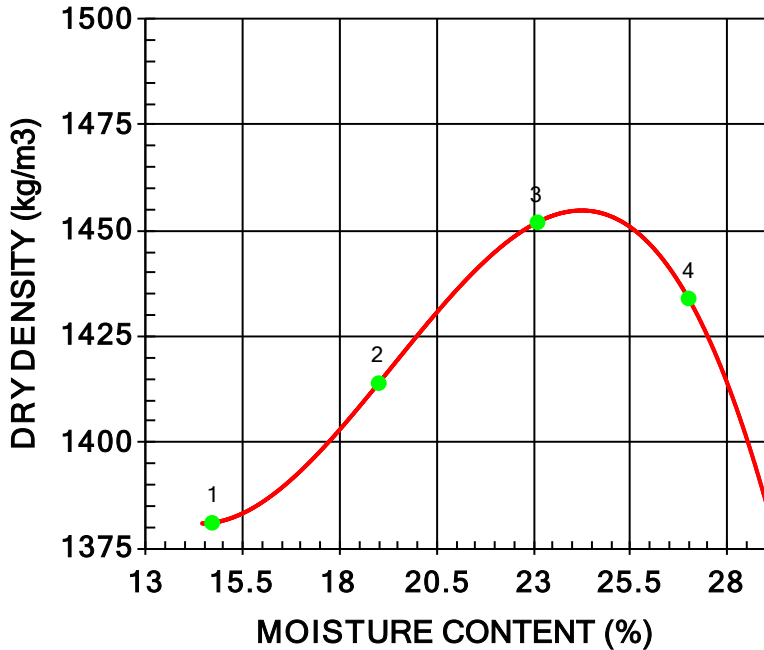
CLIENT City of Winnipeg  
 C.C.

ATTN: Geoff Kerr

PROJECT 2025 Local Street Renewal Program

PROJECT NO. 123317463-3 - Contract 3  
 PROCTOR NO. 5 DATE SAMPLED 2025.Jan.07 DATE RECEIVED 2025.Jan.07 DATE TESTED 2025.Jan.31

INSITU MOISTURE	30.3 %	COMPACTION STANDARD	Standard Proctor, ASTM
TESTED BY	Donald Eliazar		D698
MATERIAL IDENTIFICATION		COMPACTION PROCEDURE	A: 101.6mm Mold, Passing 4.75mm
MAJOR COMPONENT	Subgrade	RAMMER TYPE	Manual
SIZE	Fat Clay (CH)	PREPARATION	Moist
DESCRIPTION		OVERSIZE CORRECTION METHOD	None
SUPPLIER	Existing Materials	RETAINED 4.75mm SCREEN	N/A %
SOURCE	BH-215, 0.7 m (De Vries Ave)		



TRIAL NUMBER	WET DENSITY (kg/m³)	DRY DENSITY (kg/m³)	MOISTURE CONTENT (%)
1	1584	1381	14.7
2	1683	1414	19.0
3	1787	1452	23.1
4	1821	1434	27.0

	MAXIMUM DRY DENSITY (kg/m³)	OPTIMUM MOISTURE CONTENT (%)
CALCULATED	1460	24.5
OVERSIZE CORRECTED		

**COMMENTS**

Stantec Sample No. 5624.

## ASTM D1883 - CALIFORNIA BEARING RATIO (CBR) OF LABORATORY-COMPACTED SOILS

 TO City of Winnipeg, Public Works Dept.  
 104 - 1155 Pacific Avenue  
 Winnipeg, Manitoba  
 R3E 3P1

 PROJECT 2025 Local Street Renewals Program  
 Contract 3

PROJECT NO. 123317463-3

ATTN Geoff Kerr

REPORT NO. 1

 DATE SAMPLED: 2025.Jan.08  
 SAMPLED BY: Larry Presado

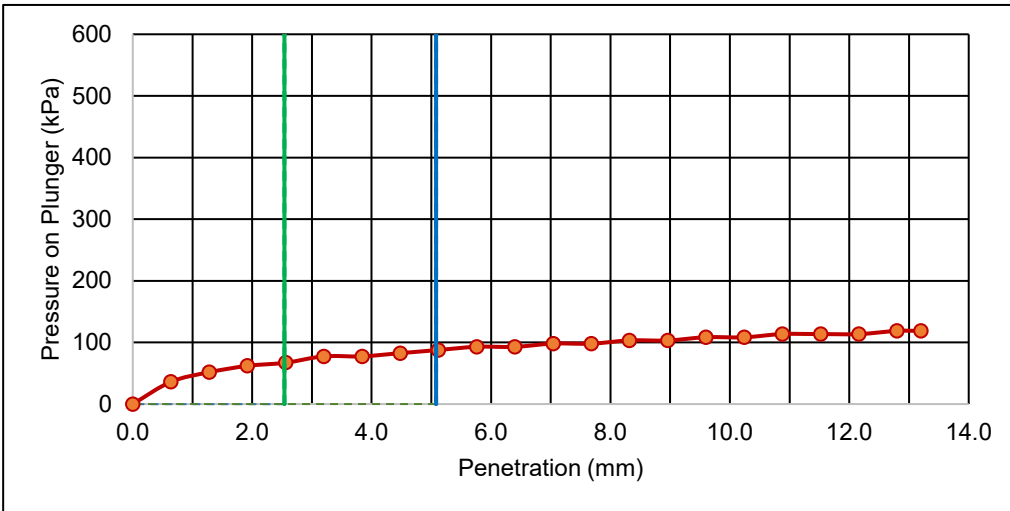
 DATE RECEIVED: 2025.Jan.08  
 SUBMITTED BY: Larry Presado

 DATE TESTED: 2025.Jan.30  
 TESTED BY: Donald Eliazar

**MATERIAL IDENTIFICATION**

MATERIAL USE	Subgrade	SUPPLIER	Existing Material
MAX. NOMINAL SIZE	< 4.75 mm	SOURCE	In Situ
MATERIAL TYPE	Silty Sand (SM)	SAMPLE LOCATION	BH-211, 0.7 m - De Vries Ave.
SPECIFICATION ID	Not Applicable	STANTEC SAMPLE NO.	5620

IMMERSION PERIOD	96 ± 2 hr	TARGET MAX. DRY DENSITY	1410 kg/m <sup>3</sup>
CONDITION OF SAMPLE	Soaked	TARGET OPTIMUM MOISTURE	26.5 %
SURCHARGE MASS	4.54 kg		
+19 mm OVERSIZE	0 %	AS-COMPACTED DRY DENSITY	1341 kg/m <sup>3</sup>
SWELL OF SAMPLE	9.25 %	AS-COMPACTED MOISTURE	26.4 %
POST-TEST MOISTURE	53.6 %	AS-COMPACTED % COMPACTION	95 %




<b>CBR VALUE AT 2.54 mm PENETRATION</b> <b>1.0</b>
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<b>CBR VALUE AT 5.08 mm PENETRATION</b> <b>0.9</b>
---

**COMMENTS**

Sample prepared to 95% of the maximum dry density at the optimum moisture content as determined from ASTM D698.

REPORT DATE 2025.Feb.10

 REVIEWED BY Guillaume Beauce, P.Eng. Geotechnical Engineer - Materials Testing Services
--

## ASTM D1883 - CALIFORNIA BEARING RATIO (CBR) OF LABORATORY-COMPACTED SOILS

 TO City of Winnipeg, Public Works Dept.  
 104 - 1155 Pacific Avenue  
 Winnipeg, Manitoba  
 R3E 3P1

 PROJECT 2025 Local Street Renewals Program  
 Contract 3

PROJECT NO. 123317463-3

ATTN Geoff Kerr

REPORT NO. 2

 DATE SAMPLED: 2025.Jan.08  
 SAMPLED BY: Larry Presado

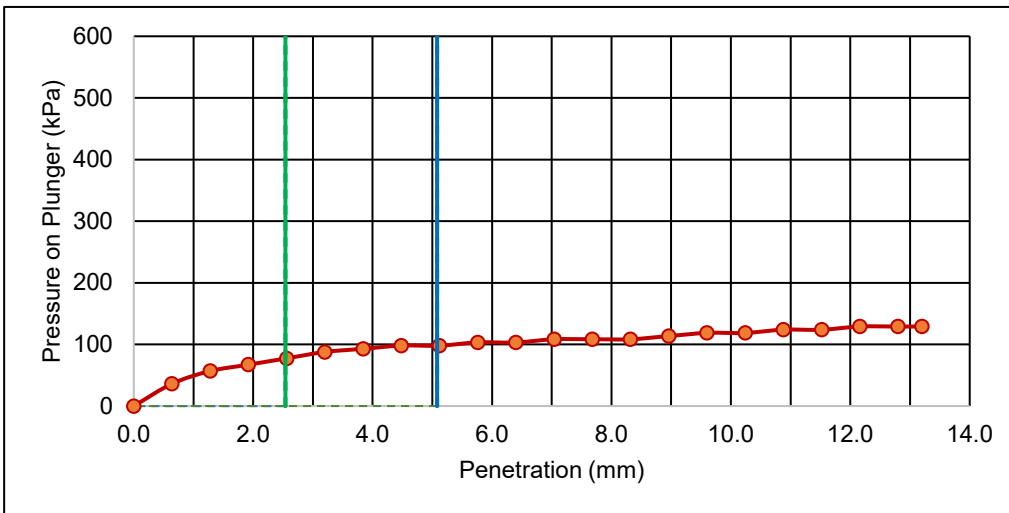
 DATE RECEIVED: 2025.Jan.08  
 SUBMITTED BY: Larry Presado

 DATE TESTED: 2025.Jan.30  
 TESTED BY: Donald Eliazar

**MATERIAL IDENTIFICATION**

MATERIAL USE	Subgrade	SUPPLIER	Existing Material
MAX. NOMINAL SIZE	< 4.75 mm	SOURCE	In Situ
MATERIAL TYPE	Fat Clay (CH)	SAMPLE LOCATION	BH-212, 0.7 m - De Vries Ave.
SPECIFICATION ID	Not Applicable	STANTEC SAMPLE NO.	5621

IMMERSION PERIOD	96 ± 2 hr	TARGET MAX. DRY DENSITY	1490 kg/m <sup>3</sup>
CONDITION OF SAMPLE	Soaked	TARGET OPTIMUM MOISTURE	24.5 %
SURCHARGE MASS	4.54 kg		
+19 mm OVERSIZE	0 %	AS-COMPACTED DRY DENSITY	1415 kg/m <sup>3</sup>
SWELL OF SAMPLE	9.15 %	AS-COMPACTED MOISTURE	24.6 %
POST-TEST MOISTURE	52.8 %	AS-COMPACTED % COMPACTION	95 %




<b>CBR VALUE AT 2.54 mm PENETRATION</b> <b>1.1</b>
---

<b>CBR VALUE AT 5.08 mm PENETRATION</b> <b>1.0</b>
---

**COMMENTS**

Sample prepared to 95% of the maximum dry density at the optimum moisture content as determined from ASTM D698.

REPORT DATE 2025.Feb.10

  
 REVIEWED BY Guillaume Beauce, P.Eng.  
 Geotechnical Engineer - Materials Testing Services

## ASTM D1883 - CALIFORNIA BEARING RATIO (CBR) OF LABORATORY-COMPACTED SOILS

TO City of Winnipeg, Public Works Dept.  
 104 - 1155 Pacific Avenue  
 Winnipeg, Manitoba  
 R3E 3P1

PROJECT 2025 Local Street Renewals Program  
 Contract 3

PROJECT NO. 123317463-3

ATTN Geoff Kerr

REPORT NO. 3

DATE SAMPLED: 2025.Jan.08  
 SAMPLED BY: Larry Presado

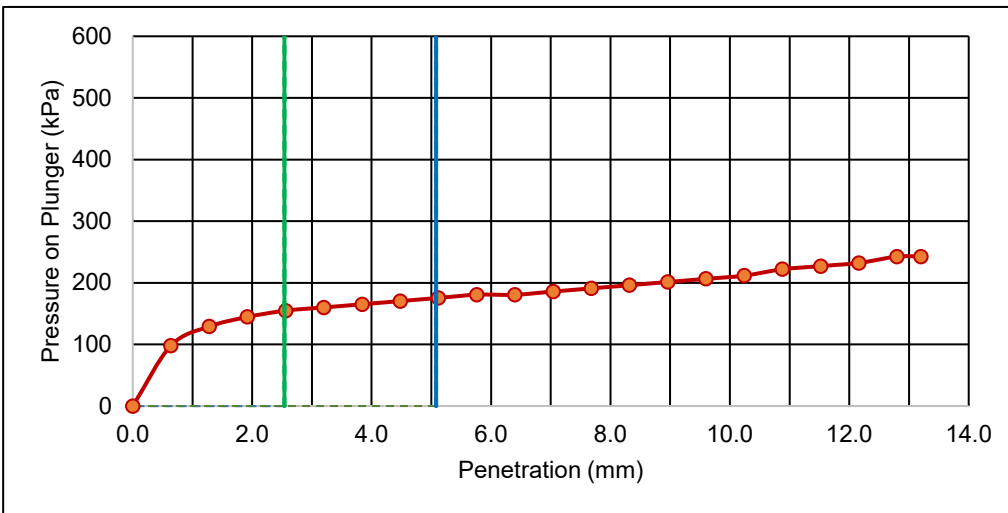
DATE RECEIVED: 2025.Jan.08  
 SUBMITTED BY: Larry Presado

DATE TESTED: 2025.Feb.04  
 TESTED BY: Donald Eliazar

**MATERIAL IDENTIFICATION**

MATERIAL USE	Subgrade	SUPPLIER	Existing Material
MAX. NOMINAL SIZE	< 4.75 mm	SOURCE	In Situ
MATERIAL TYPE	Fat Clay (CH)	SAMPLE LOCATION	BH-213, 0.7 m - De Vries Ave.
SPECIFICATION ID	Not Applicable	STANTEC SAMPLE NO.	5622

IMMERSION PERIOD	96 ± 2 hr	TARGET MAX. DRY DENSITY	1450 kg/m <sup>3</sup>
CONDITION OF SAMPLE	Soaked	TARGET OPTIMUM MOISTURE	27.0 %
SURCHARGE MASS	4.54 kg		
+19 mm OVERSIZE	0 %	AS-COMPACTED DRY DENSITY	1377 kg/m <sup>3</sup>
SWELL OF SAMPLE	4.05 %	AS-COMPACTED MOISTURE	27.1 %
POST-TEST MOISTURE	38.4 %	AS-COMPACTED % COMPACTION	95 %




**CBR VALUE AT 2.54 mm PENETRATION**  
2.2

**CBR VALUE AT 5.08 mm PENETRATION**  
1.8

**COMMENTS**

Sample prepared to 95% of the maximum dry density at the optimum moisture content as determined from ASTM D698.

REPORT DATE 2025.Feb.10

  
 REVIEWED BY Guillaume Beauce, P.Eng.  
 Geotechnical Engineer - Materials Testing Services

## ASTM D1883 - CALIFORNIA BEARING RATIO (CBR) OF LABORATORY-COMPACTED SOILS

TO City of Winnipeg, Public Works Dept.  
 104 - 1155 Pacific Avenue  
 Winnipeg, Manitoba  
 R3E 3P1

PROJECT 2025 Local Street Renewals Program  
 Contract 3

PROJECT NO. 123317463-3

ATTN Geoff Kerr

REPORT NO. 4

DATE SAMPLED: 2025.Jan.08  
 SAMPLED BY: Larry Presado

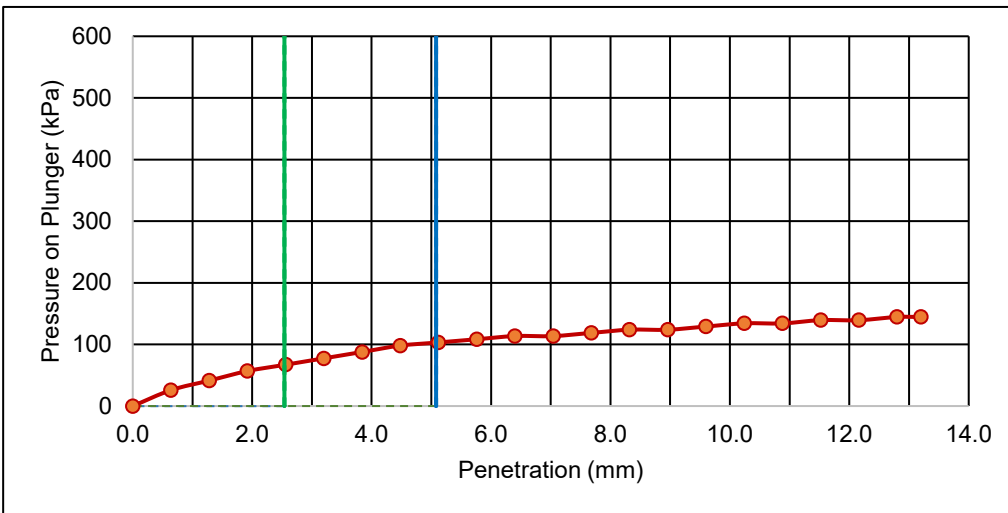
DATE RECEIVED: 2025.Jan.08  
 SUBMITTED BY: Larry Presado

DATE TESTED: 2025.Feb.04  
 TESTED BY: Donald Eliazar

**MATERIAL IDENTIFICATION**

MATERIAL USE	Subgrade	SUPPLIER	Existing Material
MAX. NOMINAL SIZE	< 4.75 mm	SOURCE	In Situ
MATERIAL TYPE	Fat Clay (CH)	SAMPLE LOCATION	BH-214, 0.7 m - De Vries Ave.
SPECIFICATION ID	Not Applicable	STANTEC SAMPLE NO.	5623

IMMERSION PERIOD	96 ± 2 hr	TARGET MAX. DRY DENSITY	1400 kg/m <sup>3</sup>
CONDITION OF SAMPLE	Soaked	TARGET OPTIMUM MOISTURE	28.0 %
SURCHARGE MASS	4.54 kg		
+19 mm OVERSIZE	0 %	AS-COMPACTED DRY DENSITY	1331 kg/m <sup>3</sup>
SWELL OF SAMPLE	7.69 %	AS-COMPACTED MOISTURE	27.9 %
POST-TEST MOISTURE	47.7 %	AS-COMPACTED % COMPACTION	95 %




**CBR VALUE AT 2.54 mm  
PENETRATION**  
1.0

**CBR VALUE AT 5.08 mm  
PENETRATION**  
1.0

**COMMENTS**

Sample prepared to 95% of the maximum dry density at the optimum moisture content as determined from ASTM D698.

REPORT DATE 2025.Feb.10

  
 REVIEWED BY Guillaume Beauce, P.Eng.  
 Geotechnical Engineer - Materials Testing Services

## ASTM D1883 - CALIFORNIA BEARING RATIO (CBR) OF LABORATORY-COMPACTED SOILS

TO City of Winnipeg, Public Works Dept.  
 104 - 1155 Pacific Avenue  
 Winnipeg, Manitoba  
 R3E 3P1

PROJECT 2025 Local Street Renewals Program  
 Contract 3

PROJECT NO. 123317463-3

ATTN Geoff Kerr

REPORT NO. 5

DATE SAMPLED: 2025.Jan.08  
 SAMPLED BY: Larry Presado

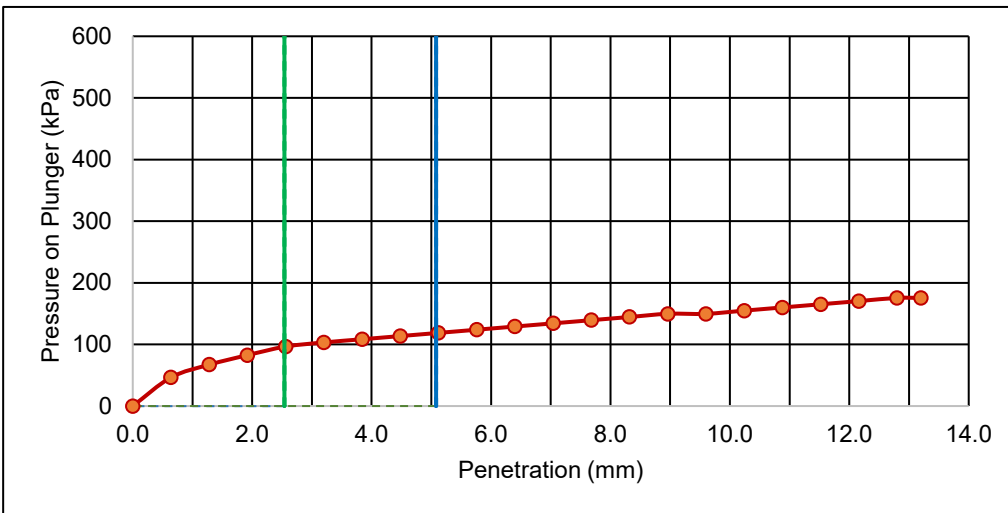
DATE RECEIVED: 2025.Jan.08  
 SUBMITTED BY: Larry Presado

DATE TESTED: 2025.Feb.04  
 TESTED BY: Donald Eliazar

**MATERIAL IDENTIFICATION**

MATERIAL USE	Subgrade	SUPPLIER	Existing Material
MAX. NOMINAL SIZE	< 4.75 mm	SOURCE	In Situ
MATERIAL TYPE	Fat Clay (CH)	SAMPLE LOCATION	BH-215, 0.7 m - De Vries Ave.
SPECIFICATION ID	Not Applicable	STANTEC SAMPLE NO.	5624

IMMERSION PERIOD	96 ± 2 hr	TARGET MAX. DRY DENSITY	1460 kg/m <sup>3</sup>
CONDITION OF SAMPLE	Soaked	TARGET OPTIMUM MOISTURE	24.5 %
SURCHARGE MASS	4.54 kg		
+19 mm OVERSIZE	0 %	AS-COMPACTED DRY DENSITY	1388 kg/m <sup>3</sup>
SWELL OF SAMPLE	6.68 %	AS-COMPACTED MOISTURE	24.4 %
POST-TEST MOISTURE	38.8 %	AS-COMPACTED % COMPACTION	95 %



**CBR VALUE AT 2.54 mm PENETRATION**  
1.4

**CBR VALUE AT 5.08 mm PENETRATION**  
1.2

**COMMENTS**

Sample prepared to 95% of the maximum dry density at the optimum moisture content as determined from ASTM D698.



REPORT DATE 2025.Feb.10

REVIEWED BY Guillaume Beauce, P.Eng.  
 Geotechnical Engineer - Materials Testing Services

Core No.	Street	Diameter (mm)	Length (mm)	L/D Ratio	Correction Factor	Peak Load (kN)	Compressive Strength (MPa)	
							Measured	Corrected
219	Kingsford Ave	75.71	170.44	2.251	1.0000	245.75	54.59	54.59
220	Kingsford Ave	75.68	154.22	2.038	1.0000	191.49	42.57	42.57
221	Kingsford Ave	75.50	129.37	1.714	0.9771	232.94	52.03	50.84
222	Corrine St	75.61	136.89	1.810	0.9848	206.79	46.06	45.36
223	Corrine St	75.55	143.38	1.898	0.9918	214.39	47.82	47.43
224	Callum Cr	75.67	160.77	2.125	1.0000	222.67	49.51	49.51
225	Callum Cr	75.61	157.98	2.089	1.0000	215.77	48.06	48.06
226	Callum Cr	75.67	134.40	1.776	0.9821	247.62	55.06	54.08
227	Callum Cr	75.72	77.44	1.023	0.8755	276.98	61.51	53.85
228	Dunits Dr	75.66	155.37	2.054	1.0000	361.71	80.45	80.45
229	Dunits Dr	75.54	151.55	2.006	1.0000	318.30	71.02	71.02
230	Dunits Dr	75.85	91.18	1.202	0.9185	361.04	79.90	73.39
231	Dunits Dr	<i>Crumbly/fractured core; test cancelled</i>						
232	Dunits Dr	75.73	137.61	1.817	0.9854	327.73	72.76	71.70
233	Dunits Dr	75.67	146.09	1.931	0.9945	384.71	85.55	85.07